

Serial No. 143

DEPARTMENT OF COMMERCE  
U.S. COAST AND GEODETIC SURVEY  
E. LESTER JONES, Director

---

# LATITUDE DEVELOPMENTS CONNECTED WITH GEODESY AND CARTOGRAPHY

WITH TABLES

INCLUDING A TABLE FOR

## LAMBERT EQUAL AREA MERIDIONAL PROJECTION

BY

OSCAR S. ADAMS

Geodetic Computer

---

Special Publication No. 67

QB  
275  
.435  
no. 67  
(1949)



UNITED STATES  
GOVERNMENT PRINTING OFFICE  
WASHINGTON : 1949

# **National Oceanic and Atmospheric Administration**

## **ERRATA NOTICE**

One or more conditions of the original document may affect the quality of the image, such as:

Discolored pages

Faded or light ink

Binding intrudes into the text

This has been a co-operative project between the NOAA Central Library and the Climate Database Modernization Program, National Climate Data Center (NCDC). To view the original document, please contact the NOAA Central Library in Silver Spring, MD at (301) 713-2607 x124 or [www.reference@nodc.noaa.gov](mailto:www.reference@nodc.noaa.gov).

LASON

Imaging Contractor

12200 Kiln Court

Beltsville, MD 20704-1387

January 1, 2006



## CONTENTS.

|   | Page. |
|---|-------|
| Foreword.....   | 5     |
| Derivation of definitions.....  | 7     |
| Recapitulation of definitions.....  | 12    |
| Development of $\varphi-\psi$ in terms of $\varphi$ .....   | 13    |
| Development of $\varphi-\psi$ in terms of $\psi$ .....  | 14    |
| Development of $\varphi-\theta$ in terms of $\varphi$ .....   | 15    |
| Development of $\varphi-\theta$ in terms of $\theta$ .....  | 15    |
| Development of $\theta-\psi$ in terms of $\theta$ and in terms of $\psi$ .....  | 15    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —first method.....  | 16    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —second method.....   | 18    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —third method.....  | 21    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —fourth method.....   | 23    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —fifth method.....  | 26    |
| Development of $\varphi-\chi$ in terms of $\varphi$ —sixth method.....  | 28    |
| Development of $\varphi-\chi$ in terms of $\chi$ —first method.....   | 32    |
| Development of $\varphi-\chi$ in terms of $\chi$ —second method.....  | 34    |
| Development of $\varphi-\chi$ in terms of $\chi$ —third method.....   | 38    |
| Development of $\varphi-\chi$ in terms of $\chi$ —fourth method.....  | 41    |
| Development of $\varphi-\chi$ in terms of $\chi$ —fifth method.....   | 45    |
| Development of $\varphi-\chi$ in terms of $\chi$ —sixth method.....   | 52    |
| Development of $\varphi-\chi$ in terms of $\chi$ —seventh method.....   | 55    |
| Development of $\varphi-\beta$ in terms of $\varphi$ —first method.....   | 60    |
| Development of $\varphi-\beta$ in terms of $\varphi$ —second method.....  | 63    |
| Development of $\varphi-\beta$ in terms of $\varphi$ —third method.....   | 64    |
| Development of $\varphi-\beta$ in terms of $\varphi$ —fourth method.....  | 66    |
| Development of $\varphi-\beta$ in terms of $\varphi$ —fifth method.....   | 68    |
| Development of $\varphi-\beta$ in terms of $\beta$ —first method.....   | 70    |
| Development of $\varphi-\beta$ in terms of $\beta$ —second method.....  | 71    |
| Development of $\varphi-\beta$ in terms of $\beta$ —third method.....   | 72    |
| Development of $\varphi-\beta$ in terms of $\beta$ —fourth method.....  | 75    |
| Development of $\varphi-\beta$ in terms of $\beta$ —fifth method.....   | 77    |
| Development of $\varphi-\beta$ in terms of $\beta$ —sixth method.....   | 80    |
| Tabulation of all of the developments.....  | 84    |
| Determination of the numerical values of the coefficients in the<br>developments for the Clarke spheroid of 1866.....                               | 85    |
| Reduction table.....  | 88    |
| Latitude transformation—geodetic to geocentric.....   | 91    |
| Latitude transformation—geocentric to geodetic.....   | 93    |
| Latitude transformation—geodetic to parametric.....   | 95    |
| Latitude transformation—parametric to geodetic.....   | 97    |
| Latitude transformation—parametric to geocentric.....   | 99    |
| Latitude transformation—geocentric to parametric.....   | 101   |
| Latitude transformation—geodetic to isometric.....  | 103   |
| Latitude transformation—parametric to isometric.....  | 107   |
| Latitude transformation—geodetic to authalic.....   | 109   |
| Latitude transformation—authalic to geodetic.....   | 111   |
| Transformation from geographical to azimuthal coordinates—<br>center on the equator—values of the great circle central dis-<br>tance, $\zeta$ ..... | 113   |

|  | Page. |
|--|-------|
| Transformation from geographical to azimuthal coordinates—<br>center on the equator—values of the azimuth reckoned from<br>the north, $\alpha$ ..... | 115   |
| Lambert's azimuthal equivalent projection—center on the<br>equator—radial distance in units of the earth's radius, $\rho$ .....                      | 117   |
| Lambert's azimuthal equivalent projection—center on the<br>equator—coordinates in units of the earth's radius .....                                  | 119   |
| Appendix .....   | 122   |
| Definition of rectifying latitude .....  | 122   |
| Development of $\varphi-\omega$ in terms of $\varphi$ .....  | 123   |
| Development of $\varphi-\omega$ in terms of $\omega$ .....   | 126   |
| Tabulation of the development .....  | 127   |
| Latitude transformation—geodetic to rectifying .....   | 129   |
| Latitude transformation—rectifying to geodetic .....   | 131   |

## FOREWORD.

There are five different kinds of latitude that come under consideration in the application of mathematical analysis to questions of geodesy and cartography. It is the aim of this publication to express the difference between the geodetic or astronomic latitude and each of the various four other kinds of latitude in a series of the sines of the multiple arcs. This difference in each case is obtained in an expression in the sines of the multiple arcs of the geodetic or astronomic latitude and also in a series of the sines of the multiple arcs of the other latitude in question.

The analysis connected with the development of both the isometric or conformal latitude <sup>a</sup> and of the authalic or equal-area latitude <sup>a</sup> is given in some degree of detail, since it is a good example of the application of mathematical analysis to such questions.

The series are derived in their general form in the first instance in which no geodetic constant appears except the eccentricity. At the end of the text in this publication the numerical values of the various coefficients are given computed for the Clarke spheroid of 1866. This is the spheroid that is used for all geodetic purposes in North America. Finally, tables are given of the results of the computations for this spheroid calculated for every half degree of latitude. These results and tables will be useful in connection with all geodetic and cartographic questions in which it is desired to take into consideration the spheroidal shape of the earth. It is believed that no previous table has been computed for the Clarke spheroid of 1866, at least none for half degrees of latitude. It is thought that the idea of the authalic latitude is new in the science of cartography. It has been applied in the computation of the elements of an Albers' equal-area projection for the United States, and it has been found materially to simplify the calculations to be performed.

---

<sup>a</sup> For the full definition of these terms see pp. 8 and 10.

It is thought that in a later publication on equivalent or equal-area projections this latitude may be applied in the theory of the various types of projection belonging to this class.

In addition to the latitude tables there are given tables for transformation from latitude and longitude to arc distance and azimuth from a point on the equator. After these is given a table of the radial distance for a Lambert azimuthal equal-area projection upon a meridional plane, and finally a table of the coordinates for such a projection.

It is hoped that the analysis employed in the derivation of the formulas may be of interest to those who have to deal with the applications of mathematical theory to such problems as arise in practice. A few examples of such applications are of more value than any amount of the theory without the practical working out of the results in specific cases. "Learn to do by doing" is a safe maxim at all times. Finally, the numerical form of the results should appeal to those who wish to use these latitudes in questions of geodesy or cartography. The numerical forms of the expansions are given both in numbers and in logarithms. If a multiplying machine is available the coefficients expressed in numbers are more useful, but in case such a machine is not at hand it is necessary to resort to logarithms. With a five-place table of sines the results ought to be good to tenths of a second, and a six-place table should give results good to hundredths of a second. The results of computation given in the tables were derived from an eight-place table of natural sines.

# LATITUDE DEVELOPMENTS CONNECTED WITH GEODESY AND CARTOGRAPHY, WITH TABLES, INCLUDING A TABLE FOR LAMBERT EQUAL-AREA MERIDIONAL PROJECTION.

By OSCAR S. ADAMS,  
*Geodetic Computer, U. S. Coast and Geodetic Survey.*

## DERIVATION OF DEFINITIONS.

In considering subjects connected with geodesy and cartography there are five different kinds of latitude that are found to be of interest and of use in practical applications. We shall now proceed to apply analysis in the derivation of the definitions of these latitudes.

If the meridian ellipse is defined by equations in the parametric form

$$\begin{aligned}x &= a \cos \theta \\y &= b \sin \theta,\end{aligned}$$

then  $\theta$  is called the parametric latitude,  $a$  is the semi-major axis, and  $b$  is the semiminor axis of the meridian ellipse.

The geodetic or astronomic latitude is the angle which the normal at a given point of the ellipse makes with the axis of  $x$ . This latitude, denoted by  $\varphi$ , will then be defined analytically by the expression

$$\tan \varphi = -\frac{dx}{dy},$$

since it is perpendicular to the tangent at the point  $x, y$ . But from the parametric equations we get

$$-\frac{dx}{dy} = \frac{a \sin \theta}{b \cos \theta} = \frac{a}{b} \tan \theta.$$

Hence

$$\tan \varphi = \frac{a}{b} \tan \theta,$$

or

$$\tan \theta = \frac{b}{a} \tan \varphi.$$



The eccentricity,  $\epsilon$ , of the ellipse is defined by the equation

$$\epsilon^2 = \frac{a^2 - b^2}{a^2}.$$

From this expression we get

$$\frac{b}{a} = (1 - \epsilon^2)^{1/2};$$

therefore

$$\tan \theta = (1 - \epsilon^2)^{1/2} \tan \varphi.$$

The geocentric latitude is the angle formed with the axis of  $x$  by the radius vector from the center of the ellipse to the point  $x, y$ . Denoting this latitude by  $\psi$ , we define it by the form

$$\begin{aligned} \tan \psi &= \frac{y}{x} \\ &= \frac{b}{a} \tan \theta \\ &= (1 - \epsilon^2)^{1/2} \tan \theta; \end{aligned}$$

or, in terms of  $\varphi$ , by substituting the value of  $\tan \theta$  in terms of  $\varphi$ , this becomes

$$\tan \psi = (1 - \epsilon^2) \tan \varphi.$$

In the theory of the conformal representation of the spheroid, the function,  $x$ , that forms with the longitude,  $\lambda$ , a set of isometric coordinates is defined by the integral

$$x = - \int_p^{\pi/2} \frac{(1 - \epsilon^2) dp}{(1 - \epsilon^2 \cos^2 p) \sin p},$$

in which  $p$  is the geodetic colatitude.\*

$$\begin{aligned} x = - & \int_p^{\pi/2} \frac{\cos \frac{p}{2} dp}{\sin \frac{p}{2}} + \int_p^{\pi/2} \frac{-\sin \frac{p}{2} dp}{\cos \frac{p}{2}} \\ & - \frac{\epsilon}{2} \int_p^{\pi/2} \frac{-\epsilon \sin p dp}{1 + \epsilon \cos p} + \frac{\epsilon}{2} \int_p^{\pi/2} \frac{\epsilon \sin p dp}{1 - \epsilon \cos p}, \end{aligned}$$

\* See "General Theory of the Lambert Conformal Conic Projection," Special Publication No. 53, United States Coast and Geodetic Survey.

or by integration

$$\begin{aligned} x &= \log_e \sin \frac{p}{2} - \log_e \cos \frac{p}{2} + \frac{\epsilon}{2} \log_e (1 + \epsilon \cos p) \\ &\quad - \frac{\epsilon}{2} \log_e (1 - \epsilon \cos p) \\ &= \log_e \tan \frac{p}{2} + \frac{\epsilon}{2} \log_e \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right). \end{aligned}$$

On passing to exponentials this becomes

$$e^x = \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{1/2}$$

For the sphere, putting  $\epsilon = 0$ , the corresponding coordinate,  $y$ , is defined by the integral

$$y = - \int_z^{\pi/2} \frac{dz}{\sin z},$$

in which  $z$  is the colatitude on the sphere.

$$y = - \int_z^{\pi/2} \frac{\cos \frac{z}{2} dz}{\sin \frac{z}{2}} + \int_z^{\pi/2} \frac{-\sin \frac{z}{2} dz}{\cos \frac{z}{2}}$$

or by integration

$$y = \log_e \tan \frac{z}{2}$$

or

$$e^y = \tan \frac{z}{2}.$$

If we now define  $z$  by the equation

$$\tan \frac{z}{2} = \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{1/2},$$

we shall have determined a conformal representation of the spheroid upon a sphere. If we denote the isometric

latitude by  $\chi$ , and in place of  $z$  substitute its value  $\frac{\pi}{2} - \chi$

and for  $p$  its value  $\frac{\pi}{2} - \varphi$ , we get the definition of the isometric latitude in the form

$$\tan \left( \frac{\pi}{4} + \frac{\chi}{2} \right) = \tan \left( \frac{\pi}{4} + \frac{\varphi}{2} \right) \cdot \left( \frac{1 - \epsilon \sin \varphi}{1 + \epsilon \sin \varphi} \right)^{1/2}$$

This latitude  $\chi$  has been called the isometric latitude because it is determined by means of the isometric coordinate.

Besides these latitudes there is another latitude that arises when the spheroid is projected upon a sphere of equivalent surface in such a way that the representation is equivalent or equal area in every part. The element of area upon the spheroid is given by the equation

$$dS = \frac{a^2(1-\epsilon^2) \cos \varphi}{(1-\epsilon^2 \sin^2 \varphi)^2} d\varphi d\lambda.$$

The area of a section of a lune of width  $d\lambda$  from the Equator to the parallel of latitude  $\phi$  is given by the following integral multiplied by  $d\lambda$

$$S = \int_0^\varphi \frac{a^2(1-\epsilon^2) \cos \varphi}{(1-\epsilon^2 \sin^2 \varphi)^2} d\varphi.$$

But

$$a^2(1-\epsilon^2) = b^2;$$

hence

$$S = b^2 \int_0^\varphi \frac{\cos \varphi d\varphi}{(1-\epsilon^2 \sin^2 \varphi)^2} = \frac{b^2}{4} \int_0^\varphi \frac{\cos \varphi d\varphi}{(1-\epsilon \sin \varphi)^2} + \frac{b^2}{4} \int_0^\varphi \frac{\cos \varphi d\varphi}{(1+\epsilon \sin \varphi)^2} + \frac{b^2}{4} \int_0^\varphi \frac{\cos \varphi d\varphi}{1+\epsilon \sin \varphi} - \frac{b^2}{4} \int_0^\varphi \frac{-\cos \varphi d\varphi}{1-\epsilon \sin \varphi}.$$

By integration this becomes

$$S = \frac{b^2}{4\epsilon} \left[ \frac{1}{1-\epsilon \sin \varphi} - \frac{1}{1+\epsilon \sin \varphi} + \log_e (1+\epsilon \sin \varphi) - \log_e (1-\epsilon \sin \varphi) \right],$$

or

$$S = b^2 \left[ \frac{\sin \varphi}{2(1-\epsilon^2 \sin^2 \varphi)} + \frac{1}{4\epsilon} \log_e \left( \frac{1+\epsilon \sin \varphi}{1-\epsilon \sin \varphi} \right) \right].$$

If  $c$  is the radius of the sphere with area equivalent to that of the spheroid, the area of a section of a lune of width  $d\lambda$  is equal to the value of the following integral multiplied by  $d\lambda$ :

$$S' = c^2 \int_0^\beta \cos \beta d\beta,$$

in which  $\beta$  is the latitude on the sphere.

By integration this gives

$$S' = c^2 \sin \beta.$$

If the  $d\lambda$  is taken the same in this case as in that of the spheroid,  $S'$  will equal  $S$  if  $\beta$  is defined by the equation

$$c^2 \sin \beta = b^2 \left[ \frac{\sin \varphi}{2(1 - \epsilon^2 \sin^2 \varphi)} + \frac{1}{4\epsilon} \log_e \left( \frac{1 + \epsilon \sin \varphi}{1 - \epsilon \sin \varphi} \right) \right].$$

If the right-hand member is developed in a series, it will be equal to the sum of the series of its two parts.

But we have

$$\frac{\sin \varphi}{2(1 - \epsilon^2 \sin^2 \varphi)} = \frac{1}{2} \sin \varphi + \frac{1}{2} \epsilon^2 \sin^3 \varphi + \frac{1}{2} \epsilon^4 \sin^5 \varphi + \frac{1}{2} \epsilon^6 \sin^7 \varphi + \dots$$

and

$$\begin{aligned} & \frac{1}{4\epsilon} [\log_e(1 + \epsilon \sin \varphi) - \log_e(1 - \epsilon \sin \varphi)] \\ &= \frac{1}{2} \sin \varphi + \frac{1}{3} \epsilon^2 \sin^3 \varphi + \frac{1}{10} \epsilon^4 \sin^5 \varphi + \frac{1}{14} \epsilon^6 \sin^7 \varphi + \dots \end{aligned}$$

Therefore

$$c^2 \sin \beta = b^2 \sin \varphi \left( 1 + \frac{2\epsilon^2}{3} \sin^2 \varphi + \frac{3\epsilon^4}{5} \sin^4 \varphi + \frac{4\epsilon^6}{7} \sin^6 \varphi + \dots \right)$$

We can determine the ratio of  $b^2$  to  $c^2$  by setting both  $\beta$  and  $\varphi$  equal to  $\frac{\pi}{2}$ , thus introducing the condition that the latitudes shall be equal for this value. This gives us the value

$$\frac{b^2}{c^2} = \frac{1}{1 + \frac{2\epsilon^2}{3} + \frac{3\epsilon^4}{5} + \frac{4\epsilon^6}{7} + \dots}$$

We have, then, as the definition of  $\beta$  the equation

$$\sin \beta = \sin \varphi \left( \frac{1 + \frac{2\epsilon^2}{3} \sin^2 \varphi + \frac{3\epsilon^4}{5} \sin^4 \varphi + \frac{4\epsilon^6}{7} \sin^6 \varphi + \dots}{1 + \frac{2\epsilon^2}{3} + \frac{3\epsilon^4}{5} + \frac{4\epsilon^6}{7} + \dots} \right).$$

The latitude defined in this manner has been called the *authalic latitude* to conform to Tissot's term for equivalent or equal-area projections used in his "Mémoire sur la Représentations des Surfaces."

In all projects of equivalent or equal-area mapping, if this latitude is used, the spheroid can be considered as the sphere of equivalent area. That is, the spheroid is first projected equivalently upon a sphere of equal surface and then this sphere is mapped upon the plane. The principle is similar to that employed in conformal mapping when the isometric latitude is employed. This simplifies the computations for Albers' equal-area projection or for the Lambert equal-area projections of any type. In all questions of spheroidal areas bounded by meridians and parallels, the computations can be made with any desired degree of exactness upon the authalic sphere.

#### RECAPITULATION OF DEFINITIONS.

As we have just shown in considering subjects connected with geodesy and cartography, there are five different kinds of latitude that have to be dealt with. A list of the symbols and definitions is given as follows:

1.  $\varphi$  = geodetic or astronomic latitude.
2.  $\psi$  = geocentric latitude.
3.  $\theta$  = reduced or parametric latitude.
4.  $\chi$  = isometric latitude.
5.  $\beta$  = authalic latitude.

The last four are defined in terms of the first as follows:

$$\tan \psi = (1 - \epsilon^2) \tan \varphi,$$

$$\tan \theta = (1 - \epsilon^2)^{1/2} \tan \varphi,$$

$$\tan \left( \frac{\pi}{4} + \frac{\chi}{2} \right) = \tan \left( \frac{\pi}{4} + \frac{\varphi}{2} \right) \cdot \left( \frac{1 - \epsilon \sin \varphi}{1 + \epsilon \sin \varphi} \right)^{\epsilon/2},$$

$$\sin \beta = \sin \varphi \left( \frac{1 + \frac{2\epsilon^2}{3} \sin^2 \varphi + \frac{3\epsilon^4}{5} \sin^4 \varphi + \frac{4\epsilon^6}{7} \sin^6 \varphi + \dots}{1 + \frac{2\epsilon^2}{3} + \frac{3\epsilon^4}{5} + \frac{4\epsilon^6}{7} + \dots} \right)$$

In the application of these latitudes it is generally desirable to have given the difference between  $\varphi$  and the various other latitudes. It is most convenient to have this difference expressed in terms of the sines of the multiple arcs. The problem is then to determine these series in the most satisfactory manner. In most cases this can be accomplished by the use of the principles of the functions of a complex variable. We will now proceed to apply this process wherever possible.

DEVELOPMENT OF  $\varphi - \psi$  IN TERMS OF  $\varphi$ .

We have

$$\tan (\varphi - \psi) = \frac{\tan \varphi - \tan \psi}{1 + \tan \varphi \tan \psi}$$

but

$$\tan \psi = (1 - e^2) \tan \varphi$$

hence

$$\begin{aligned} \tan (\varphi - \psi) &= \frac{e^2 \tan \varphi}{1 + (1 - e^2) \tan^2 \varphi} \\ &= \frac{e^2 \sin 2 \varphi}{2 - e^2 + e^2 \cos 2 \varphi}. \end{aligned}$$

Let

$$m = \frac{e^2}{2 - e^2},$$

then

$$\varphi - \psi = \tan^{-1} \left( \frac{m \sin 2 \varphi}{1 + m \cos 2 \varphi} \right).$$

Now,

$$\log_e (1 + m e^{2i\varphi}) = m e^{2i\varphi} - \frac{m^2}{2} e^{4i\varphi} + \frac{m^3}{3} e^{6i\varphi} - \dots;$$

but

$$\log_e (1 + m e^{2i\varphi}) = \frac{1}{2} \log_e (1 + 2 m \cos 2 \varphi + m^2)$$

$$+ i \tan^{-1} \left( \frac{m \sin 2 \varphi}{1 + m \cos 2 \varphi} \right),$$

and

$$\begin{aligned} m e^{2i\varphi} - \frac{m^2}{2} e^{4i\varphi} + \frac{m^3}{3} e^{6i\varphi} - \dots &= m \cos 2 \varphi + i m \sin 2 \varphi \\ - \frac{m^2}{2} \cos 4 \varphi - i \frac{m^2}{2} \sin 4 \varphi + \frac{m^3}{3} \cos 6 \varphi + i \frac{m^3}{3} \sin 6 \varphi - \dots \end{aligned}$$

Therefore, equating the imaginary parts, we obtain

$$\begin{aligned} \tan^{-1} \left( \frac{m \sin 2 \varphi}{1 + m \cos 2 \varphi} \right) &= m \sin 2 \varphi - \frac{m^2}{2} \sin 4 \varphi \\ &+ \frac{m^3}{3} \sin 6 \varphi - \dots; \end{aligned}$$

or, finally,

$$\varphi - \psi = m \sin 2 \varphi - \frac{m^2}{2} \sin 4 \varphi + \frac{m^3}{3} \sin 6 \varphi - \dots$$

DEVELOPMENT OF  $\varphi - \psi$  IN TERMS OF  $\psi$ .

If we wish this same quantity expressed in a series of the sines of the multiple arcs of  $\psi$ , we proceed as follows:

$$\begin{aligned}\tan \varphi &= \frac{1}{1 - \epsilon^2} \tan \psi, \\ \tan (\varphi - \psi) &= \frac{\epsilon^2 \tan \psi}{1 - \epsilon^2 + \tan^2 \psi} \\ &= \frac{\epsilon^2 \sin \psi \cos \psi}{1 - \epsilon^2 \cos^2 \psi} \\ &= \frac{\epsilon^2 \sin 2\psi}{2 - \epsilon^2 - \epsilon^2 \cos 2\psi} \\ &= \frac{m \sin 2\psi}{1 - m \cos 2\psi}\end{aligned}$$

Now

$$\log_e (1 - m e^{-2i\psi}) = -m e^{-2i\psi} - \frac{m^2}{2} e^{-4i\psi} - \frac{m^3}{3} e^{-6i\psi} - \dots;$$

but

$$\begin{aligned}\log_e (1 - m e^{-2i\psi}) &= \frac{1}{2} \log_e (1 - 2m \cos 2\psi + m^2) \\ &\quad + i \tan^{-1} \left( \frac{m \sin 2\psi}{1 - m \cos 2\psi} \right),\end{aligned}$$

and

$$\begin{aligned}-m e^{-2i\psi} - \frac{m^2}{2} e^{-4i\psi} - \frac{m^3}{3} e^{-6i\psi} - \dots &= -m \cos 2\psi + i m \sin 2\psi \\ -\frac{m^2}{2} \cos 4\psi + i \frac{m^2}{2} \sin 4\psi - \frac{m^3}{3} \cos 6\psi + i \frac{m^3}{3} \sin 6\psi - \dots\end{aligned}$$

By equating the imaginary parts, we obtain

$$\tan^{-1} \left( \frac{m \sin 2\psi}{1 - m \cos 2\psi} \right) = m \sin 2\psi + \frac{m^2}{2} \sin 4\psi + \frac{m^3}{3} \sin 6\psi + \dots,$$

or

$$\varphi - \psi = m \sin 2\psi + \frac{m^2}{2} \sin 4\psi + \frac{m^3}{3} \sin 6\psi + \dots$$

This result could have been obtained directly from the previous development by changing the sign of  $m$  and by interchanging  $\varphi$  and  $\psi$ .

DEVELOPMENT OF  $\varphi - \theta$  IN TERMS OF  $\varphi$ .

By substituting the definition of  $\theta$  in the formula for  $\tan(\varphi - \theta)$  we get

$$\begin{aligned}\tan(\varphi - \theta) &= \frac{[1 - (1 - \epsilon^2)^{\frac{1}{2}}] \tan \varphi}{1 + (1 - \epsilon^2)^{\frac{1}{2}} \tan^2 \varphi} \\ &= \frac{[1 - (1 - \epsilon^2)^{\frac{1}{2}}] \sin 2\varphi}{1 + (1 - \epsilon^2)^{\frac{1}{2}} + [1 - (1 - \epsilon^2)^{\frac{1}{2}}] \cos 2\varphi}.\end{aligned}$$

Now let

$$n = \frac{1 - (1 - \epsilon^2)^{\frac{1}{2}}}{1 + (1 - \epsilon^2)^{\frac{1}{2}}}$$

then

$$\tan(\varphi - \theta) = \frac{n \sin 2\varphi}{1 + n \cos 2\varphi}.$$

Since this expression is similar in form to that which gave  $\tan(\varphi - \psi)$  in terms of  $\varphi$ , except that we have  $n$  in place of  $m$ , by a similar procedure we get

$$\varphi - \theta = n \sin 2\varphi - \frac{n^2}{2} \sin 4\varphi + \frac{n^3}{3} \sin 6\varphi - \dots$$

DEVELOPMENT OF  $\varphi - \theta$  IN TERMS OF  $\theta$ .

When  $\tan(\varphi - \theta)$  is expressed in terms of  $\theta$ , we get

$$\tan(\varphi - \theta) = \frac{n \sin 2\theta}{1 - n \cos 2\theta}.$$

From the previous development we see that this gives  $\varphi - \theta$  in terms of  $\theta$  in the form

$$\varphi - \theta = n \sin 2\theta + \frac{n^2}{2} \sin 4\theta + \frac{n^3}{3} \sin 6\theta + \dots$$

DEVELOPMENT OF  $\theta - \psi$  IN TERMS OF  $\theta$  AND IN TERMS OF  $\psi$ .

From the original relations we get

$$\tan \psi = (1 - \epsilon^2)^{\frac{1}{2}} \tan \theta,$$



This relation is the same as that which exists between  $\theta$  and  $\varphi$ ; so we get at once

$$\theta - \psi = n \sin 2\theta - \frac{n^2}{2} \sin 4\theta + \frac{n^3}{3} \sin 6\theta - \dots$$

and

$$\theta - \psi = n \sin 2\psi + \frac{n^2}{2} \sin 4\psi + \frac{n^3}{3} \sin 6\psi + \dots$$

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\varphi$ —FIRST METHOD.

When we come to the isometric latitude, we meet difficulties of a different order. In the first place let  $p$  be the complement of  $\varphi$  and let  $z$  be the complement of  $\chi$ . The definition then becomes

$$\tan \frac{z}{2} = \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{1/2}.$$

Let

$$e^v = \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{1/2};$$

then

$$\tan \frac{z}{2} = e^v \tan \frac{p}{2}$$

$$\begin{aligned} \tan \left( \frac{z-p}{2} \right) &= \frac{(e^v - 1) \tan \frac{p}{2}}{1 + e^v \tan^2 \frac{p}{2}} \\ &= \frac{(e^v - 1) \sin p}{e^v + 1 - (e^v - 1) \cos p}. \end{aligned}$$

Let

$$q = \frac{e^v - 1}{e^v + 1};$$

then

$$\tan \left( \frac{z-p}{2} \right) = \frac{q \sin p}{1 - q \cos p}.$$

By analysis similar to that used before, we get

$$\frac{z-p}{2} = q \sin p + \frac{q^2}{2} \sin 2p + \frac{q^3}{3} \sin 3p + \dots;$$

but

$$\begin{aligned} v &= \frac{\epsilon}{2} \log_e (1 + \epsilon \cos p) - \frac{\epsilon}{2} \log_e (1 - \epsilon \cos p) \\ &= \epsilon^2 \cos p + \frac{\epsilon^4}{3} \cos^3 p + \frac{\epsilon^6}{5} \cos^5 p + \frac{\epsilon^8}{7} \cos^7 p + \dots \end{aligned}$$

and

$$q = \frac{e^v - 1}{e^v + 1} = \tanh \frac{v}{2} = \frac{v}{2} - \frac{v^3}{24} + \frac{v^5}{240} - \frac{17v^7}{40320} + \dots$$

Including terms in the eighth power of  $\epsilon$ , we get

$$q = \frac{\epsilon^2}{2} \cos p + \left( \frac{\epsilon^4}{6} - \frac{\epsilon^6}{24} \right) \cos^3 p + \left( \frac{\epsilon^6}{10} - \frac{\epsilon^8}{24} \right) \cos^5 p + \frac{\epsilon^8}{14} \cos^7 p +$$

Hence

$$\begin{aligned} z-p &= \left[ \epsilon^2 \cos p + \left( \frac{\epsilon^4}{3} - \frac{\epsilon^6}{12} \right) \cos^3 p + \left( \frac{\epsilon^6}{5} - \frac{\epsilon^8}{12} \right) \cos^5 p \right. \\ &\quad \left. + \frac{\epsilon^8}{7} \cos^7 p \right] \sin p + \left[ \frac{\epsilon^4}{4} \cos^3 p + \left( \frac{\epsilon^6}{6} - \frac{\epsilon^8}{24} \right) \cos^5 p \right. \\ &\quad \left. + \frac{23\epsilon^8}{180} \cos^7 p \right] \sin 2p + \frac{1}{3} \left( \frac{\epsilon^6}{4} \cos^3 p + \frac{\epsilon^8}{4} \cos^5 p \right) \sin 3p \\ &\quad + \frac{\epsilon^8}{32} \cos^4 p \sin 4p + \dots \end{aligned}$$

When this expression is reduced to terms in the sines of multiple arcs (see reduction table on p. 88), we get

$$\begin{aligned} z-p &= \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} + \dots \right) \sin 2p + \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} \right. \\ &\quad \left. + \frac{697\epsilon^8}{11520} + \dots \right) \sin 4p + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} + \dots \right) \sin 6p \\ &\quad + \left( \frac{1237\epsilon^8}{161280} + \dots \right) \sin 8p + \dots \end{aligned}$$

or in terms of  $\varphi$  and  $\chi$  to the desired approximation

$$\begin{aligned} \varphi - \chi &= \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ &\quad + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi. \end{aligned}$$

DEVELOPMENT OF  $\varphi - x$  IN TERMS OF  $\varphi$ —SECOND METHOD.

The isometric latitude can be developed in terms of  $\varphi$  by another method that is very simple in application. From the definition

$$\tan \frac{z}{2} = \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{\epsilon/2}$$

we obtain at once

$$\begin{aligned} \log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + \epsilon^2 \cos p + \frac{\epsilon^4}{3} \cos^3 p + \frac{\epsilon^6}{5} \cos^5 p \\ + \frac{\epsilon^8}{7} \cos^7 p + \dots \end{aligned}$$

By Taylor's theorem we have

$$\begin{aligned} f\left(\frac{p}{2} + h\right) = f\left(\frac{p}{2}\right) + \frac{h}{1!} \left[ \frac{df}{dh} \right] + \frac{h^2}{2!} \left[ \frac{d^2f}{dh^2} \right] + \frac{h^3}{3!} \left[ \frac{d^3f}{dh^3} \right] \\ + \frac{h^4}{4!} \left[ \frac{d^4f}{dh^4} \right] + \dots, \end{aligned}$$

in which the brackets denote the values of the derivatives of  $f\left(\frac{p}{2} + h\right)$  with respect to  $h$  for  $h = 0$ .

Let

$$f\left(\frac{p}{2} + h\right) = \log_e \tan \left(\frac{p}{2} + h\right).$$

Then

$$f\left(\frac{p}{2}\right) = \log_e \tan \frac{p}{2}$$

$$\frac{df}{dh} = \frac{\sec^2\left(\frac{p}{2} + h\right)}{\tan\left(\frac{p}{2} + h\right)} = \frac{1}{\sin\left(\frac{p}{2} + h\right) \cos\left(\frac{p}{2} + h\right)} = \frac{2}{\sin(p + 2h)}.$$

$$\left[ \frac{df}{dh} \right] = \frac{2}{\sin p}$$

$$\frac{d^2f}{dh^2} = -4 \operatorname{cosec}(p + 2h) \cot(p + 2h)$$

$$\left[ \frac{d^2f}{dh^2} \right] = -4 \operatorname{cosec} p \cot p = -\frac{4 \cos p}{\sin^2 p}$$

$$\frac{d^3f}{dh^3} = 8 \operatorname{cosec}(p + 2h) \cot^2(p + 2h) + 8 \operatorname{cosec}^3(p + 2h)$$

$$\left[ \frac{d^3 f}{dh^3} \right] = 8 \operatorname{cosec} p \cot^2 p + 8 \operatorname{cosec}^3 p = \frac{8 \cos^2 p}{\sin^3 p} + \frac{8}{\sin^3 p}$$

$$\begin{aligned} \frac{d^4 p}{dh^4} &= -16 \operatorname{cosec} (p+2h) \cot^3 (p+2h) \\ &\quad - 80 \operatorname{cosec}^3 (p+2h) \cot (p+2h) \end{aligned}$$

$$\begin{aligned} \left[ \frac{d^4 f}{dh^4} \right] &= -16 \operatorname{cosec} p \cot^3 p - 80 \operatorname{cosec}^3 p \cot p \\ &= -\frac{16 \cos^3 p}{\sin^4 p} - \frac{80 \cos p}{\sin^4 p}. \end{aligned}$$

Substituting these values in Taylor's series, we get

$$\begin{aligned} \log_e \tan \left( \frac{p}{2} + h \right) &= \log_e \tan \frac{p}{2} + \frac{2h}{\sin p} - \frac{2 \cos p}{\sin^3 p} h^2 \\ &+ \left( \frac{4 \cos^3 p}{3 \sin^3 p} + \frac{4}{3 \sin^3 p} \right) h^3 - \left( \frac{2 \cos^3 p}{3 \sin^4 p} + \frac{10 \cos p}{3 \sin^4 p} \right) h^4 + \dots \end{aligned}$$

Now let us assume the relation

$$\frac{z}{2} = \frac{p}{2} + a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8 + \dots,$$

then

$$h = a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8 + \dots$$

Substituting this value of  $h$  and retaining all powers of  $\epsilon$  up to and including the eighth, we obtain

$$\begin{aligned} \log_e \tan \left( \frac{p}{2} + h \right) &= \log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + \frac{z}{\sin p} (a\epsilon^2 \\ &+ b\epsilon^4 + c\epsilon^6 + d\epsilon^8) - \frac{2 \cos p}{\sin^3 p} (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8)^2 \\ &+ \left( \frac{4 \cos^3 p}{3 \sin^3 p} + \frac{4}{3 \sin^3 p} \right) (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8)^3 \\ &- \left( \frac{2 \cos^3 p}{3 \sin^4 p} + \frac{10 \cos p}{3 \sin^4 p} \right) (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8)^4 + \dots, \end{aligned}$$

or

$$\begin{aligned} \log_e \tan \frac{z}{2} &= \log_e \tan \frac{p}{2} + \frac{z}{\sin p} (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8) \\ &- \frac{2 \cos p}{\sin^3 p} [a^2\epsilon^4 + 2ab\epsilon^6 + (b^2 + 2ac)\epsilon^8] + \left( \frac{4 \cos^3 p}{3 \sin^3 p} \right. \\ &+ \left. \frac{4}{3 \sin^3 p} \right) (a^3\epsilon^6 + 3a^2b\epsilon^8) - \left( \frac{2 \cos^3 p}{3 \sin^4 p} \right. \\ &+ \left. \frac{10 \cos p}{3 \sin^4 p} \right) a^4\epsilon^8 + \dots \end{aligned}$$

But in the original series for  $\log_e \tan \frac{z}{2}$  we have

$$\log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + \epsilon^2 \cos p + \frac{\epsilon^4}{3} \cos^3 p + \frac{\epsilon^6}{5} \cos^5 p + \frac{\epsilon^8}{7} \cos^7 p + \dots$$

These two series must be identically equal and so we can equate the coefficients of the same powers of  $\epsilon$ . In this way we get

$$\frac{2a}{\sin p} = \cos p,$$

$$\frac{2b}{\sin p} - \frac{2a^2 \cos p}{\sin^2 p} = \frac{\cos^3 p}{3},$$

$$\frac{2c}{\sin p} - \frac{4ab \cos p}{\sin^2 p} + \frac{4a^3 \cos^2 p}{3 \sin^3 p} + \frac{4a^5}{3 \sin^3 p} = \frac{\cos^5 p}{5},$$

$$\begin{aligned} \frac{2d}{\sin p} - \frac{2(b^2 + 2ac) \cos p}{\sin^2 p} + \frac{4a^2 b \cos^2 p}{\sin^3 p} + \frac{4a^2 b}{\sin^3 p} - \frac{2a^4 \cos^3 p}{3 \sin^4 p} \\ - \frac{10a^4 \cos p}{3 \sin^4 p} = \frac{\cos^7 p}{7}. \end{aligned}$$

From these equations, we can in succession determine the values of  $a$ ,  $b$ ,  $c$ , and  $d$ .

(For the reductions see the reduction table p. 88.)

$$a = \frac{1}{2} \sin p \cos p = \frac{1}{4} \sin 2p,$$

$$b = \frac{5}{12} \sin p \cos^3 p = \frac{5}{48} \sin 2p + \frac{5}{96} \sin 4p,$$

$$\begin{aligned} c = \frac{13}{30} \sin p \cos^5 p - \frac{1}{12} \sin p \cos^3 p = \frac{3}{64} \sin 2p \\ + \frac{7}{160} \sin 4p + \frac{13}{960} \sin 6p, \end{aligned}$$

$$\begin{aligned} d = \frac{1237}{2520} \sin p \cos^7 p - \frac{3}{16} \sin p \cos^5 p = \frac{281}{11520} \sin 2p \\ + \frac{697}{23040} \sin 4p + \frac{461}{26880} \sin 6p + \frac{1237}{322560} \sin 8p. \end{aligned}$$

Substituting these values of  $a, b, c,$  and  $d$  and rearranging, we get to the desired approximation

$$z = p + \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2p + \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4p + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6p + \frac{1237\epsilon^8}{161280} \sin 8p.$$

Substitute

$$z = \frac{\pi}{2} - \chi \text{ and } p = \frac{\pi}{2} - \varphi,$$

and we get, as before, the approximation

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

**DEVELOPMENT OF  $\varphi - \chi$  IN TERMS OF  $\varphi$ —THIRD METHOD.**

The difference between  $\varphi$  and  $\chi$  can be developed directly by Maclaurin's theorem. Let us take the definition in the form

$$\log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + \epsilon^2 \cos p + \frac{\epsilon^4}{3} \cos^3 p + \frac{\epsilon^6}{5} \cos^5 p + \frac{\epsilon^8}{7} \cos^7 p + \dots$$

In this expression, setting  $\epsilon^2 = h$ , we get

$$\log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + h \cos p + \frac{h^2}{3} \cos^3 p + \frac{h^3}{5} \cos^5 p + \frac{h^4}{7} \cos^7 p + \dots$$

Differentiating this expression, considering  $z$  as a function of  $h$  or  $\epsilon^2$ , we get in succession

$$\operatorname{cosec} z \frac{dz}{dh} = \cos p + \frac{2h}{3} \cos^3 p + \frac{3h^2}{5} \cos^5 p + \frac{4h^3}{7} \cos^7 p,$$

$$\operatorname{cosec} z \frac{d^2 z}{dh^2} - \operatorname{cosec} z \cot z \left( \frac{dz}{dh} \right)^2 = \frac{2}{3} \cos^3 p + \frac{6h}{5} \cos^5 p + \frac{12h^2}{7} \cos^7 p,$$

$$\operatorname{cosec} z \frac{d^3 z}{dh^3} - 3 \operatorname{cosec} z \cot z \frac{dz}{dh} \frac{d^2 z}{dh^2} + \operatorname{cosec} z \cot^2 z \left( \frac{dz}{dh} \right)^2 \\ + \operatorname{cosec}^3 z \left( \frac{dz}{dh} \right)^3 = \frac{6}{5} \cos^5 p + \frac{24h}{7} \cos^7 p,$$

$$\operatorname{cosec} z \frac{d^4 z}{dh^4} - 4 \operatorname{cosec} z \cot z \frac{dz}{dh} \frac{d^3 z}{dh^3} - 3 \operatorname{cosec} z \cot z \left( \frac{d^2 z}{dh^2} \right)^2 \\ + 6 \operatorname{cosec} z \cot^2 z \left( \frac{dz}{dh} \right)^2 \frac{d^2 z}{dh^2} + 6 \operatorname{cosec}^3 z \left( \frac{dz}{dh} \right)^2 \frac{d^2 z}{dh^2} \\ - \operatorname{cosec} z \cot^3 z \left( \frac{dz}{dh} \right)^4 - 5 \operatorname{cosec}^3 z \cot z \left( \frac{dz}{dh} \right)^4 \\ = \frac{24}{7} \cos^7 p.$$

Denoting by brackets the values of these successive derivatives for  $h=0$ , remembering that functions of  $z$  become functions of  $p$  for  $h=0$ , we get. (For the necessary reductions see the reduction table, p. 88.)

$$[z] = p,$$

$$\left[ \frac{dz}{dh} \right] = \sin p \cos p = \frac{1}{2} \sin 2p,$$

$$\left[ \frac{d^2 z}{dh^2} \right] = \frac{5}{3} \sin p \cos^3 p = \frac{5}{12} \sin 2p + \frac{5}{24} \sin 4p,$$

$$\left[ \frac{d^3 z}{dh^3} \right] = -\sin p \cos^3 p + \frac{26}{5} \sin p \cos^5 p \\ = \frac{9}{16} \sin 2p + \frac{21}{40} \sin 4p + \frac{13}{80} \sin 6p,$$

$$\left[ \frac{d^4 z}{dh^4} \right] = -9 \sin p \cos^5 p + \frac{2474}{105} \sin p \cos^7 p \\ = \frac{281}{240} \sin 2p + \frac{697}{480} \sin 4p + \frac{461}{560} \sin 6p + \frac{1237}{8720} \sin 8p.$$

By Maclaurin's series we have

$$z = [z] + \frac{\epsilon^2}{1!} \left[ \frac{dz}{dh} \right] + \frac{\epsilon^4}{2!} \left[ \frac{d^2 z}{dh^2} \right] + \frac{\epsilon^6}{3!} \left[ \frac{d^3 z}{dh^3} \right] + \frac{\epsilon^8}{4!} \left[ \frac{d^4 z}{dh^4} \right] + \dots,$$

in which  $h$  is replaced by its value  $\epsilon^2$ .

By substituting the above values in this series and rearranging we get, as before, the approximation

$$z = p + \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2p + \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4p \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6p + \frac{1237\epsilon^8}{161280} \sin 8p,$$

or in  $\varphi$  and  $\chi$  we get, as before, the approximation

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

**DEVELOPMENT OF  $\varphi - \chi$  IN TERMS OF  $\varphi$ —FOURTH METHOD.**

The isometric latitude could be developed by direct differentiation of the equation in the form

$$\tan \frac{z}{2} = \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{\epsilon/2},$$

or in the form

$$z = 2 \tan^{-1} \left[ \tan \frac{p}{2} \cdot \left( \frac{1 + \epsilon \cos p}{1 - \epsilon \cos p} \right)^{\epsilon/2} \right].$$

In fact, Herz in his "Lehrbuch der Landkartenprojektionen" does differentiate the form

$$\frac{\pi}{2} + \chi = 2 \tan^{-1} \left[ \tan \left( \frac{\pi}{4} + \frac{\varphi}{2} \right) \cdot \left( \frac{1 - \epsilon \sin \varphi}{1 + \epsilon \sin \varphi} \right)^{\epsilon/2} \right].$$

He obtains the development to include the term in  $\epsilon^4$ . The difficulty lies in the fact that it is necessary to differentiate with respect to  $\epsilon$ , although it is evident that  $\chi$ , considered as a function of  $\epsilon$ , is an even function. If one wishes to proceed in this manner, it is better to write the expression in the form

$$z = 2 \tan^{-1} \left[ \tan \frac{p}{2} \cdot \exp^* \left( \epsilon^2 \cos p + \frac{\epsilon^4}{3} \cos^3 p + \frac{\epsilon^6}{5} \cos^5 p \right. \right. \\ \left. \left. + \frac{\epsilon^8}{7} \cos^7 p + \dots \right) \right],$$

---

\*  $\exp z = e^z$



or it is still better to develop the exponential to include all powers of  $\epsilon$  to the eighth inclusive.

$$z = 2 \tan^{-1} \left\{ \tan \frac{p}{2} \cdot \left[ 1 + \epsilon^2 \cos p + \epsilon^4 \left( \frac{\cos^2 p}{2} + \frac{\cos^3 p}{3} \right) + \epsilon^6 \left( \frac{\cos^3 p}{6} + \frac{\cos^4 p}{3} + \frac{\cos^5 p}{5} \right) + \epsilon^8 \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23 \cos^6 p}{90} + \frac{\cos^7 p}{7} \right) \right] \right\}.$$

In this form the substitution  $h = \epsilon^2$  can be made and the development attained by four differentiations instead of eight. Thus by careful consideration the formal work required can often be considerably reduced in amount. Using the expression as Herz did, it requires almost as much work to carry the development to  $\epsilon^4$  as it does in any of the above forms to carry it to include the term in  $\epsilon^8$ . It is also more convenient to differentiate the expression not as an arc tangent, but in the form  $\tan \frac{z}{2}$ . As an illustration we shall make the development by differentiating successively the expression

$$\tan \frac{z}{2} = \tan \frac{p}{2} \left[ 1 + h \cos p + h^2 \left( \frac{\cos^2 p}{2} + \frac{\cos^3 p}{3} \right) + h^3 \left( \frac{\cos^3 p}{6} + \frac{\cos^4 p}{3} + \frac{\cos^5 p}{5} \right) + h^4 \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23 \cos^6 p}{90} + \frac{\cos^7 p}{7} \right) \right].$$

$$\frac{1}{2} \sec^2 \frac{z}{2} \frac{dz}{dh} = \tan \frac{p}{2} \left[ \cos p + 2h \left( \frac{\cos^2 p}{2} + \frac{\cos^3 p}{3} \right) + 3h^2 \left( \frac{\cos^3 p}{6} + \frac{\cos^4 p}{3} + \frac{\cos^5 p}{5} \right) + 4h^3 \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23 \cos^6 p}{90} + \frac{\cos^7 p}{7} \right) \right],$$

$$\frac{1}{2} \sec^2 \frac{z}{2} \frac{d^2 z}{dh^2} + \frac{1}{2} \sec^2 \frac{z}{2} \tan \frac{z}{2} \left( \frac{dz}{dh} \right)^2 = \tan \frac{p}{2} \left[ \cos^2 p + \frac{2 \cos^3 p}{3} + 6h \left( \frac{\cos^3 p}{6} + \frac{\cos^4 p}{3} + \frac{\cos^5 p}{5} \right) + 12h^2 \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23 \cos^6 p}{90} + \frac{\cos^7 p}{7} \right) \right],$$

$$\begin{aligned} & \frac{1}{2} \sec^2 \frac{z}{2} \frac{d^2 z}{dh^2} + \frac{3}{2} \sec^2 \frac{z}{2} \tan \frac{z}{2} \frac{dz}{dh} \frac{d^2 z}{dh^2} + \left( \frac{1}{2} \sec^2 \frac{z}{2} \tan^2 \frac{z}{2} \right. \\ & \quad \left. + \frac{1}{4} \sec^4 \frac{z}{2} \right) \left( \frac{dz}{dh} \right)^2 = \tan \frac{p}{2} \left[ \cos^3 p + 2 \cos^4 p \right. \\ & \quad \left. + \frac{6 \cos^5 p}{5} + 24h \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23 \cos^6 p}{90} \right. \right. \\ & \quad \left. \left. + \frac{\cos^7 p}{7} \right) \right], \end{aligned}$$

$$\begin{aligned} & \frac{1}{2} \sec^2 \frac{z}{2} \frac{d^4 z}{dh^4} + \frac{3}{2} \sec^2 \frac{z}{2} \tan \frac{z}{2} \left( \frac{d^2 z}{dh^2} \right)^2 + 2 \sec^2 \frac{z}{2} \tan \frac{z}{2} \frac{dz}{dh} \frac{d^3 z}{dh^3} \\ & \quad + \left( 3 \sec^2 \frac{z}{2} \tan^2 \frac{z}{2} + \frac{3}{2} \sec^4 \frac{z}{2} \right) \left( \frac{dz}{dh} \right)^2 \frac{d^2 z}{dh^2} \\ & \quad + \left( \frac{1}{2} \sec^2 \frac{z}{2} \tan^3 \frac{z}{2} + \sec^4 \frac{z}{2} \tan \frac{z}{2} \right) \left( \frac{dz}{dh} \right)^4 \\ & \quad = \tan \frac{p}{2} \left( \cos^4 p + 4 \cos^5 p + \frac{92 \cos^6 p}{15} + \frac{24 \cos^7 p}{7} \right). \end{aligned}$$

Evaluating these derivatives for  $h=0$ , remembering that functions of  $z$  become functions of  $p$  for  $h=0$ , we obtain (for the necessary reductions see the reduction table, p. 88):

$$[z] = p,$$

$$\left[ \frac{dz}{dh} \right] = \sin p \cos p = \frac{1}{2} \sin 2p,$$

$$\left[ \frac{d^2 z}{dh^2} \right] = \frac{5}{3} \sin p \cos^3 p = \frac{5}{12} \sin 2p + \frac{5}{24} \sin 4p,$$

$$\begin{aligned} \left[ \frac{d^3 z}{dh^3} \right] &= -\sin p \cos^5 p + \frac{26}{5} \sin p \cos^3 p \\ &= \frac{9}{16} \sin 2p + \frac{21}{40} \sin 4p + \frac{13}{80} \sin 6p, \end{aligned}$$

$$\begin{aligned} \left[ \frac{d^4 z}{dh^4} \right] &= -9 \sin p \cos^7 p + \frac{2474}{105} \sin p \cos^5 p \\ &= \frac{281}{240} \sin 2p + \frac{697}{480} \sin 4p + \frac{461}{560} \sin 6p + \frac{1237}{6720} \sin 8p. \end{aligned}$$

Substituting these values in Maclaurin's series (see p. 22), we get, as before, the approximation:

$$z = p + \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2p + \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4p \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6p + \frac{1237\epsilon^8}{161280} \sin 8p,$$

or, in terms of  $\varphi$  and  $\chi$ , the approximation,

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\varphi$ —FIFTH METHOD.

This difference can be expressed first in terms of  $\varphi$  directly from the equation of definition by the third, fourth, fifth, or sixth method given later under those developments (see pp. 38-55), and then the development can be inverted into terms of  $\varphi$  by Lagrange's theorem. We start with the approximation:

$$\chi = \varphi - \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi - \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ - \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi - \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

In this case Lagrange's series becomes:

$$\chi = \varphi + \frac{1}{1!} g(\varphi) + \frac{1}{2!} \frac{d}{d\varphi} [g(\varphi)]^2 + \frac{1}{3!} \frac{d^2}{d\varphi^2} [g(\varphi)]^3 \\ + \frac{1}{4!} \frac{d^3}{d\varphi^3} [g(\varphi)]^4 + \dots,$$

in which

$$g(\varphi) = - \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\varphi - \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\varphi \\ - \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\varphi - \frac{4279\epsilon^8}{161280} \sin 8\varphi.$$

In the powers of this function we must retain all powers of  $\epsilon$  to the eighth, inclusive.

$$[g(\varphi)]^2 = \left( \frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24} + \frac{73\epsilon^8}{576} \right) \sin^2 2\varphi + \frac{49\epsilon^8}{2304} \sin^2 4\varphi + \left( \frac{7\epsilon^6}{48} + \frac{523\epsilon^8}{2880} \right) \sin 2\varphi \sin 4\varphi + \frac{7\epsilon^8}{120} \sin 2\varphi \sin 6\varphi$$

$$[g(\varphi)]^3 = - \left( \frac{\epsilon^6}{8} + \frac{5\epsilon^8}{32} \right) \sin^2 2\varphi - \frac{7\epsilon^8}{64} \sin^2 2\varphi \sin 4\varphi$$

$$[g(\varphi)]^4 = \frac{\epsilon^8}{16} \sin^4 2\varphi.$$

Differentiating and reducing by the table on p. 88, we get

$$\begin{aligned} \frac{d}{d\varphi} [g(\varphi)]^2 &= \left( \epsilon^4 + \frac{5\epsilon^6}{6} + \frac{73\epsilon^8}{144} \right) \sin 2\varphi \cos 2\varphi + \frac{49\epsilon^8}{288} \sin 4\varphi \cos 4\varphi \\ &\quad + \left( \frac{7\epsilon^6}{24} + \frac{523\epsilon^8}{1440} \right) \cos 2\varphi \sin 4\varphi \\ &\quad + \left( \frac{7\epsilon^6}{12} + \frac{523\epsilon^8}{720} \right) \sin 2\varphi \cos 4\varphi + \frac{7\epsilon^8}{60} \cos 2\varphi \sin 6\varphi \\ &\quad + \frac{7\epsilon^8}{20} \sin 2\varphi \cos 6\varphi \end{aligned}$$

$$\begin{aligned} &= - \left( \frac{7\epsilon^6}{48} + \frac{523\epsilon^8}{2880} \right) \sin 2\varphi + \left( \frac{\epsilon^4}{2} + \frac{5\epsilon^6}{12} + \frac{197\epsilon^8}{1440} \right) \sin 4\varphi \\ &\quad + \left( \frac{7\epsilon^6}{16} + \frac{523\epsilon^8}{960} \right) \sin 6\varphi + \frac{917\epsilon^8}{2880} \sin 8\varphi, \end{aligned}$$

$$\begin{aligned} \frac{d^2}{d\varphi^2} [g(\varphi)]^3 &= - \left( 3\epsilon^6 + \frac{15\epsilon^8}{4} \right) \sin 2\varphi \cos^2 2\varphi + \left( \frac{3\epsilon^6}{2} + \frac{15\epsilon^8}{8} \right) \sin^3 2\varphi \\ &\quad - \frac{21\epsilon^8}{16} \sin 8\varphi + \frac{7\epsilon^8}{4} \sin^2 2\varphi \sin 4\varphi \\ &= \left( \frac{3\epsilon^6}{8} + \frac{15\epsilon^8}{32} \right) \sin 2\varphi + \frac{7\epsilon^8}{8} \sin 4\varphi - \left( \frac{9\epsilon^6}{8} + \frac{45\epsilon^8}{32} \right) \sin 6\varphi \\ &\quad - \frac{7\epsilon^8}{4} \sin 8\varphi, \end{aligned}$$

$$\frac{d^3}{d\varphi^3} [g(\varphi)]^4 = -2\epsilon^8 \sin 4\varphi + 4\epsilon^8 \sin 8\varphi.$$

Substituting these values in Lagrange's series, we get the approximation

$$\begin{aligned} x = \varphi - & \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\varphi - \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\varphi \\ & - \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\varphi - \frac{4279\epsilon^8}{161280} \sin 8\varphi \\ & - \left( \frac{7\epsilon^6}{96} + \frac{523\epsilon^8}{5760} \right) \sin 2\varphi + \left( \frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24} + \frac{197\epsilon^8}{2880} \right) \sin 4\varphi + \left( \frac{7\epsilon^6}{32} \right. \\ & \left. + \frac{523\epsilon^8}{1920} \right) \sin 6\varphi + \frac{917\epsilon^8}{5760} \sin 8\varphi + \left( \frac{\epsilon^6}{16} + \frac{5\epsilon^8}{64} \right) \sin 2\varphi \\ & + \frac{7\epsilon^8}{48} \sin 4\varphi - \left( \frac{3\epsilon^6}{16} + \frac{15\epsilon^8}{64} \right) \sin 6\varphi - \frac{7\epsilon^8}{24} \sin 8\varphi \\ & - \frac{\epsilon^8}{12} \sin 4\varphi + \frac{\epsilon^8}{6} \sin 8\varphi. \end{aligned}$$

By collecting and rearranging we get, as before, the approximation

$$\begin{aligned} \varphi - x = & \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ & + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi. \end{aligned}$$

#### DEVELOPMENT OF $\varphi - x$ IN TERMS OF $\varphi$ —SIXTH METHOD.

$\varphi - x$  can be developed in terms of  $\varphi$  by Arbogast's rule. If the symbol  $f$  denotes an arbitrary analytic function, we can expand

$$f\left(a_0 + a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots\right)$$

in terms of  $x$  at once by Taylor's theorem in the form

$$\begin{aligned} f\left(a_0 + a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots\right) = & f(a_0) \\ & + \frac{1}{1!} f'(a_0) \left( a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \right) \\ & + \frac{1}{2!} f''(a_0) \left( a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \right)^2 \\ & + \frac{1}{3!} f'''(a_0) \left( a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \right)^3 \\ & + \frac{1}{4!} f^{(4)}(a_0) \left( a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \right)^4 + \dots \end{aligned}$$

The exponents of  $f$  denote the values of the various successive derivatives of  $f(a_0 + g)$  with respect to  $g$  for  $g=0$ , or, what amounts to the same thing, the values of the various successive derivatives of  $f(a_0)$  with respect to  $a_0$ . By expanding the various powers of the polynomial in  $x$  in the above expression and by rearranging in powers of  $x$ , we may determine the coefficients of the various  $\frac{x^n}{n!}$  in the expansion in a series of terms of  $x$ . A more expeditious way of determining these coefficients is devised in the following manner:

Let us define a partial differential operator in the form

$$\Delta = a_1 \frac{\partial}{\partial a_0} + a_2 \frac{\partial}{\partial a_1} + a_3 \frac{\partial}{\partial a_2} + a_4 \frac{\partial}{\partial a_3} + \dots ;$$

then

$$\begin{aligned} \Delta f \left( a_0 + a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} + a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \right) &= \left( a_1 + a_2 \frac{x}{1!} \right. \\ &+ a_3 \frac{x^2}{2!} + a_4 \frac{x^3}{3!} + a_5 \frac{x^4}{4!} + \dots \left. \right) f' \left( a_0 + a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} \right. \\ &+ a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \left. \right) = \frac{d}{dx} f \left( a_0 + a_1 \frac{x}{1!} + a_2 \frac{x^2}{2!} \right. \\ &+ a_3 \frac{x^3}{3!} + a_4 \frac{x^4}{4!} + \dots \left. \right). \end{aligned}$$

Therefore, if  $A_n$  denotes the  $n$ th coefficient in the expansion of the given function, we have

$$\begin{aligned} \Delta A_0 + \Delta A_1 \frac{x}{1!} + \Delta A_2 \frac{x^2}{2!} + \Delta A_3 \frac{x^3}{3!} + \Delta A_4 \frac{x^4}{4!} + \dots \\ = A_1 + A_2 \frac{x}{1!} + A_3 \frac{x^2}{2!} + A_4 \frac{x^3}{3!} + A_5 \frac{x^4}{4!} + \dots \end{aligned}$$

Equating the coefficients of the like powers of  $x$  in this identity, we obtain the recurrence formula

$$A_{n+1} = \Delta A_n.$$

Now in the Taylor development we see that

$$A_0 = f(a_0).$$

By applying the recurrence formula in succession, we may write down the coefficients,

$$A_1 = a_1 f^1(a_0),$$

$$A_2 = a_1^2 f^2(a_0) + a_2 f^1(a_0),$$

$$A_3 = a_1^3 f^3(a_0) + 3a_1 a_2 f^2(a_0) + a_3 f^1(a_0),$$

$$A_4 = a_1^4 f^4(a_0) + 6a_1^2 a_2 f^3(a_0) + 4a_1 a_3 f^2(a_0) + 3a_2^2 f^2(a_0) + a_4 f^1(a_0),$$

etc.

We shall now apply these principles in the development of the function

$$z = 2 \tan^{-1} \exp^* \left( \log_e \tan \frac{p}{2} + \frac{h}{1!} \cos p + \frac{h^2}{2!} \frac{2}{3} \cos^3 p + \frac{h^3}{3!} \frac{6}{5} \cos^5 p + \frac{h^4}{4!} \frac{24}{7} \cos^7 p + \dots \right) = A_0 + A_1 \frac{h}{1!} + A_2 \frac{h^2}{2!} + A_3 \frac{h^3}{3!} + A_4 \frac{h^4}{4!} + \dots,$$

in which  $h = e^2$ .

In this case

$$a_0 = \log_e \tan \frac{p}{2},$$

$$\frac{da_0}{dp} = \frac{\sec^2 \frac{p}{2}}{2 \tan \frac{p}{2}} = \frac{1}{\sin p},$$

or

$$\frac{dp}{da_0} = \sin p,$$

$$f(a_0) = 2 \tan^{-1} e^{a_0} = p,$$

$$f^1(a_0) = \frac{dp}{da_0} = \sin p,$$

$$f^2(a_0) = \cos p \frac{dp}{da_0} = \sin p \cos p = \frac{1}{2} \sin 2p,$$

$$f^3(a_0) = \cos 2p \frac{dp}{da_0} = \sin p \cos 2p = \frac{1}{2} \sin 3p - \frac{1}{2} \sin p,$$

$$f^4(a_0) = \left( \frac{3}{2} \cos 3p - \frac{1}{2} \cos p \right) \frac{dp}{da_0} = \left( \frac{3}{2} \cos 3p - \frac{1}{2} \cos p \right) \sin p = \frac{3}{4} \sin 4p - \sin 2p.$$

---

\*  $\exp x = e^x$

In the function to be expanded, we are given

$$a_0 = \log_e \tan \frac{p}{2},$$

$$a_1 = \cos p,$$

$$a_2 = \frac{2}{3} \cos^3 p,$$

$$a_3 = \frac{6}{5} \cos^5 p,$$

$$a_4 = \frac{24}{7} \cos^7 p.$$

With these values we may compute the various  $A_n$  and reduce them by aid of the reduction table on page 88.

$$A_0 = p,$$

$$A_1 = \sin p \cos p = \frac{1}{2} \sin 2p,$$

$$\begin{aligned} A_2 &= \frac{1}{2} \cos^2 p \sin 2p + \frac{2}{3} \cos^3 p \sin p = \frac{5}{3} \sin p \cos^3 p \\ &= \frac{5}{12} \sin 2p + \frac{5}{24} \sin 4p, \end{aligned}$$

$$\begin{aligned} A_3 &= \cos^3 p \left( \frac{1}{2} \sin 3p - \frac{1}{2} \sin p \right) + \cos^4 p \sin 2p + \frac{6}{5} \cos^5 p \sin p \\ &= -\sin p \cos^3 p + \frac{26}{5} \sin p \cos^5 p \\ &= \frac{9}{16} \sin 2p + \frac{21}{40} \sin 4p + \frac{13}{80} \sin 6p, \end{aligned}$$

$$\begin{aligned} A_4 &= \cos^4 p \left( \frac{3}{4} \sin 4p - \sin 2p \right) + 4 \cos^5 p \sin p \cos 2p \\ &\quad + \frac{24}{5} \cos^6 p \sin p \cos p + \frac{4}{3} \cos^6 p \sin p \cos p \\ &\quad + \frac{24}{7} \cos^7 p \sin p = -9 \sin p \cos^5 p + \frac{2474}{105} \sin p \cos^7 p \\ &= \frac{281}{240} \sin 2p + \frac{697}{480} \sin 4p + \frac{461}{560} \sin 6p + \frac{1237}{6720} \sin 8p \end{aligned}$$



Substituting these values in the expansion and remembering that  $h = \epsilon^2$ , we get, after rearrangement as the desired approximation,

$$z = p + \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2p + \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4p \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6p + \frac{1237\epsilon^8}{161280} \sin 8p,$$

or, in terms of  $\varphi$  and  $\chi$ , we get, as before, the approximation:

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\chi$ —FIRST METHOD.

The quantity  $\varphi - \chi$  can be expressed in terms of  $\chi$  by the application of Lagrange's series. We have given

$$\varphi = \chi + f(\varphi).$$

Since  $f(\varphi)$  is a small quantity, Lagrange's series becomes

$$\varphi = \chi + \frac{1}{1!} f(\chi) + \frac{1}{2!} \frac{d}{d\chi} [f(\chi)]^2 + \frac{1}{3!} \frac{d^2}{d\chi^2} [f(\chi)]^3 \\ + \frac{1}{4!} \frac{d^3}{d\chi^3} [f(\chi)]^4 + \dots$$

But in the series for  $\varphi - \chi$  given above, we see that

$$f(\varphi) = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

Squaring this expression and reducing by aid of the table on p. 88, we get

$$[f(\varphi)]^2 = \frac{\epsilon^4}{8} + \frac{5\epsilon^6}{48} + \frac{341\epsilon^8}{4608} - \left( \frac{5\epsilon^6}{96} + \frac{377\epsilon^8}{5760} \right) \cos 2\varphi - \left( \frac{\epsilon^4}{8} + \frac{5\epsilon^6}{48} \right. \\ \left. + \frac{317\epsilon^8}{5760} \right) \cos 4\varphi + \left( \frac{5\epsilon^6}{96} + \frac{377\epsilon^8}{5760} \right) \cos 6\varphi - \frac{437\epsilon^8}{23040} \cos 8\varphi,$$

and, by cubing and reducing, we get

$$[f(\varphi)]^3 = \left(\frac{3\epsilon^6}{32} + \frac{15\epsilon^8}{128}\right) \sin 2\varphi - \frac{5\epsilon^8}{128} \sin 4\varphi - \left(\frac{\epsilon^6}{32} + \frac{5\epsilon^8}{128}\right) \sin 6\varphi \\ + \frac{5\epsilon^8}{256} \sin 8\varphi,$$

and for the fourth power, by a similar process, we obtain

$$[f(\varphi)]^4 = \frac{3\epsilon^8}{128} - \frac{\epsilon^8}{32} \cos 4\varphi + \frac{\epsilon^8}{128} \cos 8\varphi.$$

$$\frac{d}{d\chi} [f(x)]^3 = \left(\frac{5\epsilon^6}{48} + \frac{377\epsilon^8}{2880}\right) \sin 2\chi + \left(\frac{\epsilon^4}{2} + \frac{5\epsilon^6}{12} + \frac{317\epsilon^8}{1440}\right) \sin 4\chi \\ - \left(\frac{5\epsilon^6}{16} + \frac{377\epsilon^8}{960}\right) \sin 6\chi + \frac{437\epsilon^8}{2880} \sin 8\chi,$$

$$\frac{d^2}{d\chi^2} [f(x)]^3 = -\left(\frac{3\epsilon^6}{8} + \frac{15\epsilon^8}{32}\right) \sin 2\chi + \frac{5\epsilon^8}{8} \sin 4\chi \\ + \left(\frac{9\epsilon^6}{8} + \frac{45\epsilon^8}{32}\right) \sin 6\chi - \frac{5\epsilon^8}{4} \sin 8\chi,$$

$$\frac{d^3}{d\chi^3} [f(x)]^4 = -2\epsilon^8 \sin 4\chi + 4\epsilon^8 \sin 8\chi.$$

Substituting these values in Lagrange's series, we get the approximation

$$\varphi - \chi = \left(\frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760}\right) \sin 2\chi - \left(\frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520}\right) \sin 4\chi \\ + \left(\frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440}\right) \sin 6\chi - \frac{1237\epsilon^8}{161280} \sin 8\chi \\ + \left(\frac{5\epsilon^6}{96} + \frac{377\epsilon^8}{5760}\right) \sin 2\chi + \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24} + \frac{317\epsilon^8}{2880}\right) \sin 4\chi \\ - \left(\frac{5\epsilon^6}{32} + \frac{377\epsilon^8}{1920}\right) \sin 6\chi + \frac{437\epsilon^8}{5760} \sin 8\chi - \left(\frac{\epsilon^6}{16} + \frac{5\epsilon^8}{64}\right) \sin 2\chi \\ + \frac{5\epsilon^8}{48} \sin 4\chi + \left(\frac{3\epsilon^6}{16} + \frac{15\epsilon^8}{64}\right) \sin 6\chi - \frac{5\epsilon^8}{24} \sin 8\chi \\ - \frac{\epsilon^8}{12} \sin 4\chi + \frac{\epsilon^8}{6} \sin 8\chi.$$

When similar terms are collected, this approximation becomes

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\chi$ —SECOND METHOD

The series for  $\varphi - \chi$  in terms of  $\varphi$  can be expressed in terms of the second argument by the method of successive approximations. In the series for  $\varphi - \chi$ , let

$$\varphi = \chi + a.$$

Then  $a$  will be equal to a small quantity since we have (see above)

$$a = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} \right) \sin 4\varphi \\ + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right) \sin 6\varphi - \frac{1237\epsilon^8}{161280} \sin 8\varphi.$$

In the series for  $\varphi - \chi$ ,  $\varphi$  must first be replaced by  $\chi + a$ , and this developed far enough to include terms in  $\epsilon^8$ . The value of  $a$  is then substituted, and this introduces terms in  $\varphi$  again. These terms are then developed in  $\chi$  and  $a$ , and the process repeated until all terms in  $\epsilon^8$  have been included. To shorten the work assume

$$\varphi = \chi + A \sin 2\varphi - B \sin 4\varphi + C \sin 6\varphi - D \sin 8\varphi.$$

Then the lowest power of  $\epsilon$  in  $A$  is  $\epsilon^2$ ; in  $B$  is  $\epsilon^4$ ; in  $C$  is  $\epsilon^6$ ; and in  $D$  is  $\epsilon^8$ .

(For the necessary reductions see the reduction table, p. 88.)

Substitute for  $\varphi$  in the above series  $\chi + a$  and we have

$$\varphi = \chi + A \sin (2\chi + 2a) - B \sin (4\chi + 4a) + C \sin (6\chi + 6a) \\ - D \sin (8\chi + 8a),$$

or

$$\varphi = \chi + A \sin 2\chi \cos 2a + A \cos 2\chi \sin 2a - B \sin 4\chi \cos 4a \\ - B \cos 4\chi \sin 4a + C \sin 6\chi \cos 6a + C \cos 6\chi \sin 6a \\ - D \sin 8\chi \cos 8a - D \cos 8\chi \sin 8a.$$

Developing the functions in  $a$  far enough to include all terms in  $\epsilon^8$ , we get

$$\begin{aligned}\varphi = & \chi + A \left(1 - \frac{4a^2}{2}\right) \sin 2\chi + A \left(2a - \frac{8a^3}{6}\right) \cos 2\chi \\ & - B \left(1 - \frac{16a^2}{2}\right) \sin 4\chi - B 4a \cos 4\chi + C \sin 6\chi \\ & + C 6a \cos 6\chi - D \sin 8\chi.\end{aligned}$$

These coefficients must now be evaluated and second and third approximations applied wherever necessary to get the required exactness.

$$\begin{aligned}A(1-2a^2) &= A \left[1 - 2 \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24}\right) \sin^2 2\varphi + \frac{5\epsilon^6}{24} \sin 2\varphi \sin 4\varphi\right] \\ &= A \left[1 - \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24}\right) + \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24}\right) \cos 4\varphi\right. \\ &\quad \left.+ \frac{5\epsilon^6}{24} \sin 2\chi \sin 4\chi\right]\end{aligned}$$

In this expression, since the lowest power of  $\epsilon$  in  $A$  is  $\epsilon^2$ , we do not have to carry the development farther than to include terms in  $\epsilon^6$ .

But

$$\cos 4\varphi = \cos(4\chi + 4a) = \cos 4\chi \cos 4a - \sin 4\chi \sin 4a.$$

No term beyond  $\epsilon^2$  is needed in this approximation. Hence for the exactness required

$$\cos 4\varphi = \cos 4\chi - 2\epsilon^2 \sin 2\chi \sin 4\chi.$$

Therefore

$$\begin{aligned}A(1-2a^2) &= A \left[1 - \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24}\right) + \left(\frac{\epsilon^4}{4} + \frac{5\epsilon^6}{24}\right) \cos 4\chi\right. \\ &\quad \left.- \frac{\epsilon^6}{2} \sin 2\chi \sin 4\chi + \frac{5\epsilon^6}{24} \sin 2\chi \sin 4\chi\right].\end{aligned}$$

On multiplying the two factors and reducing to a series of cosines of the multiple arcs, we get

$$\begin{aligned}A(1-2a^2) &= \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} - \frac{\epsilon^6}{32} - \frac{619\epsilon^8}{5760} - \frac{7\epsilon^8}{96} \cos 2\chi \\ &\quad + \left(\frac{\epsilon^6}{8} + \frac{5\epsilon^8}{32}\right) \cos 4\chi + \frac{7\epsilon^8}{96} \cos 6\chi\end{aligned}$$

By a similar procedure, we get

$$A \left( 2a - \frac{4a^3}{3} \right) = A \left[ \left( \epsilon^2 + \frac{5\epsilon^4}{12} + \frac{3\epsilon^6}{16} \right) \sin 2\varphi - \left( \frac{5\epsilon^4}{24} + \frac{7\epsilon^6}{40} \right) \sin 4\varphi \right. \\ \left. + \frac{13\epsilon^6}{240} \sin 6\varphi - \frac{4}{3} \left( \frac{\epsilon^6}{8} \right) \sin^3 2\varphi \right],$$

or

$$A \left( 2a - \frac{4a^3}{3} \right) = A \left[ \left( \epsilon^2 + \frac{5\epsilon^4}{12} + \frac{3\epsilon^6}{16} \right) (\sin 2\chi \cos 2a \right. \\ \left. + \cos 2\chi \sin 2a) - \left( \frac{5\epsilon^4}{24} + \frac{7\epsilon^6}{40} \right) (\sin 4\chi \cos 4a \right. \\ \left. + \cos 4\chi \sin 4a) + \frac{13\epsilon^6}{240} \sin 6\chi - \frac{\epsilon^6}{6} \sin^3 2\chi \right],$$

$$A \left( 2a - \frac{4a^3}{3} \right) = A \left[ \left( \epsilon^2 + \frac{5\epsilon^4}{12} + \frac{3\epsilon^6}{16} \right) \left( 1 - \frac{4a^2}{2} \right) \sin 2\chi \right. \\ \left. + 2a \left( \epsilon^2 + \frac{5\epsilon^4}{12} \right) \cos 2\chi - \left( \frac{5\epsilon^4}{24} + \frac{7\epsilon^6}{40} \right) \sin 4\chi \right. \\ \left. - 4a \left( \frac{5\epsilon^4}{24} \right) \cos 4\chi + \frac{13\epsilon^6}{240} \sin 6\chi - \frac{\epsilon^6}{6} \sin^3 2\chi \right],$$

$$A \left( 2a - \frac{4a^3}{3} \right) = A \left[ \left( \epsilon^2 + \frac{5\epsilon^4}{12} + \frac{3\epsilon^6}{16} \right) \sin 2\chi - \frac{\epsilon^6}{2} \sin^3 2\chi \right. \\ \left. + \left( \epsilon^4 + \frac{5\epsilon^6}{6} \right) \sin 2\varphi \cos 2\chi - \frac{5\epsilon^6}{24} \sin 4\chi \cos 2\chi \right. \\ \left. - \left( \frac{5\epsilon^4}{24} + \frac{7\epsilon^6}{40} \right) \sin 4\chi - \frac{5\epsilon^6}{12} \sin 2\chi \cos 4\chi \right. \\ \left. + \frac{13\epsilon^6}{240} \sin 6\chi - \frac{\epsilon^6}{6} \sin^3 2\chi \right].$$

Finally, on developing  $\sin 2\varphi$  in the above expression, we get

$$A \left( 2a - \frac{4a^3}{3} \right) = A \left[ \left( \epsilon^2 + \frac{5\epsilon^4}{12} + \frac{3\epsilon^6}{16} \right) \sin 2\chi - \frac{\epsilon^6}{2} \sin^3 2\chi \right. \\ \left. + \left( \epsilon^4 + \frac{5\epsilon^6}{6} \right) \sin 2\chi \cos 2\chi + \epsilon^6 \sin 2\chi \cos^3 2\chi \right. \\ \left. - \frac{5\epsilon^6}{24} \sin 4\chi \cos 2\chi - \left( \frac{5\epsilon^4}{24} + \frac{7\epsilon^6}{40} \right) \sin 4\chi - \frac{5\epsilon^6}{12} \sin 2\chi \cos 4\chi \right. \\ \left. + \frac{13\epsilon^6}{240} \sin 6\chi - \frac{\epsilon^6}{6} \sin^3 2\chi \right],$$

$$\begin{aligned}
 A\left(2a - \frac{4a^3}{3}\right) &= \left(\frac{\epsilon^4}{2} + \frac{5\epsilon^6}{12} + \frac{79\epsilon^8}{288}\right) \sin 2\chi - \frac{\epsilon^8}{4} \sin^3 2\chi \\
 &+ \left(\frac{\epsilon^6}{2} + \frac{5\epsilon^8}{8}\right) \sin 2\chi \cos 2\chi + \frac{\epsilon^8}{2} \sin 2\chi \cos^2 2\chi \\
 &- \frac{5\epsilon^8}{48} \sin 4\chi \cos 2\chi - \left(\frac{5\epsilon^8}{48} + \frac{377\epsilon^8}{2880}\right) \sin 4\chi \\
 &- \frac{5\epsilon^8}{24} \sin 2\chi \cos 4\chi + \frac{13\epsilon^8}{480} \sin 6\chi - \frac{\epsilon^8}{12} \sin^3 2\chi.
 \end{aligned}$$

Reducing this to a series in the sines of multiple arcs by aid of the reduction table on p. 88, we obtain

$$\begin{aligned}
 A\left(2a - \frac{4a^3}{3}\right) &= \left(\frac{\epsilon^4}{2} + \frac{5\epsilon^6}{12} + \frac{29\epsilon^8}{144}\right) \sin 2\chi + \left(\frac{7\epsilon^6}{48} + \frac{523\epsilon^8}{2880}\right) \sin 4\chi \\
 &+ \frac{19\epsilon^8}{240} \sin 6\chi.
 \end{aligned}$$

$$B(1 - 8a^2) = B(1 - 2\epsilon^4 \sin^2 2\chi) = \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} - \frac{503\epsilon^8}{11520} + \frac{5\epsilon^8}{48} \cos 4\chi.$$

$$\begin{aligned}
 4Ba &= 4B \left[ \left(\frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24}\right) \sin 2\varphi - \frac{5\epsilon^4}{48} \sin 4\chi \right] \\
 &= 4B \left[ \left(\frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24}\right) \sin 2\chi + \frac{\epsilon^4}{2} \sin 2\chi \cos 2\chi - \frac{5\epsilon^4}{48} \sin 4\chi \right] \\
 &= \left(\frac{5\epsilon^8}{24} + \frac{377\epsilon^8}{1440}\right) \sin 2\chi + \frac{35\epsilon^8}{576} \sin 4\chi.
 \end{aligned}$$

$$6Ca = 3C\epsilon^2 \sin 2\chi = \frac{13\epsilon^8}{160} \sin 2\chi.$$

On substituting these values in the original expression, we get the approximation

$$\begin{aligned}
 \varphi - \chi &= \left(\frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} - \frac{\epsilon^6}{32} - \frac{619\epsilon^8}{5760}\right) \sin 2\chi - \frac{7\epsilon^8}{96} \sin 2\chi \cos 2\chi \\
 &+ \left(\frac{\epsilon^6}{8} + \frac{5\epsilon^8}{32}\right) \sin 2\chi \cos 4\chi + \frac{7\epsilon^8}{96} \sin 2\chi \cos 6\chi \\
 &+ \left(\frac{\epsilon^4}{2} + \frac{5\epsilon^6}{12} + \frac{29\epsilon^8}{144}\right) \sin 2\chi \cos 2\chi + \left(\frac{7\epsilon^6}{48} + \frac{523\epsilon^8}{2880}\right) \sin 4\chi \cos 2\chi \\
 &+ \frac{19\epsilon^8}{240} \sin 6\chi \cos 2\chi - \left(\frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} - \frac{503\epsilon^8}{11520}\right) \sin 4\chi \\
 &- \frac{5\epsilon^8}{48} \sin 4\chi \cos 4\chi - \left(\frac{5\epsilon^6}{24} + \frac{377\epsilon^8}{1440}\right) \sin 2\chi \cos 4\chi \\
 &- \frac{35\epsilon^8}{576} \sin 4\chi \cos 4\chi + \left(\frac{13\epsilon^8}{480} + \frac{461\epsilon^8}{13440}\right) \sin 6\chi \\
 &+ \frac{13\epsilon^8}{160} \sin 2\chi \cos 6\chi - \frac{1237\epsilon^8}{161280} \sin 8\chi,
 \end{aligned}$$

or, on reduction and rearrangement, this becomes

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

This approximation agrees with the expression determined by Lagrange's series.

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\chi$ —THIRD METHOD.

We can develop  $\varphi - \chi$  in terms of  $\chi$  by a method similar to the second method of developing the same in terms of  $\varphi$ . (See p. 18.)

Let

$$\frac{p}{2} = \frac{z}{2} - (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8 + \dots).$$

But

$$\log_e \tan \frac{p}{2} = \log_e \tan \frac{z}{2} - \epsilon^2 \cos p - \frac{\epsilon^4}{3} \cos^3 p - \frac{\epsilon^6}{5} \cos^5 p \\ - \frac{\epsilon^8}{7} \cos^7 p - \dots$$

From the Taylor development on p. 19, by changing the sign of  $h$ , and by interchanging  $p$  and  $z$ , we get

$$\log_e \tan \left( \frac{z}{2} - h \right) = \log_e \tan \frac{z}{2} - \frac{2h}{\sin z} - \frac{2 \cos z}{\sin^2 z} h^2 - \left( \frac{4 \cos^2 z}{3 \sin^3 z} \right. \\ \left. + \frac{4}{3 \sin^3 z} \right) h^3 - \left( \frac{2 \cos^3 z}{3 \sin^4 z} + \frac{10 \cos z}{3 \sin^4 z} \right) h^4 - \dots$$

By substituting the value of  $h$  and by retaining terms to the eighth power of  $\epsilon$  inclusive, we obtain

$$\log_e \tan \left( \frac{z}{2} - h \right) = \log_e \tan \frac{z}{2} - \frac{2}{\sin z} (a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + d\epsilon^8) \\ - \frac{2 \cos z}{3 \sin^2 z} [a^2\epsilon^4 + 2 ab\epsilon^6 + (b^2 + 2 ac) \epsilon^8] - \left( \frac{4 \cos^2 z}{3 \sin^3 z} \right. \\ \left. + \frac{4}{3 \sin^3 z} \right) (a^3\epsilon^6 + 3 a^2 b\epsilon^8) - \left( \frac{2 \cos^3 z}{3 \sin^4 z} + \frac{10 \cos z}{3 \sin^4 z} \right) a^4\epsilon^8.$$

The powers of  $\cos p$  must now be approximated in terms of functions of  $z$  to include all eighth powers of  $\epsilon$ . We have assumed

$$\frac{p}{2} = \frac{z}{2} - h,$$

or

$$\begin{aligned} p &= z - 2h. \\ \cos(z - 2h) &= \cos z \cos 2h + \sin z \sin 2h \\ &= (1 - 2h^2) \cos z + \left(2h - \frac{4h^3}{3}\right) \sin z. \end{aligned}$$

The approximation does not need to be carried further, since powers of  $\epsilon$  are not required above the sixth, because we are approximating for  $\epsilon^2 \cos p$ .

Substituting the value of  $h$ , we get

$$\begin{aligned} \cos(z - 2h) &= \cos p = (1 - 2a^2\epsilon^4 - 4abe^6) \cos z + \\ &\quad \left(2a\epsilon^2 + 2b\epsilon^4 + 2c\epsilon^6 - \frac{4a^3}{3}\epsilon^6\right) \sin z, \end{aligned}$$

$$\begin{aligned} \cos^3 p &= (1 - 6a^2\epsilon^4) \cos^3 z + 3(2a\epsilon^2 + 2b\epsilon^4) \sin z \cos^2 z \\ &\quad + 12a^2\epsilon^4 \sin^2 z \cos z, \end{aligned}$$

$$\cos^5 p = \cos^5 z + 10a\epsilon^2 \sin z \cos^4 z,$$

$$\cos^7 p = \cos^7 z.$$

Substituting these values in the series for

$$\log_e \tan \frac{p}{2},$$

we get

$$\begin{aligned} \log_e \tan \frac{p}{2} &= \log_e \tan \frac{z}{2} - (\epsilon^2 - 2a^2\epsilon^6 - 4abe^8) \cos z \\ &\quad - \left(2a\epsilon^4 + 2b\epsilon^6 + 2c\epsilon^8 - \frac{4a^3}{3}\epsilon^8\right) \sin z - \left(\frac{\epsilon^4}{3} - 2a^2\epsilon^6\right) \cos^2 z \\ &\quad - (2a\epsilon^2 + 2b\epsilon^4) \sin z \cos^2 z - 4a^2\epsilon^4 \sin^2 z \cos z - \frac{\epsilon^6}{5} \cos^4 z \\ &\quad - 2a\epsilon^2 \sin z \cos^4 z - \frac{\epsilon^8}{7} \cos^6 z. \end{aligned}$$

This series must be identically equal to the series obtained above by the Taylor development and hence the coefficients of similar powers of  $\epsilon$  must be equal in the two series.



Equating these coefficients, we get:

$$\begin{aligned}
 -\frac{2a}{\sin z} &= -\cos z, \\
 -\frac{2b}{\sin z} - \frac{2a^2 \cos z}{\sin^2 z} &= -2a \sin z - \frac{\cos^3 z}{3}, \\
 -\frac{2c}{\sin z} - \frac{4ab \cos z}{\sin^2 z} - \frac{4a^3 \cos^2 z}{3 \sin^3 z} - \frac{4a^3}{3 \sin^3 z} &= 2a^2 \cos z \\
 &\quad - 2b \sin z - 2a \sin z \cos^2 z - \frac{\cos^5 z}{5}, \\
 -\frac{2d}{\sin z} - \frac{2b^2 \cos z}{\sin^2 z} - \frac{4ac \cos z}{\sin^2 z} - \frac{4a^2 b \cos^2 z}{\sin^3 z} - \frac{4a^2 b}{\sin^3 z} \\
 &\quad - \frac{2a^4 \cos^3 z}{3 \sin^4 z} - \frac{10a^4 \cos z}{3 \sin^4 z} = 4ab \cos z - 2c \sin z + \frac{4a^3 \sin z}{3} \\
 &\quad + 2a^2 \cos^3 z - 2b \sin z \cos^2 z - 4a^2 \sin^2 z \cos z \\
 &\quad - 2a \sin z \cos^4 z - \frac{\cos^7 z}{7}.
 \end{aligned}$$

From these equations in succession we obtain the values of  $a$ ,  $b$ ,  $c$ , and  $d$ .

(For the necessary reductions see the reduction table, p. 88.)

$$a = \frac{1}{2} \sin z \cos z = \frac{1}{4} \sin 2z,$$

$$b = \frac{1}{2} \sin z \cos z - \frac{7}{12} \sin z \cos^3 z = \frac{5}{48} \sin 2z - \frac{7}{96} \sin 4z,$$

$$\begin{aligned}
 c &= \frac{1}{2} \sin z \cos z - \frac{17}{12} \sin z \cos^3 z + \frac{14}{15} \sin z \cos^5 z \\
 &= \frac{1}{24} \sin 2z - \frac{29}{480} \sin 4z + \frac{7}{240} \sin 6z,
 \end{aligned}$$

$$\begin{aligned}
 d &= \frac{1}{2} \sin z \cos z - \frac{5}{2} \sin z \cos^3 z + \frac{889}{240} \sin z \cos^5 z \\
 &\quad - \frac{4279}{2520} \sin z \cos^7 z = \frac{13}{720} \sin 2z - \frac{811}{23040} \sin 4z \\
 &\quad + \frac{81}{2240} \sin 6z - \frac{4279}{322560} \sin 8z.
 \end{aligned}$$

With these values the series becomes after rearrangement the desired approximation

$$p = z - \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2z + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4z \\ - \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6z + \frac{4279\epsilon^8}{161280} \sin 8z;$$

or, in terms of  $\varphi$  and  $\chi$ , we get, as before, the approximation

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

**DEVELOPMENT OF  $\varphi - \chi$  IN TERMS OF  $\chi$ —FOURTH METHOD.**

$\varphi - \chi$  may be developed in terms of  $\chi$  by differentiating the equation of definition considering  $\varphi$  as a function of  $\epsilon^2$  or of  $h$ , or by using the more convenient form containing  $p$  and by considering  $p$  as a function of  $\epsilon^2$  or of  $h$ . For convenience we write the expression in the form

$$\log_e \tan \frac{z}{2} = \log_e \tan \frac{p}{2} + \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p \\ + \left( \frac{h^2}{12} + \frac{h^3}{16} + \frac{3h^4}{64} \right) \cos 3p + \left( \frac{h^3}{80} + \frac{h^4}{64} \right) \cos 5p \\ + \frac{h^4}{448} \cos 7p.$$

Differentiating this expression, considering  $p$  as a function of  $h$ , we get

$$\left[ \operatorname{cosec} p - \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p - \left( \frac{h^2}{4} + \frac{3h^3}{16} + \frac{9h^4}{64} \right) \sin 3p \right. \\ \left. - \left( \frac{h^3}{16} + \frac{5h^4}{64} \right) \sin 5p - \frac{h^4}{64} \sin 7p \right] \frac{dp}{dh} \\ + \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \cos p + \left( \frac{h}{6} + \frac{3h^2}{16} + \frac{3h^3}{16} \right) \cos 3p \\ + \left( \frac{3h^2}{80} + \frac{h^3}{16} \right) \cos 5p + \frac{h^3}{112} \cos 7p = 0,$$

$$\begin{aligned}
& \left[ \operatorname{cosec} p - \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p - \left( \frac{h^2}{4} + \frac{3h^3}{16} + \frac{9h^4}{64} \right) \sin 3p \right. \\
& \quad - \left. \left( \frac{h^3}{16} + \frac{5h^4}{64} \right) \sin 5p - \frac{h^4}{64} \sin 7p \right] \frac{d^2 p}{dh^2} - \left[ \operatorname{cosec} p \cot p \right. \\
& \quad + \left. \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p + \left( \frac{3h^2}{4} + \frac{9h^3}{16} + \frac{27h^4}{64} \right) \cos 3p \right. \\
& \quad + \left. \left( \frac{5h^3}{16} + \frac{25h^4}{64} \right) \cos 5p + \frac{7h^4}{64} \cos 7p \right] \left( \frac{dp}{dh} \right)^2 \\
& \quad - 2 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \sin p + \left( \frac{h}{2} + \frac{9h^2}{16} + \frac{9h^3}{16} \right) \sin 3p \right. \\
& \quad + \left. \left( \frac{3h^2}{16} + \frac{5h^3}{16} \right) \sin 5p + \frac{h^3}{16} \sin 7p \right] \frac{dp}{dh} \\
& \quad + \left( \frac{1}{2} + \frac{3h}{4} + \frac{15h^2}{16} \right) \cos p + \left( \frac{1}{6} + \frac{3h}{8} + \frac{9h^2}{16} \right) \cos 3p \\
& \quad + \left( \frac{3h}{40} + \frac{3h^2}{16} \right) \cos 5p + \frac{3h^2}{112} \cos 7p = 0,
\end{aligned}$$

$$\begin{aligned}
& \left[ \operatorname{cosec} p - \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p - \left( \frac{h^2}{4} + \frac{3h^3}{16} + \frac{9h^4}{64} \right) \sin 3p \right. \\
& \quad - \left. \left( \frac{h^3}{16} + \frac{5h^4}{64} \right) \sin 5p - \frac{h^4}{64} \sin 7p \right] \frac{d^3 p}{dh^3} + \left[ \operatorname{cosec} p \cot^2 p \right. \\
& \quad + \operatorname{cosec}^3 p + \left. \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p \right. \\
& \quad + \left. \left( \frac{9h^2}{4} + \frac{27h^3}{16} + \frac{81h^4}{64} \right) \sin 3p + \left( \frac{25h^3}{16} + \frac{125h^4}{64} \right) \sin 5p \right. \\
& \quad + \left. \frac{49h^4}{64} \sin 7p \right] \left( \frac{dp}{dh} \right)^3 - 3 \left[ \operatorname{cosec} p \cot p \right. \\
& \quad + \left. \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p + \left( \frac{3h^2}{4} + \frac{9h^3}{16} + \frac{27h^4}{64} \right) \cos 3p \right. \\
& \quad + \left. \left( \frac{5h^3}{16} + \frac{25h^4}{64} \right) \cos 5p + \frac{7h^4}{64} \cos 7p \right] \frac{dp}{dh} \frac{d^2 p}{dh^2} \\
& \quad - 3 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \sin p + \left( \frac{h}{2} + \frac{9h^2}{16} + \frac{9h^3}{16} \right) \sin 3p \right. \\
& \quad + \left. \left( \frac{3h^2}{16} + \frac{5h^3}{16} \right) \sin 5p + \frac{h^3}{16} \sin 7p \right] \frac{d^2 p}{dh^2} \\
& \quad - 3 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \cos p + \left( \frac{3h}{2} + \frac{27h^2}{16} + \frac{27h^3}{16} \right) \cos 3p \right. \\
& \quad + \left. \left( \frac{15h^2}{16} + \frac{25h^3}{16} \right) \cos 5p + \frac{7h^3}{16} \cos 7p \right] \left( \frac{dp}{dh} \right)^2
\end{aligned}$$

$$\begin{aligned}
& -3 \left[ \left( \frac{1}{2} + \frac{3h}{4} + \frac{15h^2}{16} \right) \sin p + \left( \frac{1}{2} + \frac{9h}{8} + \frac{27h^2}{16} \right) \sin 3p \right. \\
& + \left. \left( \frac{3h}{8} + \frac{15h^2}{16} \right) \sin 5p + \frac{3h^2}{16} \sin 7p \right] \frac{dp}{dh} + \left( \frac{3}{4} + \frac{15h}{8} \right) \cos p \\
& + \left( \frac{3}{8} + \frac{9h}{8} \right) \cos 3p + \left( \frac{3}{40} + \frac{3h}{8} \right) \cos 5p + \frac{3h}{56} \cos 7p = 0, \\
& \left[ \operatorname{cosec} p - \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p - \left( \frac{h^2}{4} + \frac{3h^3}{16} + \frac{9h^4}{64} \right) \sin 3p \right. \\
& - \left. \left( \frac{h^3}{16} + \frac{5h^4}{64} \right) \sin 5p - \frac{h^4}{64} \sin 7p \right] \frac{d^4 p}{dh^4} + \left[ -\operatorname{cosec} p \cot^3 p \right. \\
& - 5 \operatorname{cosec}^3 p \cot p + \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p \\
& + \left( \frac{27h^2}{4} + \frac{81h^3}{16} + \frac{243h^4}{64} \right) \cos 3p + \left( \frac{125h^3}{16} + \frac{625h^4}{64} \right) \cos 5p \\
& + \left. \frac{343h^4}{64} \cos 7p \right] \left( \frac{dp}{dh} \right)^4 - 4 \left[ \operatorname{cosec} p \cot p \right. \\
& + \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p + \left( \frac{3h^2}{4} + \frac{9h^3}{16} + \frac{27h^4}{64} \right) \cos 3p \\
& + \left. \left( \frac{5h^3}{16} + \frac{25h^4}{64} \right) \cos 5p + \frac{7h^4}{64} \cos 7p \right] \frac{dp}{dh} \frac{d^2 p}{dh^2} \\
& - 4 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \sin p + \left( \frac{h}{2} + \frac{9h^2}{16} + \frac{9h^3}{16} \right) \sin 3p \right. \\
& + \left. \left( \frac{3h^2}{16} + \frac{5h^3}{16} \right) \sin 5p + \frac{h^3}{16} \sin 7p \right] \frac{d^3 p}{dh^3} \\
& + 4 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \sin p + \left( \frac{9h}{2} + \frac{81h^2}{16} + \frac{81h^3}{16} \right) \sin 3p \right. \\
& + \left. \left( \frac{75h^2}{16} + \frac{125h^3}{16} \right) \sin 5p + \frac{49h^3}{16} \sin 7p \right] \left( \frac{dp}{dh} \right)^3 \\
& + 6 \left[ \operatorname{cosec} p \cot^2 p + \operatorname{cosec}^3 p + \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \sin p \right. \\
& + \left( \frac{9h^2}{4} + \frac{27h^3}{16} + \frac{81h^4}{64} \right) \sin 3p + \left( \frac{25h^3}{16} + \frac{125h^4}{64} \right) \sin 5p \\
& + \left. \frac{49h^4}{64} \sin 7p \right] \left( \frac{dp}{dh} \right)^2 \frac{d^2 p}{dh^2} - 3 \left[ \operatorname{cosec} p \cot p \right. \\
& + \left( h + \frac{h^2}{4} + \frac{h^3}{8} + \frac{5h^4}{64} \right) \cos p + \left( \frac{3h^2}{4} + \frac{9h^3}{16} + \frac{27h^4}{64} \right) \cos 3p \\
& + \left. \left( \frac{5h^3}{16} + \frac{25h^4}{64} \right) \cos 5p + \frac{7h^4}{64} \cos 7p \right] \left( \frac{d^2 p}{dh^2} \right)^2 \\
& - 12 \left[ \left( 1 + \frac{h}{2} + \frac{3h^2}{8} + \frac{5h^3}{16} \right) \cos p + \left( \frac{3h}{2} + \frac{27h^2}{16} + \frac{27h^3}{16} \right) \cos 3p \right.
\end{aligned}$$

$$\begin{aligned}
& + \left( \frac{15h^2}{16} + \frac{25h^3}{16} \right) \cos 5p + \frac{7h^3}{16} \cos 7p \left] \frac{dp}{dh} \frac{d^2p}{dh^2} \right. \\
& - 6 \left[ \left( \frac{1}{2} + \frac{3h}{4} + \frac{15h^2}{16} \right) \sin p + \left( \frac{1}{2} + \frac{9h}{8} + \frac{27h^2}{16} \right) \sin 3p \right. \\
& + \left. \left( \frac{3h}{8} + \frac{15h^2}{16} \right) \sin 5p + \frac{3h^2}{16} \sin 7p \right] \frac{d^2p}{dh^2} \\
& - 6 \left[ \left( \frac{1}{2} + \frac{3h}{4} + \frac{15h^2}{16} \right) \cos p + \left( \frac{3}{2} + \frac{27h}{8} + \frac{81h^2}{16} \right) \cos 3p \right. \\
& + \left. \left( \frac{15h}{8} + \frac{75h^2}{16} \right) \cos 5p + \frac{21h^2}{16} \cos 7p \right] \left( \frac{dp}{dh} \right)^2 \\
& - 4 \left[ \left( \frac{3}{4} + \frac{15h}{8} \right) \sin p + \left( \frac{9}{8} + \frac{27h}{8} \right) \sin 3p \right. \\
& + \left. \left( \frac{3}{8} + \frac{15h}{8} \right) \sin 5p + \frac{3h}{8} \sin 7p \right] \frac{dp}{dh} + \frac{15}{8} \cos p \\
& + \frac{9}{8} \cos 3p + \frac{3}{8} \cos 5p + \frac{3}{56} \cos 7p = 0.
\end{aligned}$$

Denoting by brackets the values of these derivatives for  $h=0$ , and remembering that functions of  $p$  become functions of  $z$  for  $h=0$ , we obtain in succession by substitution and reduction (for the necessary reductions see the reduction table, p. 88):

$$[p] = z;$$

$$\left[ \frac{dp}{dh} \right] = -\sin z \cos z = -\frac{1}{2} \sin 2z,$$

$$\left[ \frac{d^2p}{dh^2} \right] = -2 \sin z \cos z + \frac{7}{3} \sin z \cos^3 z = -\frac{5}{12} \sin 2z + \frac{7}{24} \sin 4z,$$

$$\begin{aligned}
\left[ \frac{d^3p}{dh^3} \right] &= -6 \sin z \cos z + 17 \sin z \cos^3 z - \frac{56}{5} \sin z \cos^5 z \\
&= -\frac{1}{2} \sin 2z + \frac{29}{40} \sin 4z - \frac{7}{20} \sin 6z,
\end{aligned}$$

$$\begin{aligned}
\left[ \frac{d^4p}{dh^4} \right] &= -24 \sin z \cos z + 120 \sin z \cos^3 z - \frac{889}{5} \sin z \cos^5 z \\
&+ \frac{8558}{105} \sin z \cos^7 z = -\frac{13}{15} \sin 2z + \frac{811}{480} \sin 4z \\
&- \frac{243}{140} \sin 6z + \frac{4279}{6720} \sin 8z.
\end{aligned}$$

But from Maclauren's theorem, we have:

$$p = \left[ p \right] + \frac{\epsilon^2}{1!} \left[ \frac{dp}{dh} \right] + \frac{\epsilon^4}{2!} \left[ \frac{d^2p}{dh^2} \right] + \frac{\epsilon^6}{3!} \left[ \frac{d^3p}{dh^3} \right] + \frac{\epsilon^8}{4!} \left[ \frac{d^4p}{dh^4} \right] + \dots$$

Substituting the above values in this series and rearranging, we obtain the approximation sought:

$$p = z - \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2z + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4z \\ - \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6z + \frac{4279\epsilon^8}{161280} \sin 8z,$$

or, in terms of  $\varphi$  and  $\chi$ , we obtain, as before, the approximation:

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

**DEVELOPMENT OF  $\varphi - \chi$  IN TERMS OF  $\chi$ —FIFTH METHOD.**

If we wish to develop  $\varphi - \chi$  in terms of  $\chi$ , starting with the expression:

$$\tan \frac{z}{2} = \tan \frac{p}{2} \left[ 1 + h \cos p + h^2 \left( \frac{\cos^2 p}{2} + \frac{\cos^3 p}{3} \right) + h^3 \left( \frac{\cos^3 p}{6} \right. \right. \\ \left. \left. + \frac{\cos^4 p}{3} + \frac{\cos^5 p}{5} \right) + h^4 \left( \frac{\cos^4 p}{24} + \frac{\cos^5 p}{6} + \frac{23\cos^6 p}{90} + \frac{\cos^7 p}{7} \right) \right]$$

it is more convenient to make the substitution

$$\tan \frac{p}{2} = \frac{\sin p}{1 + \cos p}$$

and write it in the form (for the reductions, see table, p. 88.)

$$-(1 + \cos p) \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \sin p \\ + \left( \frac{h}{2} + \frac{h^2}{12} + \frac{7h^3}{96} + \frac{h^4}{24} \right) \sin 2p + \left( \frac{h^2}{8} + \frac{h^3}{16} + \frac{7h^4}{160} \right) \sin 3p \\ + \left( \frac{h^2}{24} + \frac{11h^3}{240} + \frac{7h^4}{192} \right) \sin 4p + \left( \frac{h^3}{48} + \frac{13h^4}{576} \right) \sin 5p \\ + \left( \frac{h^3}{160} + \frac{h^4}{84} \right) \sin 6p + \frac{23h^4}{5760} \sin 7p + \frac{h^4}{896} \sin 8p = 0.$$

We shall now differentiate this expression considering  $p$  as a function of  $h$  or of  $\epsilon^2$ .

$$\begin{aligned} & \left[ \sin p \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p \right. \\ & + \left( h + \frac{h^2}{6} + \frac{7h^3}{48} + \frac{h^4}{12} \right) \cos 2p + \left( \frac{3h^2}{8} + \frac{3h^3}{16} + \frac{21h^4}{160} \right) \cos 3p \\ & + \left( \frac{h^2}{6} + \frac{11h^3}{60} + \frac{7h^4}{48} \right) \cos 4p + \left( \frac{5h^3}{48} + \frac{65h^4}{576} \right) \cos 5p \\ & + \left( \frac{3h^3}{80} + \frac{h^4}{14} \right) \cos 6p + \frac{161h^4}{5760} \cos 7p + \frac{h^4}{112} \cos 8p \left. \right] \frac{dp}{dh} \\ & + \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \sin p + \left( \frac{1}{2} + \frac{h}{6} + \frac{7h^2}{32} + \frac{h^3}{6} \right) \sin 2p \\ & + \left( \frac{h}{4} + \frac{3h^2}{16} + \frac{7h^3}{40} \right) \sin 3p + \left( \frac{h}{12} + \frac{11h^2}{80} + \frac{7h^3}{48} \right) \sin 4p \\ & + \left( \frac{h^2}{16} + \frac{13h^3}{144} \right) \sin 5p + \left( \frac{3h^2}{160} + \frac{h^3}{21} \right) \sin 6p + \frac{23h^3}{1440} \sin 7p \\ & + \frac{h^3}{224} \sin 8p = 0, \end{aligned}$$

$$\begin{aligned} & \left[ \sin p \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p \right. \\ & + \left( h + \frac{h^2}{6} + \frac{7h^3}{48} + \frac{h^4}{12} \right) \cos 2p + \left( \frac{3h^2}{8} + \frac{3h^3}{16} + \frac{21h^4}{160} \right) \cos 3p \\ & + \left( \frac{h^2}{6} + \frac{11h^3}{60} + \frac{7h^4}{48} \right) \cos 4p + \left( \frac{5h^3}{48} + \frac{65h^4}{576} \right) \cos 5p \\ & + \left( \frac{3h^3}{80} + \frac{h^4}{14} \right) \cos 6p + \frac{161h^4}{5760} \cos 7p \\ & + \frac{h^4}{112} \cos 8p \left. \right] \frac{d^2p}{dh^2} + \left[ \cos p \tan \frac{z}{2} \right. \\ & - \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \sin p - \left( 2h + \frac{h^2}{3} + \frac{7h^3}{24} + \frac{h^4}{6} \right) \sin 2p \\ & - \left( \frac{9h^2}{8} + \frac{9h^3}{16} + \frac{63h^4}{160} \right) \sin 3p - \left( \frac{2h^2}{3} + \frac{11h^3}{15} + \frac{7h^4}{12} \right) \sin 4p \\ & - \left( \frac{25h^3}{48} + \frac{325h^4}{576} \right) \sin 5p - \left( \frac{9h^3}{40} + \frac{3h^4}{7} \right) \sin 6p \\ & - \frac{1127h^4}{5760} \sin 7p - \frac{h^4}{14} \sin 8p \left. \right] \left( \frac{dp}{dh} \right)^2 \\ & + 2 \left[ \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \cos p + \left( 1 + \frac{h}{3} + \frac{7h^2}{16} + \frac{h^3}{3} \right) \cos 2p \right. \end{aligned}$$

$$\begin{aligned}
 & + \left( \frac{3h}{4} + \frac{9h^2}{16} + \frac{21h^3}{40} \right) \cos 3p + \left( \frac{h}{3} + \frac{11h^2}{20} + \frac{7h^3}{12} \right) \cos 4p \\
 & + \left( \frac{5h^2}{16} + \frac{65h^3}{144} \right) \cos 5p + \left( \frac{9h^2}{80} + \frac{2h^3}{7} \right) \cos 6p \\
 & + \left. \frac{161h^3}{1440} \cos 7p + \frac{h^3}{28} \cos 8p \right] \frac{dp}{dh} + \left( \frac{1}{4} + \frac{h}{4} + \frac{29h^2}{96} \right) \sin p \\
 & + \left( \frac{1}{6} + \frac{7h}{16} + \frac{h^2}{2} \right) \sin 2p + \left( \frac{1}{4} + \frac{3h}{8} + \frac{21h^2}{40} \right) \sin 3p \\
 & + \left( \frac{1}{12} + \frac{11h}{40} + \frac{7h^2}{16} \right) \sin 4p + \left( \frac{h}{8} + \frac{13h^2}{48} \right) \sin 5p \\
 & + \left( \frac{3h}{80} + \frac{h^2}{7} \right) \sin 6p + \frac{23h^3}{480} \sin 7p + \frac{3h^2}{224} \sin 8p = 0,
 \end{aligned}$$

$$\begin{aligned}
 & \left[ \sin p \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p \right. \\
 & + \left( h + \frac{h^2}{6} + \frac{7h^3}{48} + \frac{h^4}{12} \right) \cos 2p + \left( \frac{3h^2}{8} + \frac{3h^3}{16} + \frac{21h^4}{160} \right) \cos 3p \\
 & + \left( \frac{h^2}{6} + \frac{11h^3}{60} + \frac{7h^4}{48} \right) \cos 4p + \left( \frac{5h^3}{48} + \frac{65h^4}{576} \right) \cos 5p \\
 & + \left. \left( \frac{3h^3}{80} + \frac{h^4}{14} \right) \cos 6p + \frac{161h^4}{5760} \cos 7p + \frac{h^4}{112} \cos 8p \right] \frac{d^2p}{dh^2} \\
 & + \left[ -\sin p \tan \frac{z}{2} - \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p \right. \\
 & - \left( 4h + \frac{2h^2}{3} + \frac{7h^3}{12} + \frac{h^4}{3} \right) \cos 2p - \left( \frac{27h^2}{8} + \frac{27h^3}{16} + \frac{189h^4}{160} \right) \cos 3p \\
 & - \left( \frac{8h^2}{3} + \frac{44h^3}{15} + \frac{7h^4}{3} \right) \cos 4p - \left( \frac{125h^3}{48} + \frac{1625h^4}{576} \right) \cos 5p \\
 & - \left( \frac{27h^3}{20} + \frac{18h^4}{7} \right) \cos 6p - \frac{7889h^4}{5760} \cos 7p \\
 & - \left. \frac{4h^4}{7} \cos 8p \right] \left( \frac{dp}{dh} \right)^2 + 3 \left[ \cos p \tan \frac{z}{2} \right. \\
 & - \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \sin p - \left( 2h + \frac{h^2}{3} + \frac{7h^3}{24} + \frac{h^4}{6} \right) \sin 2p \\
 & - \left( \frac{9h^2}{8} + \frac{9h^3}{16} + \frac{63h^4}{160} \right) \sin 3p - \left( \frac{2h^3}{3} + \frac{11h^3}{15} + \frac{7h^4}{12} \right) \sin 4p \\
 & - \left( \frac{25h^3}{48} + \frac{325h^4}{576} \right) \sin 5p - \left( \frac{9h^3}{40} + \frac{3h^4}{7} \right) \sin 6p \\
 & \left. - \frac{1127h^4}{5760} \sin 7p - \frac{h^4}{14} \sin 8p \right] \frac{dp}{dh} \frac{d^2p}{dh^2}
 \end{aligned}$$



$$\begin{aligned}
& + 3 \left[ \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \cos p + \left( 1 + \frac{h}{3} + \frac{7h^2}{16} + \frac{h^3}{3} \right) \cos 2p \right. \\
& + \left( \frac{3h}{4} + \frac{9h^2}{16} + \frac{21h^3}{40} \right) \cos 3p + \left( \frac{h}{3} + \frac{11h^2}{20} + \frac{7h^3}{12} \right) \cos 4p \\
& + \left( \frac{5h^2}{16} + \frac{65h^3}{144} \right) \cos 5p + \left( \frac{9h^2}{80} + \frac{2h^3}{7} \right) \cos 6p \\
& + \frac{161h^3}{1440} \cos 7p + \frac{h^3}{28} \cos 8p \left] \frac{d^2p}{dh^2} + 3 \left[ - \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \sin p \right. \\
& - \left( 2 + \frac{2h}{3} + \frac{7h^2}{8} + \frac{2h^3}{3} \right) \sin 2p - \left( \frac{9h}{4} + \frac{27h^2}{16} + \frac{63h^3}{40} \right) \sin 3p \\
& - \left( \frac{4h}{3} + \frac{11h^2}{5} + \frac{7h^3}{3} \right) \sin 4p - \left( \frac{25h^2}{16} + \frac{325h^3}{144} \right) \sin 5p \\
& - \left( \frac{27h^2}{40} + \frac{12h^3}{7} \right) \sin 6p - \frac{1127h^3}{1440} \sin 7p \\
& \left. - \frac{2h^3}{7} \sin 8p \right] \left( \frac{dp}{dh} \right)^2 + 3 \left[ \left( \frac{1}{4} + \frac{h}{4} + \frac{29h^2}{96} \right) \cos p \right. \\
& + \left( \frac{1}{3} + \frac{7h}{8} + h^2 \right) \cos 2p + \left( \frac{3}{4} + \frac{9h}{8} + \frac{63h^2}{40} \right) \cos 3p \\
& + \left( \frac{1}{3} + \frac{11h}{10} + \frac{7h^2}{4} \right) \cos 4p + \left( \frac{5h}{8} + \frac{65h^2}{48} \right) \cos 5p \\
& + \left( \frac{9h}{40} + \frac{6h^2}{7} \right) \cos 6p + \frac{161h^2}{480} \cos 7p \\
& + \frac{3h^2}{28} \cos 8p \left] \frac{dp}{dh} + \left( \frac{1}{4} + \frac{29h}{48} \right) \sin p + \left( \frac{7}{16} + h \right) \sin 2p \\
& + \left( \frac{3}{8} + \frac{21h}{20} \right) \sin 3p + \left( \frac{11}{40} + \frac{7h}{8} \right) \sin 4p \\
& + \left( \frac{1}{8} + \frac{13h}{24} \right) \sin 5p + \left( \frac{3}{80} + \frac{2h}{7} \right) \sin 6p + \frac{23h}{240} \sin 7p \\
& + \frac{3h}{112} \sin 8p = 0,
\end{aligned}$$

$$\begin{aligned}
& \left[ \sin p \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p \right. \\
& + \left( h + \frac{h^2}{6} + \frac{7h^3}{48} + \frac{h^4}{12} \right) \cos 2p + \left( \frac{3h^2}{8} + \frac{3h^3}{16} + \frac{21h^4}{160} \right) \cos 3p \\
& + \left( \frac{h^2}{6} + \frac{11h^3}{60} + \frac{7h^4}{48} \right) \cos 4p + \left( \frac{5h^3}{48} + \frac{65h^4}{576} \right) \cos 5p \\
& + \left( \frac{3h^3}{80} + \frac{h^4}{14} \right) \cos 6p + \frac{161h^4}{5760} \cos 7p + \frac{h^4}{112} \cos 8p \left] \frac{d^4p}{dh^4} \right. \\
& \left. + \left[ - \cos p \tan \frac{z}{2} + \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \sin p \right. \right.
\end{aligned}$$

$$\begin{aligned}
 & + \left( 8h + \frac{4h^2}{3} + \frac{7h^3}{6} + \frac{2h^4}{3} \right) \sin 2p \\
 & + \left( \frac{81h^2}{8} + \frac{81h^3}{16} + \frac{567h^4}{160} \right) \sin 3p \\
 & + \left( \frac{32h^2}{3} + \frac{176h^3}{15} + \frac{28h^4}{3} \right) \sin 4p \\
 & + \left( \frac{625h^3}{48} + \frac{8125h^4}{576} \right) \sin 5p + \left( \frac{81h^3}{10} + \frac{108h^4}{7} \right) \sin 6p \\
 & + \frac{55223h^4}{5760} \sin 7p + \frac{32h^4}{7} \sin 8p \left] \left( \frac{dp}{dh} \right)^4 \right. \\
 & + 4 \left[ \cos p \tan \frac{z}{2} - \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \sin p \right. \\
 & - \left( 2h + \frac{h^2}{3} + \frac{7h^3}{24} + \frac{h^4}{6} \right) \sin 2p - \left( \frac{9h^2}{8} + \frac{9h^3}{16} + \frac{63h^4}{160} \right) \sin 3p \\
 & - \left( \frac{2h^2}{3} + \frac{11h^3}{15} + \frac{7h^4}{12} \right) \sin 4p - \left( \frac{25h^3}{48} + \frac{325h^4}{576} \right) \sin 5p \\
 & - \left( \frac{9h^3}{40} + \frac{3h^4}{7} \right) \sin 6p - \frac{1127h^4}{5760} \sin 7p \\
 & \left. - \frac{h^4}{14} \sin 8p \right] \frac{dp}{dh} \frac{d^2p}{dh^2} + 4 \left[ \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \cos p \right. \\
 & + \left( 1 + \frac{h}{3} + \frac{7h^2}{16} + \frac{h^3}{3} \right) \cos 2p + \left( \frac{3h}{4} + \frac{9h^2}{16} + \frac{21h^3}{40} \right) \cos 3p \\
 & + \left( \frac{h}{3} + \frac{11h^2}{20} + \frac{7h^3}{12} \right) \cos 4p + \left( \frac{5h^2}{16} + \frac{65h^3}{144} \right) \cos 5p \\
 & + \left( \frac{9h^2}{80} + \frac{2h^3}{7} \right) \cos 6p + \frac{161h^3}{1440} \cos 7p \\
 & \left. + \frac{h^3}{28} \cos 8p \right] \frac{d^2p}{dh^2} + 4 \left[ - \left( \frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288} \right) \cos p \right. \\
 & - \left( 4 + \frac{4h}{3} + \frac{7h^2}{4} + \frac{4h^3}{3} \right) \cos 2p - \left( \frac{27h}{4} + \frac{81h^2}{16} + \frac{189h^3}{40} \right) \cos 3p \\
 & - \left( \frac{16h}{3} + \frac{44h^2}{5} + \frac{28h^3}{3} \right) \cos 4p - \left( \frac{125h^2}{16} + \frac{1625h^3}{144} \right) \cos 5p \\
 & - \left( \frac{81h^2}{20} + \frac{72h^3}{7} \right) \cos 6p - \frac{7889h^3}{1440} \cos 7p \\
 & \left. - \frac{16h^3}{7} \cos 8p \right] \left( \frac{dp}{dh} \right)^3 + 6 \left[ - \sin p \tan \frac{z}{2} \right. \\
 & \left. - \left( 1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152} \right) \cos p - \left( 4h + \frac{2h^2}{3} + \frac{7h^3}{12} + \frac{h^4}{3} \right) \cos 2p \right.
 \end{aligned}$$

$$\begin{aligned}
& -\left(\frac{27h^2}{8} + \frac{27h^3}{16} + \frac{189h^4}{160}\right) \cos 3p - \left(\frac{8h^2}{3} + \frac{44h^3}{15} + \frac{7h^4}{3}\right) \cos 4p \\
& -\left(\frac{125h^2}{48} + \frac{1625h^4}{576}\right) \cos 5p - \left(\frac{27h^3}{20} + \frac{18h^4}{7}\right) \cos 6p \\
& -\frac{7889h^4}{5760} \cos 7p - \frac{4h^4}{7} \cos 8p \left] \left(\frac{dp}{dh}\right)^2 \frac{d^2p}{dh^2} \right. \\
& + 3 \left[ \cos p \tan \frac{z}{2} - \left(1 + \frac{h^2}{8} + \frac{h^3}{24} + \frac{29h^4}{1152}\right) \sin p \right. \\
& - \left(2h + \frac{h^2}{3} + \frac{7h^3}{24} + \frac{h^4}{6}\right) \sin 2p - \left(\frac{9h^2}{8} + \frac{9h^3}{16} + \frac{63h^4}{160}\right) \sin 3p \\
& - \left(\frac{2h^2}{3} + \frac{11h^3}{15} + \frac{7h^4}{12}\right) \sin 4p - \left(\frac{25h^3}{48} + \frac{325h^4}{576}\right) \sin 5p \\
& - \left(\frac{9h^3}{40} + \frac{3h^4}{7}\right) \sin 6p - \frac{1127h^4}{5760} \sin 7p \\
& - \frac{h^4}{14} \sin 8p \left] \left(\frac{d^2p}{dh^2}\right)^2 + 12 \left[ -\left(\frac{h}{4} + \frac{h^2}{8} + \frac{29h^3}{288}\right) \sin p \right. \\
& - \left(2 + \frac{2h}{3} + \frac{7h^2}{8} + \frac{2h^3}{3}\right) \sin 2p - \left(\frac{9h}{4} + \frac{27h^2}{16} + \frac{63h^3}{40}\right) \sin 3p \\
& - \left(\frac{4h}{3} + \frac{11h^2}{5} + \frac{7h^3}{3}\right) \sin 4p - \left(\frac{25h^2}{16} + \frac{325h^3}{144}\right) \sin 5p \\
& - \left(\frac{27h^2}{40} + \frac{12h^3}{7}\right) \sin 6p - \frac{1127h^3}{1440} \sin 7p \\
& - \frac{2h^3}{7} \sin 8p \left] \frac{dp}{dh} \frac{d^2p}{dh^2} + 6 \left[ \left(\frac{1}{4} + \frac{h}{4} + \frac{29h^2}{96}\right) \cos p \right. \\
& + \left(\frac{1}{3} + \frac{7h}{8} + h^2\right) \cos 2p + \left(\frac{3}{4} + \frac{9h}{8} + \frac{63h^2}{40}\right) \cos 3p \\
& + \left(\frac{1}{3} + \frac{11h}{10} + \frac{7h^2}{4}\right) \cos 4p + \left(\frac{5h}{8} + \frac{65h^2}{48}\right) \cos 5p \\
& + \left(\frac{9h}{40} + \frac{6h^2}{7}\right) \cos 6p + \frac{161h^2}{480} \cos 7p + \frac{3h^2}{28} \cos 8p \left] \frac{d^2p}{dh^2} \right. \\
& + 6 \left[ -\left(\frac{1}{4} + \frac{h}{4} + \frac{29h^2}{96}\right) \sin p - \left(\frac{2}{3} + \frac{7h}{4} + 2h^2\right) \sin 2p \right. \\
& - \left(\frac{9}{4} + \frac{27h}{8} + \frac{189h^2}{40}\right) \sin 3p - \left(\frac{4}{3} + \frac{22h}{5} + 7h^2\right) \sin 4p \\
& - \left(\frac{25h}{8} + \frac{325h^2}{48}\right) \sin 5p - \left(\frac{27h}{20} + \frac{36h^2}{7}\right) \sin 6p \\
& - \frac{1127h^2}{480} \sin 7p - \frac{6h^2}{7} \sin 8p \left] \left(\frac{dp}{dh}\right)^2 \right. \\
& + 4 \left[ \left(\frac{1}{4} + \frac{29h}{48}\right) \cos p + \left(\frac{7}{8} + 2h\right) \cos 2p \right.
\end{aligned}$$

$$\begin{aligned}
& + \left( \frac{9}{8} + \frac{63h}{20} \right) \cos 3p + \left( \frac{11}{10} + \frac{7h}{2} \right) \cos 4p \\
& + \left( \frac{5}{8} + \frac{65h}{24} \right) \cos 5p + \left( \frac{9}{40} + \frac{12h}{7} \right) \cos 6p \\
& + \frac{161h}{240} \cos 7p + \frac{3h}{14} \cos 8p \left] \frac{dp}{dh} + \frac{29}{48} \sin p + \sin 2p \right. \\
& + \frac{21}{20} \sin 3p + \frac{7}{8} \sin 4p + \frac{13}{24} \sin 5p + \frac{2}{7} \sin 6p \\
& \left. + \frac{23}{240} \sin 7p + \frac{3}{112} \sin 8p = 0.
\end{aligned}$$

Evaluating these derivatives for  $h=0$ , remembering that functions of  $p$  become functions of  $z$  for  $h=0$ , we get by successive substitution and reduction (for the necessary reductions see the reduction table, p. 88):

$$\begin{aligned}
[p] &= z, \\
\left[ \frac{dp}{dh} \right] &= -\sin z \cos z = -\frac{1}{2} \sin 2z, \\
\left[ \frac{d^2p}{dh^2} \right] &= -2 \sin z \cos z + \frac{7}{3} \sin z \cos^3 z = -\frac{5}{12} \sin 2z + \frac{7}{24} \sin 4z, \\
\left[ \frac{d^3p}{dh^3} \right] &= -6 \sin z \cos z + 17 \sin z \cos^3 z - \frac{56}{5} \sin z \cos^5 z \\
&= -\frac{1}{2} \sin 2z + \frac{29}{40} \sin 4z - \frac{7}{20} \sin 6z, \\
\left[ \frac{d^4p}{dh^4} \right] &= -24 \sin z \cos z + 120 \sin z \cos^3 z - \frac{889}{5} \sin z \cos^5 z \\
&\quad + \frac{8558}{105} \sin z \cos^7 z \\
&= -\frac{13}{15} \sin 2z + \frac{811}{480} \sin 4z - \frac{243}{140} \sin 6z + \frac{4279}{6720} \sin 8z.
\end{aligned}$$

When these values are substituted in the Maclaurin development (see p. 45) and rearranged, we obtain, as before, the desired approximation:

$$\begin{aligned}
z = p + \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2z - \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4z \\
+ \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6z - \frac{4279\epsilon^8}{161280} \sin 8z,
\end{aligned}$$

or, in terms of  $\varphi$  and  $\chi$ , the approximation:

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

#### DEVELOPMENT OF $\varphi - \chi$ IN TERMS OF $\chi$ —SIXTH METHOD.

$\varphi - \chi$  can be developed in terms of  $\chi$  directly from the equation of definition by the application of Lagrange's theorem. Let us take the form:

$$\log_e \tan \frac{p}{2} = \log_e \tan \frac{z}{2} - \epsilon^2 \cos p - \frac{\epsilon^4}{3} \cos^3 p - \frac{\epsilon^6}{5} \cos^5 p \\ - \frac{\epsilon^8}{7} \cos^7 p - \dots$$

In this expression, let

$$x = \log_e \tan \frac{p}{2}$$

$$y = \log_e \tan \frac{z}{2},$$

and it becomes:

$$x = y - \epsilon^2 \cos p - \frac{\epsilon^4}{3} \cos^3 p - \frac{\epsilon^6}{5} \cos^5 p - \frac{\epsilon^8}{7} \cos^7 p - \dots$$

The series in  $\epsilon^2$  is a function of  $x$ , since  $p$  is a function of  $x$ . We might replace  $\cos p$  by its value in terms of  $x$ , but this is not necessary. The problem in hand is to develop the function  $2 \tan^{-1} e^x$  in terms of  $y$  or in terms of  $z$  through the functional relation between  $y$  and  $z$ . By Lagrange's theorem, since the series in  $\epsilon^2$  is a small quantity, the development may be expressed in general terms as follows:

$$f(x) = f(y) + \frac{1}{1!} g(y) f'(y) + \frac{1}{2!} \frac{d}{dy} \{ [g(y)]^2 f'(y) \} \\ + \frac{1}{3!} \frac{d^2}{dy^2} \{ [g(y)]^3 f'(y) \} + \frac{1}{4!} \frac{d^3}{dy^3} \{ [g(y)]^4 f'(y) \} + \dots$$

in which  $f(x)$  denotes the function of  $x$  to be developed and  $g(y)$  denotes the series in  $\epsilon^2$  with  $z$  replacing  $p$ . The prime denotes differentiation with respect to  $y$ .

$$f(y) = 2 \tan^{-1} e^y$$

$$f(y) = \frac{2e^y}{1+e^{2y}} = \frac{2 \tan \frac{z}{2}}{\sec^2 \frac{z}{2}} = 2 \sin \frac{z}{2} \cos \frac{z}{2} = \sin z.$$

Retaining all powers of  $\epsilon$  up to the eighth inclusive, we get:

$$g(y) = -\left(\epsilon^2 \cos z + \frac{\epsilon^4}{3} \cos^3 z + \frac{\epsilon^6}{5} \cos^5 z + \frac{\epsilon^8}{7} \cos^7 z\right)$$

$$g(y) f'(y) = -\left(\epsilon^2 \sin z \cos z + \frac{\epsilon^4}{3} \sin z \cos^3 z + \frac{\epsilon^6}{5} \sin z \cos^5 z + \frac{\epsilon^8}{7} \sin z \cos^7 z\right)$$

$$[g(y)]^2 = \epsilon^4 \cos^2 z + \frac{2\epsilon^6}{3} \cos^4 z + \frac{23\epsilon^8}{45} \cos^6 z$$

$$[g(y)]^2 f'(y) = \epsilon^4 \sin z \cos^3 z + \frac{2\epsilon^6}{3} \sin z \cos^5 z + \frac{23\epsilon^8}{45} \sin z \cos^7 z$$

$$[g(y)]^3 = -\epsilon^6 \cos^3 z - \epsilon^8 \cos^5 z,$$

$$[g(y)]^3 f'(y) = -\epsilon^6 \sin z \cos^4 z - \epsilon^8 \sin z \cos^6 z,$$

$$[g(y)]^4 = \epsilon^8 \cos^4 z,$$

$$[g(y)]^4 f'(y) = \epsilon^8 \sin z \cos^4 z.$$

To differentiate these expressions with respect to  $y$ , we may differentiate with respect to  $z$  and multiply by  $\frac{dz}{dy}$  or  $\sin z$ , since  $f(y)$  is equal to  $z$ . For successive differentiations, we differentiate with respect to  $z$  and multiply by  $\sin z$ ; then differentiate with respect to  $z$  again and multiply by  $\sin z$  again, and so on for the remaining differentiations.

With this understanding, we get by differentiation and reduction:

$$\begin{aligned} \frac{d}{dy} \{[g(y)]^2 f'(y)\} &= \epsilon^4 \sin z \cos^3 z - 2\epsilon^4 \sin^3 z \cos z + \frac{2\epsilon^6}{3} \sin z \cos^5 z \\ &\quad - \frac{8\epsilon^8}{3} \sin^3 z \cos^3 z + \frac{23\epsilon^8}{45} \sin z \cos^7 z - \frac{46\epsilon^8}{15} \sin^3 z \cos^5 z \\ &= -2\epsilon^4 \sin z \cos z + \left(3\epsilon^4 - \frac{8\epsilon^6}{3}\right) \sin z \cos^3 z \\ &\quad + \left(\frac{10\epsilon^6}{3} - \frac{46\epsilon^8}{15}\right) \sin z \cos^5 z + \frac{161\epsilon^8}{45} \sin z \cos^7 z, \end{aligned}$$

$$\begin{aligned} \frac{d^2}{dy^2}\{[g(y)]^3 f'(y)\} &= -\epsilon^6 \sin z \cos^5 z + 4\epsilon^6 \sin^3 z \cos^3 z \\ &+ 9\epsilon^6 \sin^5 z \cos z - 6\epsilon^6 \sin^7 z \\ &+ 6\epsilon^8 \sin^3 z \cos^5 z + 15\epsilon^8 \sin^5 z \cos^3 z - 20\epsilon^8 \sin^7 z \cos z \\ &= -6\epsilon^6 \sin z \cos z + (25\epsilon^8 - 20\epsilon^8) \sin z \cos^3 z - (20\epsilon^8 - 61\epsilon^8) \\ &\sin z \cos^5 z - 42\epsilon^8 \sin z \cos^7 z, \end{aligned}$$

$$\begin{aligned} \frac{d^3}{dy^3}\{[g(y)]^4 f'(y)\} &= \epsilon^8 \sin z \cos^7 z - 6\epsilon^8 \sin^3 z \cos^5 z \\ &- 51\epsilon^8 \sin^5 z \cos^3 z + 68\epsilon^8 \sin^7 z \cos z + 60\epsilon^8 \sin^9 z \\ &- 24\epsilon^8 \sin^7 z \cos z = -24\epsilon^8 \sin z \cos z + 200\epsilon^8 \sin z \cos^3 z \\ &- 385\epsilon^8 \sin z \cos^5 z + 210\epsilon^8 \sin z \cos^7 z. \end{aligned}$$

Substituting these values in Lagrange's development, we get

$$\begin{aligned} p &= z - \epsilon^2 \sin z \cos z - \frac{\epsilon^4}{3} \sin z \cos^3 z - \frac{\epsilon^6}{5} \sin z \cos^5 z - \frac{\epsilon^8}{7} \sin z \cos^7 z \\ &- \epsilon^4 \sin z \cos z + \left(\frac{3\epsilon^4}{2} - \frac{4\epsilon^6}{3}\right) \sin z \cos^3 z \\ &+ \left(\frac{5\epsilon^6}{3} - \frac{23\epsilon^8}{15}\right) \sin z \cos^5 z + \frac{161\epsilon^8}{90} \sin z \cos^7 z - \epsilon^8 \sin z \cos z \\ &+ \left(\frac{25\epsilon^8}{6} - \frac{10\epsilon^8}{3}\right) \sin z \cos^3 z - \left(\frac{10\epsilon^8}{3} - \frac{61\epsilon^8}{6}\right) \sin z \cos^5 z \\ &- 7\epsilon^8 \sin z \cos^7 z - \epsilon^8 \sin z \cos z + \frac{25\epsilon^8}{3} \sin z \cos^3 z \\ &- \frac{385\epsilon^8}{24} \sin z \cos^5 z + \frac{35\epsilon^8}{4} \sin z \cos^7 z. \end{aligned}$$

By collecting like terms, this becomes

$$\begin{aligned} p &= z - (\epsilon^2 + \epsilon^4 + \epsilon^6 + \epsilon^8) \sin z \cos z + \left(\frac{7\epsilon^4}{6} + \frac{17\epsilon^6}{6} + 5\epsilon^8\right) \sin z \cos^3 z \\ &- \left(\frac{28\epsilon^8}{15} + \frac{889\epsilon^8}{120}\right) \sin z \cos^5 z + \frac{4279\epsilon^8}{1260} \sin z \cos^7 z. \end{aligned}$$

Substituting the reductions from the table on page 88 and rearranging, we obtain the desired approximation

$$\begin{aligned} p &= z - \left(\frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360}\right) \sin 2z + \left(\frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520}\right) \sin 4z \\ &- \left(\frac{7\epsilon^8}{120} + \frac{81\epsilon^8}{1120}\right) \sin 6z + \frac{4279\epsilon^8}{161280} \sin 8z. \end{aligned}$$

In terms of  $\varphi$  and  $\chi$  this becomes, as before, the approximation

$$\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\ + \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.$$

**DEVELOPMENT OF  $\varphi - \chi$  IN TERMS OF  $\chi$ —SEVENTH METHOD.**

$\varphi - \chi$  can be developed in terms of  $\chi$  by the application of Arbogast's rule (see p. 28). The function to be developed in this case is

$$p = 2 \tan^{-1} \exp^* \left( \log_e \tan \frac{z}{2} - \frac{h}{1!} \cos p - \frac{h^2}{2!} \frac{2}{3} \cos^3 p \right. \\ \left. - \frac{h^3}{3!} \frac{6}{5} \cos^5 p - \frac{h^4}{4!} \frac{24}{7} \cos^7 p - \dots \right) = A_0 + A_1 \frac{h}{1!} \\ + A_2 \frac{h^2}{2!} + A_3 \frac{h^3}{3!} + A_4 \frac{h^4}{4!} + \dots$$

The  $A$ 's are computed as before in the forms

$$A_0 = f(a_0), \\ A_1 = a_1 f^1(a_0), \\ A_2 = a_1^2 f^2(a_0) + a_2 f^1(a_0), \\ A_3 = a_1^3 f^3(a_0) + 3a_1 a_2 f^2(a_0) + a_3 f^1(a_0), \\ A_4 = a_1^4 f^4(a_0) + 6a_1^2 a_2 f^3(a_0) + 4a_1 a_3 f^2(a_0) \\ + 3a_2^2 f^2(a_0) + a_4 f^1(a_0), \\ \text{etc.}$$

(For the necessary reductions in the following work consult the table on p. 88.)

$$f(a_0) = z, \\ f^1(a_0) = \frac{dz}{da_0};$$

but

$$a_0 = \log_e \tan \frac{z}{2}, \\ \frac{da_0}{dz} = \frac{\sec^2 \frac{z}{2}}{2 \tan \frac{z}{2}} = \frac{1}{\sin z},$$

---

\*  $\exp x = e^x$



or

$$\frac{dz}{da_0} = \sin z;$$

hence

$$f^1(a_0) = \sin z,$$

$$f^2(a_0) = \cos z \frac{dz}{da_0} = \sin z \cos z,$$

$$f^3(a_0) = \cos 2z \frac{dz}{da_0} = \sin z \cos 2z,$$

$$f^4(a_0) = (\cos z \cos 2z - 2 \sin z \sin 2z) \frac{dz}{da_0} \\ = \sin z \cos z \cos 2z - 2 \sin^2 z \sin 2z.$$

Also

$$a_1 = -\cos p,$$

$$a_2 = -\frac{2}{3} \cos^3 p,$$

$$a_3 = -\frac{6}{5} \cos^5 p,$$

$$a_4 = -\frac{24}{7} \cos^7 p.$$

The  $A$ 's could now be computed, but they would contain a combination of functions of  $z$  and of  $p$ , since the  $a$ 's are functions of  $p$ .

It is necessary, then, to approximate these functions in terms of  $z$ .  $a_1$  must include terms in  $\epsilon^6$  or  $h^3$ ;  $a_2$ , in  $h^2$ ; and  $a_3$ , terms in  $h$ .  $a_4$  needs only to have  $p$  replaced by  $z$ . In order to obtain this approximation we must develop the function

$$f(p) = \cos [2 \tan^{-1} \exp (\log_e \tan \frac{z}{2} - \frac{h}{1!} \cos p - \frac{h^2}{2!} \frac{2}{3} \cos^3 p \\ - \frac{h^3}{3!} \frac{6}{5} \cos^5 p - \dots)] = A_0 + A_1 \frac{h}{1!} + A_2 \frac{h^2}{2!} + A_3 \frac{h^3}{3!} + \dots$$

We have now

$$a_0 = \log_e \tan \frac{z}{2}, \\ \frac{da_0}{dz} = \frac{1}{\sin z},$$

or,

$$\begin{aligned}\frac{dz}{da_0} &= \sin z, \\ f(a_0) &= \cos z, \\ f^1(a_0) &= -\sin z \frac{dz}{da_0} = -\sin^2 z, \\ f^2(a_0) &= -\sin 2z \frac{dz}{da_0} = -\sin z \sin 2z, \\ f^3(a_0) &= (-\cos z \sin 2z - 2 \sin z \cos 2z) \frac{dz}{da_0} \\ &= -\sin z \cos z \sin 2z - 2 \sin^2 z \cos 2z.\end{aligned}$$

Also

$$\begin{aligned}a_1 &= -\cos p, \\ a_2 &= -\frac{2}{3} \cos^3 p, \\ a_3 &= -\frac{6}{5} \cos^5 p.\end{aligned}$$

Therefore

$$\begin{aligned}A_0 &= \cos z, \\ A_1 &= \sin^2 z \cos p, \\ A_2 &= (\sin z \sin 2z \cos^2 p + \frac{2}{3} \sin^2 z) \cos^3 p, \\ A_3 &= (\sin z \cos z \sin 2z + 2 \sin^2 z \cos 2z) \cos^3 p \\ &\quad - 2 \sin z \sin 2z \cos^4 p + \frac{6}{5} \sin^2 z \cos^5 p.\end{aligned}$$

By substituting these values, we obtain

$$\begin{aligned}\cos p &= \cos z + \frac{h}{1!} \sin^2 z \cos p + \frac{h^2}{2!} (-\sin z \sin 2z \cos^2 p \\ &\quad + \frac{2}{3} \sin^2 z \cos^3 p) + \frac{h^3}{3!} [(\sin z \cos z \sin 2z \\ &\quad + 2 \sin^2 z \cos 2z) \cos^3 p - 2 \sin z \sin 2z \cos^4 p \\ &\quad + \frac{6}{5} \sin^2 z \cos^5 p].\end{aligned}$$

As an approximation with the first power of  $h$ , we get

$$\cos p = \cos z + h \sin^2 z \cos z.$$

Substituting this in the above expression for  $\cos p$  and retaining the second powers of  $h$ , we get

$$\cos p = \cos z + h \sin^2 z \cos z + h^2 \sin^4 z \cos z \\ + \frac{h^2}{2} \left( -\sin z \sin 2z \cos^2 z + \frac{2}{3} \sin^2 z \cos^3 z \right).$$

Finally, substituting this approximation in the expression for  $\cos p$  and retaining all third powers of  $h$ , we get the required approximation

$$\cos p = \cos z + h \sin^2 z \cos z + h^2 \sin^4 z \cos z + h^3 \sin^6 z \cos z \\ + \frac{h^3}{2} \left( -\sin^3 z \sin 2z \cos^2 z + \frac{2}{3} \sin^4 z \cos^3 z \right) \\ + \frac{h^2}{2} \left( -\sin z \sin 2z \cos^2 z \right) + h^3 \left( -\sin^3 z \sin 2z \cos^2 z \right) \\ + \frac{h^2}{3} \sin^2 z \cos^3 z + h^3 \sin^4 z \cos^3 z \\ + \frac{h^3}{6} \left( \sin z \cos^4 z \sin 2z + 2 \sin^2 z \cos^3 z \cos 2z \right. \\ \left. - 2 \sin z \cos^4 z \sin 2z + \frac{6}{5} \sin^2 z \cos^5 z \right),$$

or

$$\cos p = \cos z + h \sin^2 z \cos z + h^2 \left( \cos z - \frac{8}{3} \cos^3 z + \frac{5}{3} \cos^5 z \right) \\ + h^3 \left( \cos z - 5 \cos^3 z + \frac{36}{5} \cos^5 z - \frac{16}{5} \cos^7 z \right), \\ \cos^3 p = \cos^3 z + 3h \sin^2 z \cos^3 z + h^2 \left( 6 \cos^3 z - 14 \cos^5 z \right. \\ \left. + 8 \cos^7 z \right), \\ \cos^5 p = \cos^5 z + 5h \sin^2 z \cos^5 z, \\ \cos^7 p = \cos^7 z.$$

If these values are substituted in the expressions for the  $a$ 's on page 56, we get

$$a_1 = - \left[ \cos z + h \sin^2 z \cos z + h^2 \left( \cos z - \frac{8}{3} \cos^3 z + \frac{5}{3} \cos^5 z \right) \right. \\ \left. + h^3 \left( \cos z - 5 \cos^3 z + \frac{36}{5} \cos^5 z - \frac{16}{5} \cos^7 z \right) \right], \\ a_2 = - \frac{2}{3} \left[ \cos^3 z + 3h \sin^2 z \cos^3 z + h^2 \left( 6 \cos^3 z - 14 \cos^5 z \right. \right. \\ \left. \left. + 8 \cos^7 z \right) \right],$$

$$a_3 = -\frac{6}{5} (\cos^5 z + 5h \sin^2 z \cos^5 z),$$

$$a_4 = -\frac{24}{7} \cos^7 z.$$

With these values and the values of the derivatives of  $f(a_0)$  on page 56, we get by retaining all requisite powers of  $h$  the following approximations

$$A_0 = z,$$

$$A_1 = -[\sin z \cos z + h \sin^3 z \cos z + h^2 (\sin z \cos z - \frac{8}{3} \sin z \cos^3 z + \frac{5}{3} \sin z \cos^5 z) + h^3 (\sin z \cos z - 5 \sin z \cos^3 z + \frac{36}{5} \sin z \cos^5 z - \frac{16}{5} \sin z \cos^7 z)],$$

$$A_2 = \sin z \cos^3 z + 2h \sin^3 z \cos^3 z + h^2 (3 \sin z \cos^3 z - \frac{22}{3} \sin z \cos^5 z + \frac{13}{3} \sin z \cos^7 z) - \frac{2}{3} [\sin z \cos^3 z + 3h \sin^3 z \cos^3 z + h^2 (6 \sin z \cos^3 z - 14 \sin z \cos^5 z + 8 \sin z \cos^7 z)],$$

$$A_3 = -(\sin z \cos^3 z \cos 2z + 3h \sin^3 z \cos^3 z \cos 2z) + 2(\sin z \cos^5 z + 4h \sin^3 z \cos^5 z) - \frac{6}{5} (\sin z \cos^5 z + 5h \sin^3 z \cos^5 z),$$

$$A_4 = \sin z \cos^5 z \cos 2z - 2 \sin^2 z \cos^4 z \sin 2z - 4 \sin z \cos^5 z \cos 2z + \frac{24}{5} \sin z \cos^7 z + \frac{4}{3} \sin z \cos^7 z - \frac{24}{7} \sin z \cos^7 z.$$

Substituting these values and reducing by use of the table on p. 88, we get the approximation

$$p = z - \frac{h}{1!} \left[ \sin z \cos z + h \sin z \cos z - h \sin z \cos^3 z + h^2 \left( \sin z \cos z - \frac{8}{3} \sin z \cos^3 z + \frac{5}{3} \sin z \cos^5 z \right) + h^3 \left( \sin z \cos z - 5 \sin z \cos^3 z + \frac{36}{5} \sin z \cos^5 z \right) \right]$$

$$\begin{aligned}
& -\frac{16}{5} \sin z \cos^7 z \Big] + \frac{h^2}{2!} \left[ \frac{1}{3} \sin z \cos^3 z - h^2 (\sin z \cos^3 z \right. \\
& - 2 \sin z \cos^5 z + \sin z \cos^7 z) \Big] + \frac{h^3}{3!} \left[ \sin z \cos^3 z \right. \\
& - \frac{6}{5} \sin z \cos^5 z + h (3 \sin z \cos^3 z - 7 \sin z \cos^5 z \\
& + 4 \sin z \cos^7 z) \Big] + \frac{h^4}{4!} \left( -\sin z \cos^5 z + \frac{74}{105} \sin z \cos^7 z \right)
\end{aligned}$$

Rearranging this in powers of  $h$  or  $\epsilon^2$ , we get

$$\begin{aligned}
p = z - \epsilon^2 \sin z \cos z + \epsilon^4 \left( -\sin z \cos z + \frac{7}{6} \sin z \cos^3 z \right) \\
+ \epsilon^6 \left( -\sin z \cos z + \frac{17}{6} \sin z \cos^3 z - \frac{28}{15} \sin z \cos^5 z \right) \\
+ \epsilon^8 \left( -\sin z \cos z + 5 \sin z \cos^3 z - \frac{889}{120} \sin z \cos^5 z \right. \\
\left. + \frac{4279}{1260} \sin z \cos^7 z \right).
\end{aligned}$$

Making the reductions by use of the table on p. 88 and rearranging, we get the approximation

$$\begin{aligned}
p = z - \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2z + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4z \\
- \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6z + \frac{4279\epsilon^8}{161280} \sin 8z.
\end{aligned}$$

In terms of  $\varphi$  and  $\chi$  this becomes, as before, the approximation sought

$$\begin{aligned}
\varphi - \chi = \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} \right) \sin 2\chi + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} \right) \sin 4\chi \\
+ \left( \frac{7\epsilon^6}{120} + \frac{81\epsilon^8}{1120} \right) \sin 6\chi + \frac{4279\epsilon^8}{161280} \sin 8\chi.
\end{aligned}$$

#### DEVELOPMENT OF $\varphi - \beta$ IN TERMS OF $\varphi$ —FIRST METHOD.

In the equation of definition of aithalic latitude (see p. 12), if the fractional part is divided out up to and including the term in  $\epsilon^8$ , we get

$$\begin{aligned}
\sin \beta = \sin \varphi \left[ 1 - \frac{2\epsilon^2}{3} \cos^2 \varphi - \left( \frac{7}{45} \cos^2 \varphi + \frac{3}{5} \sin^2 \varphi \cos^2 \varphi \right) \epsilon^4 \right. \\
\left. - \left( \frac{64}{945} \cos^2 \varphi + \frac{6}{35} \sin^2 \varphi \cos^2 \varphi + \frac{4}{7} \sin^4 \varphi \cos^2 \varphi \right) \epsilon^6 + \dots \right].
\end{aligned}$$

Now let

$$\sin \beta = a \sin \varphi,$$

then

$$\tan \beta = \frac{a \tan \varphi}{[1 + (1 - a^2) \tan^2 \varphi]^{\frac{1}{2}}}.$$

Assume

$$\tan \beta = (1 - b) \tan \varphi,$$

then

$$\tan (\varphi - \beta) = \frac{b \sin 2\varphi}{2 - b + b \cos 2\varphi}.$$

If

$$q = \frac{b}{2 - b} = \frac{b}{2} + \frac{b^2}{4} + \frac{b^3}{8} + \frac{b^4}{16} + \dots$$

we get, as in former developments (see p. 13):

$$\varphi - \beta = q \sin 2\varphi - \frac{q^2}{2} \sin 4\varphi + \frac{q^3}{3} \sin 6\varphi - \dots$$

Now

$$a = 1 - \frac{2\epsilon^2}{3} \cos^2 \varphi - \left( \frac{7}{45} \cos^2 \varphi + \frac{3}{5} \sin^2 \varphi \cos^2 \varphi \right) \epsilon^4 \\ - \left( \frac{64}{945} \cos^2 \varphi + \frac{6}{35} \sin^2 \varphi \cos^2 \varphi + \frac{4}{7} \sin^4 \varphi \cos^2 \varphi \right) \epsilon^6 + \dots$$

or arranged in powers of  $\cos^2 \varphi$ , this becomes

$$a = 1 - \left( \frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945} \right) \cos^2 \varphi + \left( \frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35} \right) \cos^4 \varphi \\ - \frac{4\epsilon^6}{7} \cos^6 \varphi.$$

$$1 - b = \frac{a}{[1 + (1 - a^2) \tan^2 \varphi]^{\frac{1}{2}}}$$

$$= a \left[ 1 - \frac{1}{2} (1 - a^2) \tan^2 \varphi + \frac{3}{8} (1 - a^2)^2 \tan^4 \varphi \right.$$

$$\left. - \frac{5}{16} (1 - a^2)^3 \tan^6 \varphi + \dots \right)$$

$$a^2 = 1 - \left( \frac{4\epsilon^2}{3} + \frac{68\epsilon^4}{45} + \frac{1532\epsilon^6}{945} \right) \cos^2 \varphi + \left( \frac{74\epsilon^4}{45} + \frac{3436\epsilon^6}{945} \right) \cos^4 \varphi$$

$$- \frac{68\epsilon^6}{35} \cos^6 \varphi$$

$$(1 - a^2) \tan^2 \varphi = \left( \frac{4\epsilon^2}{3} + \frac{68\epsilon^4}{45} + \frac{1532\epsilon^6}{945} \right) \sin^2 \varphi$$

$$- \left( \frac{74\epsilon^4}{45} + \frac{3436\epsilon^6}{945} \right) \sin^2 \varphi \cos^2 \varphi + \frac{68\epsilon^6}{35} \sin^2 \varphi \cos^4 \varphi,$$

or, when arranged in powers of  $\cos^2 \varphi$ ,

$$(1-a^2) \tan^2 \varphi = \left( \frac{4\epsilon^2}{3} + \frac{68\epsilon^4}{45} + \frac{1532\epsilon^6}{945} \right) - \left( \frac{4\epsilon^2}{3} + \frac{142\epsilon^4}{45} + \frac{184\epsilon^6}{35} \right) \cos^2 \varphi + \left( \frac{74\epsilon^4}{45} + \frac{5272\epsilon^6}{945} \right) \cos^4 \varphi - \frac{68\epsilon^6}{35} \cos^6 \varphi,$$

$$[(1-a^2) \tan^2 \varphi]^2 = \frac{16\epsilon^4}{9} + \frac{544\epsilon^6}{135} - \left( \frac{32\epsilon^4}{9} + \frac{112\epsilon^6}{9} \right) \cos^2 \varphi + \left( \frac{16\epsilon^4}{9} + \frac{64\epsilon^6}{5} \right) \cos^4 \varphi - \frac{592\epsilon^6}{135} \cos^6 \varphi,$$

$$[(1-a^2) \tan^2 \varphi]^3 = \frac{64\epsilon^6}{27} - \frac{64\epsilon^6}{9} \cos^2 \varphi + \frac{64\epsilon^6}{9} \cos^4 \varphi - \frac{64\epsilon^6}{27} \cos^6 \varphi,$$

$$\frac{1}{[1+(1-a^2) \tan^2 \varphi]^{\frac{1}{2}}} = 1 - \left( \frac{2\epsilon^2}{3} + \frac{4\epsilon^4}{45} + \frac{38\epsilon^6}{945} \right) + \left( \frac{2\epsilon^2}{3} + \frac{11\epsilon^4}{45} + \frac{58\epsilon^6}{315} \right) \cos^2 \varphi - \left( \frac{7\epsilon^4}{45} + \frac{40\epsilon^6}{189} \right) \cos^4 \varphi + \frac{64\epsilon^6}{945} \cos^6 \varphi,$$

$$\frac{a}{[1+(1-a^2) \tan^2 \varphi]^{\frac{1}{2}}} = 1 - \left( \frac{2\epsilon^2}{3} + \frac{4\epsilon^4}{45} + \frac{38\epsilon^6}{945} \right) - \left( \frac{\epsilon^4}{15} + \frac{4\epsilon^6}{63} \right) \cos^2 \varphi + \frac{34\epsilon^6}{945} \cos^4 \varphi.$$

Therefore

$$b = \frac{2\epsilon^2}{3} + \frac{4\epsilon^4}{45} + \frac{38\epsilon^6}{945} + \left( \frac{\epsilon^4}{15} + \frac{4\epsilon^6}{63} \right) \cos^2 \varphi - \frac{34\epsilon^6}{945} \cos^4 \varphi.$$

But to the approximation required, we have

$$\varphi - \beta = \left( \frac{b}{2} + \frac{b^2}{4} + \frac{b^3}{8} \right) \sin 2 \varphi - \left( \frac{b^2}{8} + \frac{b^3}{8} \right) \sin 4 \varphi + \frac{b^3}{24} \sin 6 \varphi.$$

$$b^2 = \frac{4\epsilon^4}{9} + \frac{16\epsilon^6}{135} + \frac{4\epsilon^6}{45} \cos^2 \varphi,$$

$$b^3 = \frac{8\epsilon^6}{27}.$$

$$\varphi - \beta = \left[ \frac{\epsilon^2}{3} + \frac{7\epsilon^4}{45} + \frac{82\epsilon^6}{945} + \left( \frac{\epsilon^4}{30} + \frac{17\epsilon^6}{315} \right) \cos^2 \varphi - \frac{17\epsilon^6}{945} \cos^4 \varphi \right] \sin 2 \varphi - \left( \frac{\epsilon^4}{18} + \frac{7\epsilon^6}{135} + \frac{\epsilon^6}{90} \cos^2 \varphi \right) \sin 4 \varphi + \frac{\epsilon^6}{81} \sin 6 \varphi,$$

or, finally, on reduction (for reductions, see table p. 88) we get the approximation

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2 \varphi - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4 \varphi \\ & + \frac{383\epsilon^8}{45360} \sin 6 \varphi. \end{aligned}$$

**DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\varphi$ —SECOND METHOD**

The expansion of  $\beta$  in terms of  $\varphi$  can be carried through in a somewhat shorter way by the following method:

Set  $\epsilon^2 = h$  and the equation for  $\sin \beta$  becomes (see p. 60)

$$\begin{aligned} \sin \beta = \sin \varphi \left[ 1 - \frac{2}{3} h \cos^2 \varphi - \left( \frac{7}{45} \cos^2 \varphi + \frac{3}{5} \sin^2 \varphi \cos^2 \varphi \right) h^2 \right. \\ \left. - \left( \frac{64}{945} \cos^2 \varphi + \frac{6}{35} \sin^2 \varphi \cos^2 \varphi + \frac{4}{7} \sin^4 \varphi \cos^2 \varphi \right) h^3 \right. \\ \left. - \dots \right] \end{aligned}$$

Differentiating this expression, considering  $\beta$  as a function of  $h$ , we get in succession

$$\begin{aligned} \cos \beta \frac{d\beta}{dh} = \sin \varphi \left[ -\frac{2}{3} \cos^2 \varphi - \left( \frac{14}{45} \cos^2 \varphi + \frac{6}{5} \sin^2 \varphi \cos^2 \varphi \right) h \right. \\ \left. - \left( \frac{64}{315} \cos^2 \varphi + \frac{18}{35} \sin^2 \varphi \cos^2 \varphi + \frac{12}{7} \sin^4 \varphi \cos^2 \varphi \right) h^2 \right], \\ -\sin \beta \left( \frac{d\beta}{dh} \right)^2 + \cos \beta \frac{d^2\beta}{dh^2} = \sin \varphi \left[ -\left( \frac{14}{45} \cos^2 \varphi + \frac{6}{5} \sin^2 \varphi \cos^2 \varphi \right) \right. \\ \left. - \left( \frac{128}{315} \cos^2 \varphi + \frac{36}{35} \sin^2 \varphi \cos^2 \varphi + \frac{24}{7} \sin^4 \varphi \cos^2 \varphi \right) h \right], \\ -\cos \beta \left( \frac{d\beta}{dh} \right)^3 - 3 \sin \beta \frac{d\beta}{dh} \frac{d^2\beta}{dh^2} + \cos \beta \frac{d^3\beta}{dh^3} \\ = -\frac{128}{315} \sin \varphi \cos^2 \varphi - \frac{36}{35} \sin^3 \varphi \cos^2 \varphi - \frac{24}{7} \sin^5 \varphi \cos^2 \varphi. \end{aligned}$$

These expressions must now be evaluated for  $h = 0$ .  
(For the necessary reductions see the reduction table, p. 88.)



Denoting the value for  $h=0$  by brackets we get

$$[\beta] = \varphi,$$

$$\left[\frac{d\beta}{dh}\right] = -\frac{2}{3} \sin \varphi \cos \varphi = -\frac{1}{3} \sin 2\varphi,$$

$$\begin{aligned} \left[\frac{d^2\beta}{dh^2}\right] &= -\frac{14}{45} \sin \varphi \cos \varphi - \frac{34}{45} \sin^3 \varphi \cos \varphi, \\ &= -\frac{31}{90} \sin 2\varphi + \frac{17}{180} \sin 4\varphi, \end{aligned}$$

$$\begin{aligned} \left[\frac{d^3\beta}{dh^3}\right] &= -\frac{128}{315} \sin \varphi \cos \varphi - \frac{664}{945} \sin^3 \varphi \cos \varphi - \frac{1532}{945} \sin^5 \varphi \cos \varphi \\ &= -\frac{177}{280} \sin 2\varphi + \frac{61}{210} \sin 4\varphi - \frac{383}{7560} \sin 6\varphi. \end{aligned}$$

By Maclaurin's series we have, on replacing  $h$  by  $\epsilon^2$ ,

$$\beta = [\beta] + \frac{\epsilon^2}{1!} \left[\frac{d\beta}{dh}\right] + \frac{\epsilon^4}{2!} \left[\frac{d^2\beta}{dh^2}\right] + \frac{\epsilon^6}{3!} \left[\frac{d^3\beta}{dh^3}\right] + \dots$$

By substituting the values in this expansion we obtain the desired approximation

$$\begin{aligned} \beta = \varphi - \frac{\epsilon^2}{3} \sin 2\varphi - \frac{31\epsilon^4}{180} \sin 2\varphi + \frac{17\epsilon^4}{360} \sin 4\varphi - \frac{59\epsilon^6}{560} \sin 2\varphi \\ + \frac{61\epsilon^6}{1260} \sin 4\varphi - \frac{383\epsilon^6}{45360} \sin 6\varphi, \end{aligned}$$

or, as before, we obtain the approximation

$$\begin{aligned} \varphi - \beta = \left(\frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560}\right) \sin 2\varphi - \left(\frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260}\right) \sin 4\varphi \\ + \frac{383\epsilon^6}{45360} \sin 6\varphi. \end{aligned}$$

#### DEVELOPMENT OF $\varphi - \beta$ IN TERMS OF $\varphi$ —THIRD METHOD.

We can develop the authalic latitude in terms of  $\varphi$  by a method similar to that used for the isometric latitude on page 18.

$$\sin(\varphi + h) = \sin \varphi \cos h + \cos \varphi \sin h.$$

If we assume

$$h = a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + \dots,$$

and if we wish to carry the approximation only far enough to include the sixth powers of  $\epsilon$ , we get

$$\sin(\varphi + h) = \left(1 - \frac{h^2}{2}\right) \sin \varphi + \left(h - \frac{h^3}{6}\right) \cos \varphi.$$

After substitution of the value of  $h$  we obtain the approximation

$$\sin(\varphi + h) = \left(1 - \frac{a^2\epsilon^4}{2} - ab\epsilon^6\right) \sin \varphi + \left(a\epsilon^2 + b\epsilon^4 + c\epsilon^6 - \frac{a^3\epsilon^6}{6}\right) \cos \varphi.$$

Now, letting

$$\beta = \varphi + h = \varphi + a\epsilon^2 + b\epsilon^4 + c\epsilon^6 + \dots,$$

we get

$$\sin \beta = \left(1 - \frac{a^2\epsilon^4}{2} - ab\epsilon^6\right) \sin \varphi + \left(a\epsilon^2 + b\epsilon^4 + c\epsilon^6 - \frac{a^3\epsilon^6}{6}\right) \cos \varphi.$$

If the equation of definition of authalic latitude is reduced to the form approximated to  $\epsilon^6$ , inclusive,

$$\sin \beta = \sin \varphi \left[ 1 - \left(\frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945}\right) \cos^2 \varphi + \left(\frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35}\right) \cos^4 \varphi - \frac{4\epsilon^6}{7} \cos^6 \varphi \right],$$

we may equate the coefficients of like powers of  $\epsilon$  in the two series, since the two series must be identically equal. In this way we may obtain equations for the determinations of the values of  $a$ ,  $b$ , and  $c$ .

$$a \cos \varphi = -\frac{2}{3} \sin \varphi \cos^2 \varphi,$$

$$-\frac{a^2}{2} \sin \varphi + b \cos \varphi = -\frac{34}{45} \sin \varphi \cos^2 \varphi + \frac{3}{5} \sin \varphi \cos^4 \varphi,$$

$$-ab \sin \varphi + c \cos \varphi - \frac{a^3}{6} \cos \varphi = -\frac{766}{945} \sin \varphi \cos^2 \varphi$$

$$+ \frac{46}{35} \sin \varphi \cos^4 \varphi - \frac{4}{7} \sin \varphi \cos^6 \varphi.$$

From these equations we obtain the values (for the necessary reductions see the reduction table, p. 88).

$$\begin{aligned}
 a &= -\frac{2}{3} \sin \varphi \cos \varphi = -\frac{1}{3} \sin 2 \varphi, \\
 b &= -\frac{8}{15} \sin \varphi \cos \varphi + \frac{17}{45} \sin \varphi \cos^3 \varphi = -\frac{31}{180} \sin 2 \varphi + \frac{17}{360} \sin 4 \varphi, \\
 c &= -\frac{86}{189} \sin \varphi \cos \varphi + \frac{1864}{2835} \sin \varphi \cos^3 \varphi - \frac{766}{2835} \sin \varphi \cos^5 \varphi \\
 &= -\frac{59}{560} \sin 2 \varphi + \frac{61}{1260} \sin 4 \varphi - \frac{383}{45360} \sin 6 \varphi,
 \end{aligned}$$

When these values are substituted and rearranged we get, as before, the approximation

$$\begin{aligned}
 \varphi - \beta &= \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2 \varphi - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4 \varphi \\
 &\quad + \frac{383\epsilon^6}{45360} \sin 6 \varphi.
 \end{aligned}$$

#### DEVELOPMENT OF $\varphi - \beta$ IN TERMS OF $\varphi$ —FOURTH METHOD.

The development of  $\varphi - \beta$  in terms of  $\beta$  can first be made by the third, fourth, or fifth method (see pp. 72-79), and then this expression may be changed into terms of  $\varphi$  by Lagrange's theorem.

We are given the approximation

$$\begin{aligned}
 \beta = \varphi - \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2 \beta - \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4 \beta \\
 - \frac{761\epsilon^6}{45360} \sin 6 \beta.
 \end{aligned}$$

By Lagrange's theorem we have

$$\beta = \varphi + \frac{1}{1!} g'(\varphi) + \frac{1}{2!} \frac{d}{d\varphi} [g'(\varphi)]^2 + \frac{1}{3!} \frac{d^2}{d\varphi^2} [g'(\varphi)]^3 + \dots,$$

in which

$$\begin{aligned}
 g'(\varphi) &= -\left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2 \varphi - \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4 \varphi \\
 &\quad - \frac{761\epsilon^6}{45360} \sin 6 \varphi.
 \end{aligned}$$

By squaring this expression, we get

$$[g(\varphi)]^2 = \left(\frac{\epsilon^4}{9} + \frac{31\epsilon^6}{270}\right) \sin^2 2\varphi + \frac{23\epsilon^8}{540} \sin 2\varphi \sin 4\varphi,$$

and by cubing it we obtain

$$[g(\varphi)]^3 = -\frac{\epsilon^6}{27} \sin^3 2\varphi.$$

Differentiating and reducing by the table on p. 88, we get

$$\begin{aligned} \frac{d}{d\varphi} [g(\varphi)]^2 &= \left(\frac{4\epsilon^4}{9} + \frac{62\epsilon^6}{135}\right) \sin 2\varphi \cos 2\varphi + \frac{23\epsilon^8}{270} \cos 2\varphi \sin 4\varphi \\ &\quad + \frac{23\epsilon^8}{135} \sin 2\varphi \cos 4\varphi \\ &= -\frac{23\epsilon^8}{540} \sin 2\varphi + \left(\frac{2\epsilon^4}{9} + \frac{31\epsilon^6}{135}\right) \sin 4\varphi + \frac{23\epsilon^8}{180} \sin 6\varphi, \\ \frac{d^2}{d\varphi^2} [g(\varphi)]^2 &= \frac{\epsilon^6}{9} \sin 2\varphi - \frac{\epsilon^6}{3} \sin 6\varphi. \end{aligned}$$

Substituting these values in Lagrange's series, we get the approximation

$$\begin{aligned} \beta = \varphi &- \left(\frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040}\right) \sin 2\varphi - \left(\frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780}\right) \sin 4\varphi \\ &- \frac{761\epsilon^6}{45360} \sin 6\varphi - \frac{23\epsilon^8}{1080} \sin 2\varphi + \left(\frac{\epsilon^4}{9} + \frac{31\epsilon^6}{270}\right) \sin 4\varphi \\ &+ \frac{23\epsilon^8}{360} \sin 6\varphi + \frac{\epsilon^6}{54} \sin 2\varphi - \frac{\epsilon^6}{18} \sin 6\varphi. \end{aligned}$$

By collecting and rearranging we get, as before, the approximation

$$\begin{aligned} \varphi - \beta &= \left(\frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560}\right) \sin 2\varphi - \left(\frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260}\right) \sin 4\varphi \\ &\quad + \frac{383\epsilon^6}{45360} \sin 6\varphi. \end{aligned}$$

DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\varphi$ —FIFTH METHOD.

$\varphi - \beta$  can be developed in terms of  $\varphi$  by Arbogast's rule (see p. 28). In this case the function to be developed is

$$\begin{aligned} \beta &= \sin^{-1} \left[ \sin \varphi - \frac{h}{1!} \frac{2}{3} \sin \varphi \cos^2 \varphi - \frac{h^2}{2!} \left( \frac{14}{45} \sin \varphi \cos^2 \varphi \right. \right. \\ &\quad \left. \left. + \frac{6}{5} \sin^3 \varphi \cos^2 \varphi \right) - \frac{h^3}{3!} \left( \frac{128}{315} \sin \varphi \cos^2 \varphi \right. \right. \\ &\quad \left. \left. + \frac{36}{35} \sin^3 \varphi \cos^2 \varphi + \frac{24}{7} \sin^5 \varphi \cos^2 \varphi \right) + \dots \dots \right] \\ &= A_0 + A_1 \frac{h}{1!} + A_2 \frac{h^2}{2!} + A_3 \frac{h^3}{3!} + \dots \dots \dots \end{aligned}$$

with the  $A$ 's defined as before.

$$A_0 = f(a_0),$$

$$A_1 = a_1 f^1(a_0),$$

$$A_2 = a_1^2 f^2(a_0) + a_2 f^1(a_0),$$

$$A_3 = a_1^3 f^3(a_0) + 3a_1 a_2 f^2(a_0) + a_3 f^1(a_0),$$

etc.

In this function we have

$$a_0 = \sin \varphi,$$

$$\frac{da_0}{d\varphi} = \cos \varphi,$$

or

$$\frac{d\varphi}{da_0} = \sec \varphi.$$

$$f(a_0) = \varphi,$$

$$f^1(a_0) = \frac{d\varphi}{da_0} = \sec \varphi,$$

$$f^2(a_0) = \sec \varphi \tan \varphi \frac{d\varphi}{da_0} = \sec^2 \varphi \tan \varphi,$$

$$f^3(a_0) = (2 \sec^2 \varphi \tan^2 \varphi + \sec^4 \varphi) \frac{d\varphi}{da_0} = 2 \sec^3 \varphi \tan^2 \varphi + \sec^5 \varphi,$$

$$a_1 = -\frac{2}{3} \sin \varphi \cos^2 \varphi,$$

$$a_2 = -\frac{14}{45} \sin \varphi \cos^2 \varphi - \frac{6}{5} \sin^3 \varphi \cos^2 \varphi,$$

$$a_3 = -\frac{128}{315} \sin \varphi \cos^2 \varphi - \frac{36}{35} \sin^3 \varphi \cos^2 \varphi - \frac{24}{7} \sin^5 \varphi \cos^2 \varphi.$$

Substituting these values in the expressions for the  $A$ 's and reducing by aid of the table on page 88, we get

$$A_0 = \varphi,$$

$$A_1 = -\frac{2}{3} \sin \varphi \cos \varphi = -\frac{1}{3} \sin 2\varphi,$$

$$\begin{aligned} A_2 &= \frac{4}{9} \sin^3 \varphi \cos \varphi - \frac{14}{45} \sin \varphi \cos \varphi - \frac{6}{5} \sin^3 \varphi \cos \varphi \\ &= -\frac{16}{15} \sin \varphi \cos \varphi + \frac{34}{45} \sin \varphi \cos^3 \varphi \\ &= -\frac{31}{90} \sin 2\varphi + \frac{17}{180} \sin 4\varphi, \end{aligned}$$

$$\begin{aligned} A_3 &= -\frac{8}{27} \sin^3 \varphi \cos^3 \varphi (2 \sec^3 \varphi \tan^2 \varphi + \sec^5 \varphi) \\ &\quad + 2 \sin \varphi \cos^2 \varphi \left( \frac{14}{45} \sin \varphi \cos^2 \varphi \right. \\ &\quad \left. + \frac{6}{5} \sin^3 \varphi \cos^2 \varphi \right) \sec^2 \varphi \tan \varphi \\ &\quad - \left( \frac{128}{315} \sin \varphi \cos^2 \varphi + \frac{36}{35} \sin^3 \varphi \cos^2 \varphi + \frac{24}{7} \sin^5 \varphi \cos^2 \varphi \right) \sec \varphi \\ &= -\frac{16}{27} \sin^5 \varphi \cos \varphi - \frac{8}{27} \sin^3 \varphi \cos \varphi + \frac{28}{45} \sin^3 \varphi \cos \varphi \\ &\quad + \frac{12}{5} \sin^5 \varphi \cos \varphi - \frac{128}{315} \sin \varphi \cos \varphi - \frac{36}{35} \sin^3 \varphi \cos \varphi \\ &\quad - \frac{24}{7} \sin^5 \varphi \cos \varphi \\ &= -\frac{128}{315} \sin \varphi \cos \varphi - \frac{664}{945} \sin^3 \varphi \cos \varphi - \frac{1532}{945} \sin^5 \varphi \cos \varphi \\ &= -\frac{177}{280} \sin 2\varphi + \frac{61}{210} \sin 4\varphi - \frac{383}{7560} \sin 6\varphi. \end{aligned}$$

Substituting these values for the  $A$ 's in the development and replacing  $h$  by  $\epsilon^2$ , we get, after rearrangement, the value obtained by the other methods as the approximation desired.

$$\begin{aligned} \varphi - \beta &= \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2\varphi - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\varphi \\ &\quad + \frac{383\epsilon^8}{45360} \sin 6\varphi. \end{aligned}$$

DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\beta$ —FIRST METHOD.

This quantity can now be expressed in terms of  $\beta$  by the application of Lagrange's series (see page 32). In this case

$$f(\varphi) = \left( \frac{\epsilon^4}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin \varphi - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\varphi \\ + \frac{383\epsilon^6}{45360} \sin 6\varphi.$$

Squaring this and reducing by aid of the table on page 88, we get

$$[f(\varphi)]^2 = \frac{\epsilon^4}{18} + \frac{31\epsilon^6}{540} - \frac{17\epsilon^8}{1080} \cos 2\varphi - \left( \frac{\epsilon^4}{18} + \frac{31\epsilon^6}{540} \right) \cos 4\varphi \\ + \frac{17\epsilon^8}{1080} \cos 6\varphi.$$

also by cubing and reducing

$$[f(\varphi)]^3 = \frac{\epsilon^6}{36} \sin 2\varphi - \frac{\epsilon^8}{108} \sin 6\varphi. \\ \frac{d}{d\beta} [f(\beta)]^2 = \frac{17\epsilon^6}{540} \sin \beta + \left( \frac{2\epsilon^4}{9} + \frac{31\epsilon^6}{135} \right) \sin 4\beta - \frac{17\epsilon^8}{180} \sin 6\beta, \\ \frac{d^2}{d\beta^2} [f(\beta)]^2 = -\frac{\epsilon^6}{9} \sin 2\beta + \frac{\epsilon^8}{3} \sin 6\beta.$$

Substituting these values in Lagrange's series, we obtain the approximation

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2\beta - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\beta \\ + \frac{383\epsilon^6}{45360} \sin 6\beta + \frac{17\epsilon^8}{1080} \sin 2\beta + \left( \frac{\epsilon^4}{9} + \frac{31\epsilon^6}{270} \right) \sin 4\beta \\ - \frac{17\epsilon^8}{360} \sin 6\beta - \frac{\epsilon^6}{54} \sin 2\beta + \frac{\epsilon^8}{18} \sin 6\beta,$$

or, after collecting similar terms, the approximation

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4\beta \\ + \frac{761\epsilon^6}{45360} \sin 6\beta.$$

DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\beta$ —SECOND METHOD.

In the series for  $\varphi - \beta$  in terms of  $\varphi$  (see p. 69), let  $\varphi = \beta + x$ . Then

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin (2\beta + 2x) \\ - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin (4\beta + 4x) + \frac{383\epsilon^8}{45360} \sin (6\beta + 6x),$$

or

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) (\sin 2\beta \cos 2x + \cos 2\beta \sin 2x) \\ - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) (\sin 4\beta \cos 4x + \cos 4\beta \sin 4x) \\ + \frac{383\epsilon^8}{45360} (\sin 6\beta \cos 6x + \cos 6\beta \sin 6x),$$

or, including all terms in  $\epsilon^6$ ,

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) (1 - 2x^2) \sin 2\beta + \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} \right) 2x \cos 2\beta \\ - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\beta - \frac{17\epsilon^4}{360} 4x \cos 4\beta + \frac{383\epsilon^8}{45360} \sin 6\beta.$$

But

$$x = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2\varphi - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\varphi \\ + \frac{383\epsilon^8}{45360} \sin 6\varphi.$$

Substituting this value and retaining all sixth powers of  $\epsilon$ , we get

$$\varphi - \beta = \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2\beta - \frac{2\epsilon^6}{27} \sin^3 2\beta \\ + \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} \right) \left( \frac{2\epsilon^2}{3} + \frac{31\epsilon^4}{90} \right) \sin 2\varphi \cos 2\beta - \frac{17\epsilon^6}{540} \sin 4\beta \cos 2\beta \\ - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\beta - \frac{17\epsilon^6}{270} \sin 2\beta \cos 4\beta + \frac{383\epsilon^8}{45360} \sin 6\beta.$$

To the required approximation we get

$$\sin 2\varphi = \sin 2\beta + \frac{2\epsilon^2}{3} \sin 2\beta \cos 2\beta.$$



Substituting this value, we get the approximation

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} \right) \sin 2\beta - \frac{2\epsilon^6}{27} \sin^3 2\beta \\ & + \left( \frac{2\epsilon^4}{9} + \frac{31\epsilon^6}{135} \right) \sin 2\beta \cos 2\beta + \frac{4\epsilon^6}{27} \sin 2\beta \cos^2 2\beta \\ & - \frac{17\epsilon^6}{540} \sin 4\beta \cos 2\beta - \left( \frac{17\epsilon^4}{360} + \frac{61\epsilon^6}{1260} \right) \sin 4\beta \\ & - \frac{17\epsilon^6}{270} \sin 2\beta \cos 4\beta + \frac{383\epsilon^6}{45360} \sin 6\beta. \end{aligned}$$

Reduced to sines of multiple arcs (see reduction table, p. 88), this becomes the desired approximation

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4\beta \\ & + \frac{761\epsilon^6}{45360} \sin 6\beta. \end{aligned}$$

This result agrees with that already obtained.

#### DEVELOPMENT OF $\varphi - \beta$ IN TERMS OF $\beta$ —THIRD METHOD.

$\varphi - \beta$  can be developed in terms of  $\beta$  by a method similar to the third method of developing the same in terms of  $\varphi$  (see p. 64).

We have

$$\begin{aligned} \sin \varphi = & \sin \beta + \left( \frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945} \right) \sin \varphi \cos^2 \varphi \\ & - \left( \frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35} \right) \sin \varphi \cos^4 \varphi + \frac{4\epsilon^6}{7} \sin \varphi \cos^6 \varphi. \end{aligned}$$

Assume

$$\varphi = \beta - h = \beta - a\epsilon^2 - b\epsilon^4 - c\epsilon^6 - \dots,$$

then

$$\sin \varphi = \sin (\beta - h) = \sin \beta \cos h - \cos \beta \sin h,$$

or approximately

$$\begin{aligned} \sin \varphi = & \left( 1 - \frac{h^2}{2} \right) \sin \beta - \left( h - \frac{h^3}{6} \right) \cos \beta \\ = & \left( 1 - \frac{a^2\epsilon^4}{2} - ab\epsilon^6 \right) \sin \beta - \left( a\epsilon^2 + b\epsilon^4 + c\epsilon^6 - \frac{a^3\epsilon^6}{6} \right) \cos \beta. \end{aligned}$$

$$\cos \varphi = \cos (\beta - h) = \cos \beta \cos h + \sin \beta \sin h,$$

or approximately

$$\cos \varphi = \left(1 - \frac{h^2}{2}\right) \cos \beta + \left(h - \frac{h^3}{6}\right) \sin \beta.$$

No powers of  $\epsilon$  beyond the fourth are needed in this approximation.

$$\cos \varphi = \left(1 - \frac{a^2 \epsilon^4}{2}\right) \cos \beta + (a \epsilon^2 + b \epsilon^4) \sin \beta,$$

$$\cos^2 \varphi = \cos^2 \beta + 2 \epsilon^2 a \sin \beta \cos \beta + \epsilon^4 (a^2 \sin^2 \beta + 2b \sin \beta \cos \beta - a^2 \cos^2 \beta),$$

$$\begin{aligned} \sin \varphi \cos^2 \varphi = & \sin \beta \cos^2 \beta + \epsilon^2 (2a \sin^2 \beta \cos \beta - a \cos^3 \beta) \\ & + \epsilon^4 (a^2 \sin^3 \beta + 2b \sin^2 \beta \cos \beta - \frac{7a^2}{2} \sin \beta \cos^2 \beta \\ & - b \cos^3 \beta), \end{aligned}$$

$$\sin \varphi \cos^4 \varphi = \sin \beta \cos^4 \beta + \epsilon^2 (4a \sin^2 \beta \cos^3 \beta - a \cos^5 \beta),$$

$$\sin \varphi \cos^6 \varphi = \sin \beta \cos^6 \beta.$$

Substituting these approximations in the expression for  $\sin \varphi$ , we get

$$\begin{aligned} \sin \varphi = & \sin \beta + \frac{2\epsilon^2}{3} \sin \beta \cos^2 \beta + \epsilon^4 \left( \frac{4a}{3} \sin^2 \beta \cos \beta - \frac{2a}{3} \cos^3 \beta \right. \\ & \left. + \frac{34}{45} \sin \beta \cos^2 \beta \right) + \epsilon^6 \left( \frac{2a^2}{3} \sin^3 \beta + \frac{4b}{3} \sin^2 \beta \cos \beta \right. \\ & \left. - \frac{7a^2}{3} \sin \beta \cos^2 \beta - \frac{2b}{3} \cos^3 \beta + \frac{68a}{45} \sin^2 \beta \cos \beta \right. \\ & \left. - \frac{34a}{45} \cos^3 \beta \right) + \frac{766\epsilon^8}{945} \sin \beta \cos^2 \beta - \frac{3\epsilon^4}{5} \sin \beta \cos^4 \beta \\ & - \epsilon^6 \left( \frac{12a}{5} \sin^2 \beta \cos^3 \beta - \frac{3a}{5} \cos^5 \beta + \frac{46}{35} \sin \beta \cos^4 \beta \right) \\ & + \frac{4\epsilon^8}{7} \sin \beta \cos^6 \beta. \end{aligned}$$

But this series in  $\epsilon^2$  must be identically equal to the series already determined in the form

$$\sin \varphi = \sin \beta - \left( \frac{a^2 \epsilon^4}{2} + a b \epsilon^6 \right) \sin \beta - \left( a \epsilon^2 + b \epsilon^4 + c \epsilon^6 - \frac{a^3 \epsilon^6}{6} \right) \cos \beta.$$

Equating the coefficients of like powers of  $\epsilon$ , we get the equations

$$\begin{aligned}
 -a \cos \beta &= \frac{2}{3} \sin \beta \cos^2 \beta, \\
 -\frac{a^2}{2} \sin \beta - b \cos \beta &= \frac{4a}{3} \sin^2 \beta \cos \beta - \frac{2a}{3} \cos^3 \beta \\
 + \frac{34}{45} \sin \beta \cos^2 \beta - \frac{3}{5} \sin \beta \cos^4 \beta, \\
 -ab \sin \beta - c \cos \beta + \frac{a^3}{6} \cos \beta &= \frac{2a^3}{3} \sin^3 \beta + \frac{4b}{3} \sin^3 \beta \cos \beta \\
 -\frac{7a^2}{3} \sin \beta \cos^2 \beta - \frac{2b}{3} \cos^3 \beta + \frac{68a}{45} \sin^2 \beta \cos \beta \\
 -\frac{34a}{45} \cos^3 \beta + \frac{766}{945} \sin \beta \cos^2 \beta - \frac{12a}{5} \sin^3 \beta \cos^3 \beta \\
 + \frac{3a}{5} \cos^5 \beta - \frac{46}{35} \sin \beta \cos^4 \beta + \frac{4}{7} \sin \beta \cos^6 \beta.
 \end{aligned}$$

From these equations by successive substitutions and reductions (see reduction table, p. 88) we derive the values of  $a$ ,  $b$ , and  $c$ .

$$a = -\frac{2}{3} \sin \beta \cos \beta = -\frac{1}{3} \sin 2\beta,$$

$$b = -\frac{4}{45} \sin \beta \cos \beta - \frac{23}{45} \sin \beta \cos^3 \beta = -\frac{31}{180} \sin 2\beta - \frac{23}{360} \sin 4\beta,$$

$$\begin{aligned}
 c &= -\frac{38}{945} \sin \beta \cos \beta + \frac{16}{2835} \sin \beta \cos^3 \beta - \frac{1522}{2835} \sin \beta \cos^5 \beta \\
 &= -\frac{517}{5040} \sin 2\beta - \frac{251}{3780} \sin 4\beta - \frac{761}{45360} \sin 6\beta.
 \end{aligned}$$

By substituting these values and rearranging we get, as before, the desired approximation

$$\begin{aligned}
 \varphi - \beta &= \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4\beta \\
 &\quad + \frac{761\epsilon^8}{45360} \sin 6\beta.
 \end{aligned}$$

DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\beta$ —FOURTH METHOD.

The difference between the geodetic latitude and the authalic latitude can be developed by direct differentiation. Let us write the approximate equation of definition in the form (for the reductions, see table p. 88)

$$\sin \beta = \left(1 - \frac{\epsilon^2}{6} - \frac{41\epsilon^4}{360} - \frac{251\epsilon^6}{3024}\right) \sin \varphi - \left(\frac{\epsilon^2}{6} + \frac{11\epsilon^4}{144} + \frac{79\epsilon^6}{2160}\right) \sin 3\varphi \\ + \left(\frac{3\epsilon^4}{80} + \frac{21\epsilon^6}{560}\right) \sin 5\varphi - \frac{\epsilon^6}{112} \sin 7\varphi.$$

In this equation let  $h = \epsilon^2$  and it becomes

$$\sin \beta = \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \sin \varphi - \left(\frac{h}{6} + \frac{11h^2}{144} + \frac{79h^3}{2160}\right) \sin 3\varphi \\ + \left(\frac{3h^2}{80} + \frac{21h^3}{560}\right) \sin 5\varphi - \frac{h^3}{112} \sin 7\varphi.$$

Differentiate this expression, considering  $\varphi$  as a function of  $h$  or  $\epsilon^2$ , and we obtain in succession

$$\left[ \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \cos \varphi - \left(\frac{h}{2} + \frac{11h^2}{48} + \frac{79h^3}{720}\right) \cos 3\varphi \right. \\ \left. + \left(\frac{3h^2}{16} + \frac{21h^3}{112}\right) \cos 5\varphi - \frac{h^3}{16} \cos 7\varphi \right] \frac{d\varphi}{dh} - \left(\frac{1}{6} + \frac{41h}{180} \right. \\ \left. + \frac{251h^2}{1008}\right) \sin \varphi - \left(\frac{1}{6} + \frac{11h}{72} + \frac{79h^2}{720}\right) \sin 3\varphi \\ \left. + \left(\frac{3h}{40} + \frac{63h^2}{560}\right) \sin 5\varphi - \frac{3h^2}{112} \sin 7\varphi = 0,\right.$$

$$\left[ \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \cos \varphi - \left(\frac{h}{2} + \frac{11h^2}{48} + \frac{71h^3}{720}\right) \cos 3\varphi \right. \\ \left. + \left(\frac{3h^2}{16} + \frac{21h^3}{112}\right) \cos 5\varphi - \frac{h^3}{16} \cos 7\varphi \right] \frac{d^2\varphi}{dh^2} \\ - \left[ \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \sin \varphi - \left(\frac{3h}{2} + \frac{11h^2}{16} \right. \right. \\ \left. \left. + \frac{71h^3}{240}\right) \sin 3\varphi + \left(\frac{15h^2}{16} + \frac{105h^3}{112}\right) \sin 5\varphi \right. \\ \left. - \frac{7h^3}{16} \sin 7\varphi \right] \left(\frac{d\varphi}{dh}\right)^2 + 2 \left[ \left(-\frac{1}{6} - \frac{41h}{180} - \frac{251h^2}{1008}\right) \cos \varphi \right. \\ \left. - \left(\frac{1}{2} + \frac{11h}{24} + \frac{79h^2}{240}\right) \cos 3\varphi + \left(\frac{3h}{8} + \frac{63h^2}{112}\right) \cos 5\varphi \right. \\ \left. - \frac{3h^2}{16} \cos 7\varphi \right] \frac{d\varphi}{dh} - \left(\frac{41}{180} + \frac{251h}{504}\right) \sin \varphi$$

$$\begin{aligned}
& -\left(\frac{11}{72} + \frac{79h}{360}\right) \sin 3\varphi + \left(\frac{3}{40} + \frac{63h}{280}\right) \sin 5\varphi - \frac{3h}{56} \sin 7\varphi = 0, \\
& \left[ \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \cos \varphi - \left(\frac{h}{2} + \frac{11h^2}{48} + \frac{71h^3}{720}\right) \cos 3\varphi \right. \\
& \quad + \left(\frac{3h^2}{16} + \frac{21h^3}{112}\right) \cos 5\varphi - \frac{h^3}{16} \cos 7\varphi \left. \right] \frac{d^2\varphi}{dh^3} - 3 \left[ \left(1 - \frac{h}{6} \right. \right. \\
& \quad - \frac{41h^2}{360} - \frac{251h^3}{3024} \left. \right) \sin \varphi - \left(\frac{3h}{2} + \frac{11h^2}{16} + \frac{71h^3}{240}\right) \sin 3\varphi \\
& \quad + \left(\frac{15h^2}{16} + \frac{105h^3}{112}\right) \sin 5\varphi - \frac{7h^3}{16} \sin 7\varphi \left. \right] \frac{d\varphi}{dh} \frac{d^2\varphi}{dh^2} \\
& \quad + 3 \left[ -\left(\frac{1}{6} + \frac{41h}{180} + \frac{251h^2}{1008}\right) \cos \varphi - \left(\frac{1}{2} + \frac{11h}{24} \right. \right. \\
& \quad + \frac{71h^2}{240} \left. \right) \cos 3\varphi + \left(\frac{3h}{8} + \frac{63h^2}{112}\right) \cos 5\varphi - \frac{3h^2}{16} \cos 7\varphi \left. \right] \frac{d^2\varphi}{dh^2} \\
& \quad - \left[ \left(1 - \frac{h}{6} - \frac{41h^2}{360} - \frac{251h^3}{3024}\right) \cos \varphi - \left(\frac{9h}{2} + \frac{33h^2}{16} \right. \right. \\
& \quad + \frac{71h^3}{80} \left. \right) \cos 3\varphi + \left(\frac{75h^2}{16} + \frac{525h^3}{112}\right) \cos 5\varphi \\
& \quad - \frac{49h^3}{16} \cos 7\varphi \left. \right] \left(\frac{d\varphi}{dh}\right)^3 - 3 \left[ -\left(\frac{1}{6} + \frac{41h}{180} + \frac{251h^2}{1008}\right) \sin \varphi \right. \\
& \quad - \left(\frac{3}{2} + \frac{11h}{8} + \frac{71h^2}{80}\right) \sin 3\varphi + \left(\frac{15h}{8} + \frac{315h^2}{112}\right) \sin 5\varphi \\
& \quad - \frac{21h^2}{16} \sin 7\varphi \left. \right] \left(\frac{d\varphi}{dh}\right)^2 + 3 \left[ -\left(\frac{41}{180} + \frac{251h}{504}\right) \cos \varphi \right. \\
& \quad - \left(\frac{11}{24} + \frac{79h}{120}\right) \cos 3\varphi + \left(\frac{3}{8} + \frac{63h}{56}\right) \cos 5\varphi \\
& \quad - \frac{3h}{8} \cos 7\varphi \left. \right] \frac{d\varphi}{dh} - \frac{251}{504} \sin \varphi - \frac{79}{360} \sin 3\varphi \\
& \quad + \frac{63}{280} \sin 5\varphi - \frac{3}{56} \sin 7\varphi = 0.
\end{aligned}$$

Denoting by brackets the value of the derivatives for  $h=0$ , and remembering that all functions of  $\varphi$  become functions of  $\beta$  for  $h=0$ , we obtain by successive substitutions and reductions (for the reductions see the reduction table, p. 88).

$$[\varphi] = \beta,$$

$$\left[\frac{d\varphi}{dh}\right] = \frac{2}{3} \sin \beta \cos \beta = \frac{1}{3} \sin 2\beta,$$

$$\left[ \frac{d^2 \varphi}{dh^2} \right] = \frac{8}{45} \sin \beta \cos \beta + \frac{46}{45} \sin \beta \cos^3 \beta = \frac{31}{90} \sin 2\beta + \frac{23}{180} \sin 4\beta,$$

$$\begin{aligned} \left[ \frac{d^3 \varphi}{dh^3} \right] &= \frac{76}{315} \sin \beta \cos \beta - \frac{32}{945} \sin \beta \cos^3 \beta + \frac{3044}{945} \sin \beta \cos^5 \beta \\ &= \frac{517}{840} \sin 2\beta + \frac{251}{630} \sin 4\beta + \frac{761}{7560} \sin 6\beta. \end{aligned}$$

By Maclaurin's theorem, we have

$$\varphi = [\varphi] + \frac{\epsilon^2}{1!} \left[ \frac{d\varphi}{dh} \right] + \frac{\epsilon^4}{2!} \left[ \frac{d^2 \varphi}{dh^2} \right] + \frac{\epsilon^6}{3!} \left[ \frac{d^3 \varphi}{dh^3} \right] + \dots$$

By substituting the above values in this series and rearranging we obtain, as before, the approximation

$$\begin{aligned} \varphi - \beta &= \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4\beta \\ &\quad + \frac{761\epsilon^6}{45360} \sin 6\beta. \end{aligned}$$

**DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\beta$ —FIFTH METHOD.**

By Lagrange's theorem  $\varphi - \beta$  can be expressed in terms of  $\beta$  directly from the equation of definition. Let us take the equation in the form

$$\begin{aligned} x = y + \left( \frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945} \right) \sin \varphi \cos^2 \varphi - \left( \frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35} \right) \sin \varphi \cos^4 \varphi \\ + \frac{4\epsilon^6}{7} \sin \varphi \cos^6 \varphi, \end{aligned}$$

in which  $x = \sin \varphi$  and  $y = \sin \beta$ .

The series in  $\epsilon^2$  is a function of  $x$  through the functional relation between  $\varphi$  and  $x$ . We could substitute for the functions of  $\varphi$  their values in terms of  $x$ , but this is not necessary.

We wish to develop the function  $\sin^{-1} x$  in terms of  $y$  or in terms of  $\beta$  through the functional relation between  $y$  and  $\beta$ . Since the series in  $\epsilon^2$  is a small quantity, Lagrange's series may be expressed in general terms in the form

$$\begin{aligned} f(x) &= f(y) + \frac{1}{1!} g(y) f'(y) + \frac{1}{2!} \frac{d}{dy} \{ [g(y)]^2 f'(y) \} \\ &\quad + \frac{1}{3!} \frac{d^2}{dy^2} \{ [g(y)]^3 f'(y) \} + \frac{1}{4!} \frac{d^3}{dy^3} \{ [g(y)]^4 f'(y) \} + \dots, \end{aligned}$$

in which  $f(x)$  represents the function of  $x$  to be developed, and  $g(y)$  represents the series in  $\epsilon^2$  with  $\varphi$  replaced by  $\beta$ . The prime denotes differentiation with respect to  $y$ . But

$$f(y) = \sin^{-1}y,$$

$$f'(y) = \frac{1}{(1-y^2)^{\frac{1}{2}}} = \frac{1}{\cos \beta} = \sec \beta.$$

Retaining all powers of  $\epsilon$  up to the sixth, inclusive, we get

$$g(y) = \left( \frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945} \right) \sin \beta \cos^2 \beta - \left( \frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35} \right) \sin \beta \cos^4 \beta + \frac{4\epsilon^6}{7} \sin \beta \cos^6 \beta,$$

$$g(y) f'(y) = \left( \frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945} \right) \sin \beta \cos \beta - \left( \frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{35} \right) \sin \beta \cos^3 \beta + \frac{4\epsilon^6}{7} \sin \beta \cos^5 \beta,$$

$$[g(y)]^2 = \left( \frac{4\epsilon^4}{9} + \frac{136\epsilon^6}{135} \right) \sin^2 \beta \cos^4 \beta - \frac{4\epsilon^6}{5} \sin^2 \beta \cos^6 \beta,$$

$$[g(y)]^2 f'(y) = \left( \frac{4\epsilon^4}{9} + \frac{136\epsilon^6}{135} \right) \sin^2 \beta \cos^3 \beta - \frac{4\epsilon^6}{5} \sin^2 \beta \cos^5 \beta,$$

$$[g(y)]^3 = \frac{8\epsilon^6}{27} \sin^3 \beta \cos^6 \beta,$$

$$[g(y)]^3 f'(y) = \frac{8\epsilon^6}{27} \sin^3 \beta \cos^5 \beta.$$

To differentiate these expressions with respect to  $y$ , we merely differentiate with respect to  $\beta$  and multiply by  $\frac{d\beta}{dy}$ .

But  $\beta = f(y)$ ; so that  $\frac{d\beta}{dy} = f'(y) = \sec \beta$ .

For successive differentiations we differentiate with respect to  $\beta$  and multiply by  $\sec \beta$ , then differentiate again with respect to  $\beta$  and multiply again by  $\sec \beta$ , and so on for the remaining differentiations.

With this understanding, we get

$$\begin{aligned} \frac{d}{dy} \{[g(y)]^2 f'(y)\} &= \left(\frac{8\epsilon^4}{9} + \frac{272\epsilon^6}{135}\right) \sin \beta \cos^3 \beta \\ &- \left(\frac{4\epsilon^4}{3} + \frac{136\epsilon^6}{45}\right) \sin^3 \beta \cos \beta - \frac{8\epsilon^6}{5} \sin \beta \cos^5 \beta + 4\epsilon^6 \sin^3 \beta \cos^3 \beta \\ &= -\left(\frac{4\epsilon^4}{3} + \frac{136\epsilon^6}{45}\right) \sin \beta \cos \beta + \left(\frac{20\epsilon^4}{9} + \frac{244\epsilon^6}{27}\right) \sin \beta \cos^3 \beta \\ &- \frac{28\epsilon^6}{5} \sin \beta \cos^5 \beta, \end{aligned}$$

$$\begin{aligned} \frac{d^2}{dy^2} \{[g(y)]^2 f'(y)\} &= \frac{16\epsilon^6}{9} \sin \beta \cos^5 \beta - \frac{280\epsilon^6}{27} \sin^3 \beta \cos^3 \beta \\ &+ \frac{40\epsilon^6}{9} \sin^5 \beta \cos \beta \\ &= \frac{40\epsilon^6}{9} \sin \beta \cos \beta - \frac{520\epsilon^6}{27} \sin \beta \cos^3 \beta \\ &+ \frac{448\epsilon^6}{27} \sin \beta \cos^5 \beta. \end{aligned}$$

Substituting these values in the Lagrange series above, we get the approximation

$$\begin{aligned} \varphi &= \beta + \left(\frac{2\epsilon^2}{3} + \frac{34\epsilon^4}{45} + \frac{766\epsilon^6}{945}\right) \sin \beta \cos \beta - \left(\frac{3\epsilon^4}{5} + \frac{46\epsilon^6}{45}\right) \sin \beta \cos^3 \beta \\ &+ \frac{4\epsilon^6}{7} \sin \beta \cos^5 \beta - \left(\frac{2\epsilon^4}{3} + \frac{68\epsilon^6}{45}\right) \sin \beta \cos \beta + \left(\frac{10\epsilon^4}{9}\right. \\ &+ \left.\frac{122\epsilon^6}{27}\right) \sin \beta \cos^3 \beta - \frac{14\epsilon^6}{5} \sin \beta \cos^5 \beta + \frac{20\epsilon^6}{27} \sin \beta \cos \beta \\ &- \frac{260\epsilon^6}{81} \sin \beta \cos^3 \beta + \frac{224\epsilon^6}{81} \sin \beta \cos^5 \beta. \end{aligned}$$

By collecting similar terms, this becomes

$$\begin{aligned} \varphi &= \beta + \left(\frac{2\epsilon^2}{3} + \frac{4\epsilon^4}{45} + \frac{38\epsilon^6}{945}\right) \sin \beta \cos \beta + \left(\frac{23\epsilon^4}{45} - \frac{16\epsilon^6}{2835}\right) \sin \beta \cos^3 \beta \\ &+ \frac{1522\epsilon^6}{2835} \sin \beta \cos^5 \beta. \end{aligned}$$

On reduction by the table on page 88 and after rearrangement this becomes, as before, the desired approximation

$$\begin{aligned} \varphi - \beta &= \left(\frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040}\right) \sin 2\beta + \left(\frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780}\right) \sin 4\beta \\ &+ \frac{761\epsilon^6}{45360} \sin 6\beta. \end{aligned}$$



DEVELOPMENT OF  $\varphi - \beta$  IN TERMS OF  $\beta$ —SIXTH METHOD.

The difference between the geodetic latitude and the authalic latitude can be developed in terms of the authalic latitude by Arbogast's rule. (See p. 28.) We may define the function to be developed in the form

$$\begin{aligned} \varphi = \sin^{-1} & \left[ \sin \beta + \frac{h}{1!} \frac{2}{3} \sin \varphi \cos^2 \varphi \right. \\ & + \frac{h^2}{2!} \left( \frac{14}{45} \sin \varphi \cos^2 \varphi + \frac{6}{5} \sin^3 \varphi \cos^2 \varphi \right) \\ & + \frac{h^3}{3!} \left( \frac{128}{315} \sin \varphi \cos^2 \varphi + \frac{36}{35} \sin^3 \varphi \cos^2 \varphi \right. \\ & \left. + \frac{24}{7} \sin^5 \varphi \cos^2 \varphi \right) + \dots \dots \dots \left. \right] = A_0 + A_1 \frac{h}{1!} \\ & + A_2 \frac{h^2}{2!} + A_3 \frac{h^3}{3!} + \dots \dots \dots \end{aligned}$$

The  $A$ 's are defined as before

$$\begin{aligned} A_0 &= f(a_0), \\ A_1 &= a_1 f^1(a_0), \\ A_2 &= a_1^2 f^2(a_0) + a_2 f^1(a_0), \\ A_3 &= a_1^3 f^3(a_0) + 3a_1 a_2 f^2(a_0) + a_3 f^1(a_0). \\ &\text{etc.} \end{aligned}$$

In this function we have

$$\begin{aligned} a_0 &= \sin \beta, \\ \frac{da_0}{d\beta} &= \cos \beta, \end{aligned}$$

or

$$\frac{d\beta}{da_0} = \sec \beta,$$

$$f(a_0) = \beta,$$

$$f^1(a_0) = \frac{d\beta}{da_0} = \sec \beta,$$

$$f^2(a_0) = \sec \beta \tan \beta \frac{d\beta}{da_0} = \sec^2 \beta \tan \beta,$$

$$\begin{aligned} f^3(a_0) &= (2 \sec^2 \beta \tan^2 \beta + \sec^4 \beta) \frac{d\beta}{da_0} \\ &= 2 \sec^3 \beta \tan^2 \beta + \sec^5 \beta, \end{aligned}$$

$$a_1 = \frac{2}{3} \sin \varphi \cos^2 \varphi,$$

$$a_2 = \frac{14}{45} \sin \varphi \cos^2 \varphi + \frac{6}{5} \sin^3 \varphi \cos^2 \varphi,$$

$$a_3 = \frac{128}{315} \sin \varphi \cos^2 \varphi + \frac{36}{35} \sin^3 \varphi \cos^2 \varphi + \frac{24}{7} \sin^5 \varphi \cos^2 \varphi.$$

With these values of the  $a$ 's and the above values of the derivatives of  $f(a_0)$  we could compute the values of the  $A$ 's, but if we should do so at this stage we should have a combination of functions of  $\varphi$  and  $\beta$  in the development. To obviate this difficulty we must obtain approximations for the  $a$ 's in terms of functions of  $\beta$  and powers of  $h$ . The expression for  $a_1$  must include all first and second powers of  $h$  and the expression for  $a_2$  must include all first powers of  $h$ . In  $a_3$  we need only to replace  $\varphi$  by  $\beta$  in the given expression.

From the definition of the function to be expanded we see that the approximation to the first power of  $h$  for  $\sin \varphi$  is given by the expression

$$\sin \varphi = \sin \beta + \frac{2}{3} h \sin \beta \cos^2 \beta.$$

Substituting this value for  $\sin \varphi$  in the expression for  $\sin \varphi$  and retaining all second powers of  $h$ , as well as the first powers, we get

$$\begin{aligned} \sin \varphi &= \sin \beta + \frac{2}{3} h \sin \beta \cos^2 \beta - \frac{4}{3} h^2 \sin^3 \beta \cos^2 \beta \\ &+ \frac{4}{9} h^2 \sin \beta \cos^2 \beta + \frac{7}{45} h^2 \sin \beta \cos^2 \beta \\ &+ \frac{3}{5} h^2 \sin^3 \beta \cos^2 \beta, \end{aligned}$$

or

$$\begin{aligned} \sin \varphi &= \sin \beta + \frac{2}{3} h \sin \beta \cos^2 \beta + \frac{3}{5} h^2 \sin \beta \cos^2 \beta \\ &- \frac{11}{15} h^2 \sin^3 \beta \cos^2 \beta. \end{aligned}$$

Substituting this approximation in the expressions for the  $a$ 's, we get, to the required degree of exactness,

$$a_1 = \frac{2}{3} \left( \sin \beta \cos^2 \beta + \frac{2}{3} h \sin \beta \cos^2 \beta - 2h \sin^3 \beta \cos^2 \beta \right. \\ \left. + \frac{3}{5} h^2 \sin \beta \cos^2 \beta - \frac{58}{15} h^2 \sin^3 \beta \cos^2 \beta \right. \\ \left. + \frac{53}{15} h^2 \sin^5 \beta \cos^2 \beta \right),$$

$$a_2 = \frac{14}{45} \sin \beta \cos^2 \beta + \frac{6}{5} \sin^3 \beta \cos^2 \beta + \frac{28}{135} h \sin \beta \cos^2 \beta \\ + \frac{16}{9} h \sin^3 \beta \cos^2 \beta - 4h \sin^5 \beta \cos^2 \beta,$$

$$a_3 = \frac{128}{315} \sin \beta \cos^2 \beta + \frac{36}{35} \sin^3 \beta \cos^2 \beta + \frac{24}{7} \sin^5 \beta \cos^2 \beta.$$

With these approximations, the approximations for the  $A$ 's become (for the reductions see table p. 88)

$$A_0 = \beta,$$

$$A_1 = \frac{2}{3} \left( \sin \beta \cos \beta + \frac{2}{3} h \sin \beta \cos \beta - 2h \sin^3 \beta \cos \beta \right. \\ \left. + \frac{3}{5} h^2 \sin \beta \cos \beta - \frac{58}{15} h^2 \sin^3 \beta \cos \beta \right. \\ \left. + \frac{53}{15} h^2 \sin^5 \beta \cos \beta \right),$$

$$A_2 = \frac{4}{9} \left( \sin^3 \beta \cos \beta + \frac{4}{3} h \sin^3 \beta \cos \beta - 4h \sin^5 \beta \cos \beta \right) \\ + \frac{14}{45} \sin \beta \cos \beta + \frac{6}{5} \sin^3 \beta \cos \beta + \frac{128}{315} h \sin \beta \cos \beta \\ + \frac{16}{9} h \sin^3 \beta \cos \beta - 4h \sin^5 \beta \cos \beta \\ = \frac{14}{45} \sin \beta \cos \beta + \frac{74}{45} \sin^3 \beta \cos \beta + \frac{28}{135} h \sin \beta \cos \beta \\ + \frac{64}{27} h \sin^3 \beta \cos \beta - \frac{52}{9} h \sin^5 \beta \cos \beta,$$

$$\begin{aligned}
 A_1 &= \frac{8}{27} \sin^2 \beta \cos^6 \beta (2 \sec^3 \beta \tan^2 \beta + \sec^5 \beta) \\
 &+ \left( \frac{28}{45} \sin^2 \beta \cos^4 \beta + \frac{12}{5} \sin^4 \beta \cos^4 \beta \right) \sec^2 \beta \tan \beta \\
 &+ \frac{128}{315} \sin \beta \cos \beta + \frac{36}{35} \sin^3 \beta \cos \beta + \frac{24}{7} \sin^5 \beta \cos \beta \\
 &= \frac{16}{27} \sin^5 \beta \cos \beta + \frac{8}{27} \sin^3 \beta \cos \beta + \frac{28}{45} \sin^3 \beta \cos \beta \\
 &+ \frac{12}{5} \sin^5 \beta \cos \beta + \frac{128}{315} \sin \beta \cos \beta + \frac{36}{35} \sin^3 \beta \cos \beta \\
 &+ \frac{24}{7} \sin^5 \beta \cos \beta \\
 &= \frac{128}{315} \sin \beta \cos \beta + \frac{368}{189} \sin^3 \beta \cos \beta \\
 &+ \frac{6068}{945} \sin^5 \beta \cos \beta.
 \end{aligned}$$

Substituting these values in the development, we get the approximation

$$\begin{aligned}
 \varphi &= \beta + \frac{2h}{3} \left( \sin \beta \cos \beta + \frac{2}{3} h \sin \beta \cos \beta - 2h \sin^3 \beta \cos \beta \right. \\
 &+ \frac{3}{5} h^2 \sin \beta \cos \beta - \frac{58}{15} h^2 \sin^3 \beta \cos \beta \\
 &+ \left. \frac{53}{15} h^2 \sin^5 \beta \cos \beta \right) + \frac{h^2}{2} \left( \frac{14}{45} \sin \beta \cos \beta \right. \\
 &+ \frac{74}{45} \sin^3 \beta \cos \beta + \frac{28}{135} h \sin \beta \cos \beta \\
 &+ \left. \frac{64}{27} h \sin^3 \beta \cos \beta - \frac{52}{9} h \sin^5 \beta \cos \beta \right) \\
 &+ \frac{h^3}{6} \left( \frac{128}{315} \sin \beta \cos \beta + \frac{368}{189} \sin^3 \beta \cos \beta \right. \\
 &+ \left. \frac{6068}{945} \sin^5 \beta \cos \beta \right).
 \end{aligned}$$

Rearranging in powers of  $h$  and replacing  $h$  by  $e^2$  we get the approximation

$$\begin{aligned}
 \varphi &= \beta + \frac{2e^2}{3} \sin \beta \cos \beta + e^4 \left( \frac{3}{5} \sin \beta \cos \beta - \frac{23}{45} \sin^3 \beta \cos \beta \right) \\
 &+ e^6 \left( \frac{4}{7} \sin \beta \cos \beta - \frac{3028}{2835} \sin^3 \beta \cos \beta \right. \\
 &+ \left. \frac{1522}{2835} \sin^5 \beta \cos \beta \right)
 \end{aligned}$$

Making the reductions by aid of the table on page 88 and rearranging, we obtain, as before, the desired approximation

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} + \frac{251\epsilon^6}{3780} \right) \sin 4\beta \\ & + \frac{761\epsilon^8}{45360} \sin 6\beta. \end{aligned}$$

#### TABULATION OF ALL THE DEVELOPMENTS.

For convenience of reference we shall now list all of the developments in a general table.

$$m = \frac{\epsilon^2}{2 - \epsilon^2}$$

$$\varphi - \psi = m \sin 2\varphi - \frac{m^2}{2} \sin 4\varphi + \frac{m^3}{3} \sin 6\varphi - \dots$$

$$\varphi - \psi = m \sin 2\psi + \frac{m^2}{2} \sin 4\psi + \frac{m^3}{3} \sin 6\psi + \dots$$

$$n = \frac{1 - (1 - \epsilon^2)^{1/2}}{1 + (1 - \epsilon^2)^{1/2}}$$

$$\varphi - \theta = n \sin 2\varphi - \frac{n^2}{2} \sin 4\varphi + \frac{n^3}{3} \sin 6\varphi - \dots$$

$$\varphi - \theta = n \sin 2\theta + \frac{n^2}{2} \sin 4\theta + \frac{n^3}{3} \sin 6\theta + \dots$$

$$\theta - \psi = n \sin 2\theta - \frac{n^2}{2} \sin 4\theta + \frac{n^3}{3} \sin 6\theta - \dots$$

$$\theta - \psi = n \sin 2\psi + \frac{n^2}{2} \sin 4\psi + \frac{n^3}{3} \sin 6\psi + \dots$$

$$\begin{aligned} \varphi - \chi = & \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{3\epsilon^6}{32} + \frac{281\epsilon^8}{5760} + \dots \right) \sin 2\varphi \\ & - \left( \frac{5\epsilon^4}{48} + \frac{7\epsilon^6}{80} + \frac{697\epsilon^8}{11520} + \dots \right) \sin 4\varphi + \left( \frac{13\epsilon^6}{480} + \frac{461\epsilon^8}{13440} \right. \\ & \left. + \dots \right) \sin 6\varphi - \left( \frac{1237\epsilon^8}{161280} + \dots \right) \sin 8\varphi + \dots \end{aligned}$$

$$\begin{aligned} \varphi - \chi = & \left( \frac{\epsilon^2}{2} + \frac{5\epsilon^4}{24} + \frac{\epsilon^6}{12} + \frac{13\epsilon^8}{360} + \dots \right) \sin 2\chi \\ & + \left( \frac{7\epsilon^4}{48} + \frac{29\epsilon^6}{240} + \frac{811\epsilon^8}{11520} + \dots \right) \sin 4\chi + \left( \frac{7\epsilon^6}{120} \right. \\ & \left. + \frac{81\epsilon^8}{1120} + \dots \right) \sin 6\chi \\ & + \left( \frac{4279\epsilon^8}{161280} + \dots \right) \sin 8\chi + \dots \end{aligned}$$

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{59\epsilon^6}{560} + \dots \right) \sin 2\varphi - \left( \frac{17\epsilon^4}{360} \right. \\ & \left. + \frac{61\epsilon^6}{1260} + \dots \right) \sin 4\varphi + \left( \frac{383\epsilon^6}{45360} + \dots \right) \sin 6\varphi - \dots \end{aligned}$$

$$\begin{aligned} \varphi - \beta = & \left( \frac{\epsilon^2}{3} + \frac{31\epsilon^4}{180} + \frac{517\epsilon^6}{5040} + \dots \right) \sin 2\beta + \left( \frac{23\epsilon^4}{360} \right. \\ & \left. + \frac{251\epsilon^6}{3780} + \dots \right) \sin 4\beta + \left( \frac{761\epsilon^8}{45360} + \dots \right) \sin 6\beta + \dots \end{aligned}$$

If the various differences of latitude were computed as they are here given, the results would be expressed in radians. It is most convenient to have them expressed in seconds of arc; the results would therefore have to be divided by the arc of one second or by the sine of one second, since the arc and sine of one second are much more nearly equal than the approximation requires. In practice it is better to divide each of the coefficients in the above developments by the sine of one second, since in this manner we may transform from radians to seconds of arc by one operation. The various coefficients will then be expressed in seconds and the result of any computation will be in seconds of arc.

#### DETERMINATION OF THE NUMERICAL VALUE OF THE COEFFICIENTS IN THE DEVELOPMENTS FOR THE CLARKE SPHEROID OF 1866.

For computation purposes it is necessary to have the coefficients in these developments expressed as numbers or as logarithms.

The division of each of the coefficients by  $\sin 1''$  is indicated in the first development given below, and the same process must be applied in the case of each of the other developments.

We assume  $\epsilon^2$  as defined by

$$\log \epsilon^2 = 7.83050257 - 10;$$

hence

$$\epsilon^2 = 0.006768658$$

$$m = \frac{\epsilon^2}{2 - \epsilon^2}$$

$$\log m = 7.53094486 - 10.$$

If  $\varphi - \psi$  is to be expressed in seconds, we get

$$\varphi - \psi = \frac{m}{\sin 1''} \sin 2\varphi - \frac{m^2}{2 \sin 1''} \sin 4\varphi + \frac{m^3}{3 \sin 1''} \sin 6\varphi - \dots$$

or,

$$\varphi - \psi = 700^{\circ}4385 \sin 2\varphi - 1^{\circ}1893 \sin 4\varphi + 0^{\circ}0027 \sin 6\varphi,$$

or in terms of logarithms

$$\begin{aligned} \varphi - \psi = & [2.8453700] \sin 2\varphi - [0.075285] \sin 4\varphi \\ & + [7.430 - 10] \sin 6\varphi. \end{aligned}$$

Also

$$\varphi - \psi = 700^{\circ}4385 \sin 2\psi + 1^{\circ}1893 \sin 4\psi + 0^{\circ}0027 \sin 6\psi$$

and

$$\begin{aligned} \varphi - \psi = & [2.8453700] \sin 2\psi + [0.075285] \sin 4\psi \\ & + [7.430 - 10] \sin 6\psi. \end{aligned}$$

Furthermore

$$n = \frac{1 - (1 - \epsilon^2)^{1/2}}{1 + (1 - \epsilon^2)^{1/2}} = \frac{\epsilon^2}{4} + \frac{\epsilon^4}{8} + \frac{5\epsilon^6}{64} + \frac{7\epsilon^8}{128} + \dots$$

$$\log n = 7.22991610 - 10,$$

$$\varphi - \theta = 350^{\circ}2202 \sin 2\varphi - 0^{\circ}2973 \sin 4\varphi + 0^{\circ}0003 \sin 6\varphi,$$

$$\begin{aligned} \varphi - \theta = & [2.5443412] \sin 2\varphi - [9.47323 - 10] \sin 4\varphi \\ & + [6.527 - 10] \sin 6\varphi. \end{aligned}$$

Also

$$\begin{aligned} \varphi - \theta &= 350^{\circ}2202 \sin 2\theta + 0^{\circ}2973 \sin 4\theta + 0^{\circ}0003 \sin 6\theta, \\ \varphi - \theta &= [2.5443412] \sin 2\theta + [9.47323 - 10] \sin 4\theta \\ &\quad + [6.527 - 10] \sin 6\theta. \end{aligned}$$

In a similar manner we have

$$\begin{aligned} \theta - \psi &= 350^{\circ}2202 \sin 2\theta - 0^{\circ}2973 \sin 4\theta + 0^{\circ}0003 \sin 6\theta, \\ \theta - \psi &= [2.5443412] \sin 2\theta - [9.47323 - 10] \sin 4\theta \\ &\quad + [6.527 - 10] \sin 6\theta, \end{aligned}$$

and

$$\begin{aligned} \theta - \psi &= 350^{\circ}2202 \sin 2\psi + 0^{\circ}2973 \sin 4\psi + 0^{\circ}0003 \sin 6\psi, \\ \psi - \psi &= [2.5443412] \sin 2\psi + [9.47323 - 10] \sin 4\psi \\ &\quad + [6.527 - 10] \sin 6\psi, \end{aligned}$$

$$\begin{aligned} \varphi - \chi &= 700^{\circ}0427 \sin 2\varphi - 0^{\circ}9900 \sin 4\varphi + 0^{\circ}0017 \sin 6\varphi, \\ \varphi - \chi &= [2.84512455] \sin 2\varphi - [9.99563 - 10] \sin 4\varphi \\ &\quad + [7.238 - 10] \sin 6\varphi, \end{aligned}$$

$$\begin{aligned} \varphi - \chi &= 700^{\circ}0420 \sin 2\chi + 1^{\circ}3859 \sin 4\chi + 0^{\circ}0037 \sin 6\chi, \\ \varphi - \chi &= [2.84512413] \sin 2\chi + [0.141726] \sin 4\chi \\ &\quad + [7.572 - 10] \sin 6\chi, \end{aligned}$$

$$\begin{aligned} \varphi - \beta &= 467^{\circ}0129 \sin 2\varphi - 0^{\circ}4494 \sin 4\varphi + 0^{\circ}0005 \sin 6\varphi, \\ \varphi - \beta &= [2.6693289] \sin 2\varphi - [9.65258 - 10] \sin 4\varphi \\ &\quad + [6.732 - 10] \sin 6\varphi, \end{aligned}$$

and

$$\begin{aligned} \varphi - \beta &= 467^{\circ}0127 \sin 2\beta + 0^{\circ}6080 \sin 4\beta + 0^{\circ}0011 \sin 6\beta, \\ \varphi - \beta &= [2.6693287] \sin 2\beta + [9.78390 - 10] \sin 4\beta \\ &\quad + [7.031 - 10] \sin 6\beta. \end{aligned}$$

The radius of the sphere equivalent in area to the ellipsoid of revolution is defined by the formula

$$R = a \left( 1 - \frac{\epsilon^2}{6} - \frac{17\epsilon^4}{360} - \frac{67\epsilon^6}{3024} - \dots \right),$$

in which  $a$  is the equatorial radius of the ellipsoid.

For the Clarke ellipsoid of 1866

$$\log R = 6.80420742$$

$$R = 6370997.2 \text{ meters.}$$



By using the authalic latitudes and this value of  $R$ , the spheroid can be treated as a sphere in all questions of equivalent or equal-area mapping.

The appended tables of the various latitude differences are computed for the Clarke spheroid of 1866. Interpolation could be made with the table by the consideration of second differences to a degree of accuracy sufficient for ordinary purposes. The differences are given in thousandths of a second in order that the differences between adjacent values may be better preserved. The table of transformation to isometric latitude is given in a form somewhat different from the others. The isometric colatitude is given and in another column this value divided by two. This is done because in the most important applications of this latitude it is most convenient to use the semicolatitude. The table thus gives at once the value that is needed for use.

#### REDUCTION TABLE.

$$\sin^2 a = \frac{1}{2} (1 - \cos 2a)$$

$$\sin^3 a = \frac{1}{4} (3 \sin a - \sin 3a)$$

$$\sin^4 a = \frac{1}{8} (3 - 4 \cos 2a + \cos 4a)$$

$$\sin^5 a = \frac{1}{16} (10 \sin a - 5 \sin 3a + \sin 5a)$$

$$\sin^6 a = \frac{1}{32} (10 - 15 \cos 2a + 6 \cos 4a - \cos 6a)$$

$$\sin^7 a = \frac{1}{64} (35 \sin a - 21 \sin 3a + 7 \sin 5a - \sin 7a)$$

$$\cos^2 a = \frac{1}{2} (1 + \cos 2a)$$

$$\cos^3 a = \frac{1}{4} (3 \cos a + \cos 3a)$$

$$\cos^4 a = \frac{1}{8} (3 + 4 \cos 2a + \cos 4a)$$

$$\cos^5 a = \frac{1}{16} (10 \cos a + 5 \cos 3a + \cos 5a)$$

$$\cos^6 a = \frac{1}{32} (10 + 15 \cos 2a + 6 \cos 4a + \cos 6a)$$

$$\cos^7 a = \frac{1}{64} (35 \cos a + 21 \cos 3a + 7 \cos 5a + \cos 7a)$$

$$\sin 2a = 2 \sin a \cos a,$$

$$\sin 3a = 4 \sin a \cos^2 a - \sin a,$$

$$\sin 4a = 8 \sin a \cos^3 a - 4 \sin a \cos a,$$

$$\sin 5a = 16 \sin a \cos^4 a - 12 \sin a \cos^2 a + \sin a,$$

$$\sin 6a = 32 \sin a \cos^5 a - 32 \sin a \cos^3 a + 6 \sin a \cos a,$$

$$\sin 7a = 64 \sin a \cos^6 a - 80 \sin a \cos^4 a + 24 \sin a \cos^2 a - \sin a,$$

$$\sin 8a = 128 \sin a \cos^7 a - 192 \sin a \cos^5 a + 80 \sin a \cos^3 a + 8 \sin a \cos a,$$

$$\cos 2a = 2 \cos^2 a - 1,$$

$$\cos 3a = 4 \cos^3 a - 3 \cos a,$$

$$\cos 4a = 8 \cos^4 a - 8 \cos^2 a + 1,$$

$$\cos 5a = 16 \cos^5 a - 20 \cos^3 a + 5 \cos a,$$

$$\cos 6a = 32 \cos^6 a - 48 \cos^4 a + 18 \cos^2 a - 1,$$

$$\cos 7a = 64 \cos^7 a - 112 \cos^5 a + 56 \cos^3 a - 7 \cos a,$$

$$\cos 8a = 128 \cos^8 a - 256 \cos^6 a + 160 \cos^4 a - 32 \cos^2 a + 1,$$

$$\sin a \cos b = \frac{1}{2} [\sin (a+b) + \sin (a-b)], \quad a > b,$$

$$\sin a \cos b = \frac{1}{2} [\sin (b+a) - \sin (b-a)], \quad b > a,$$

$$\cos a \cos b = \frac{1}{2} [\cos (a-b) + \cos (a+b)],$$

$$\sin a \sin b = \frac{1}{2} [\cos (a-b) - \cos (a+b)],$$

$$\tan \frac{a}{2} = \frac{\sin a}{1 + \cos a} = \frac{1 - \cos a}{\sin a},$$

$$\tan \frac{a}{2} \sin a = 1 - \cos a,$$

$$\sec^2 \frac{a}{2} \sin^2 a = 2(1 - \cos a),$$

$$\sin a + \sin b = 2 \sin \frac{1}{2}(a+b) \cos \frac{1}{2}(a-b),$$

$$\sin a - \sin b = 2 \sin \frac{1}{2}(a-b) \cos \frac{1}{2}(a+b),$$

$$\cos a + \cos b = 2 \cos \frac{1}{2}(a+b) \cos \frac{1}{2}(a-b),$$

$$\cos a - \cos b = -2 \sin \frac{1}{2}(a+b) \sin \frac{1}{2}(a-b),$$

$$\sin a \cos a = \frac{1}{2} \sin 2a,$$

$$\sin a \cos^2 a = \frac{1}{4} \sin a + \frac{1}{4} \sin 3a,$$

$$\sin a \cos^3 a = \frac{1}{4} \sin 2a + \frac{1}{8} \sin 4a,$$

$$\sin a \cos^4 a = \frac{1}{8} \sin a + \frac{3}{16} \sin 3a + \frac{1}{16} \sin 5a,$$

$$\sin a \cos^5 a = \frac{5}{32} \sin 2a + \frac{1}{8} \sin 4a + \frac{1}{32} \sin 6a,$$

$$\sin a \cos^6 a = \frac{5}{64} \sin a + \frac{9}{64} \sin 3a + \frac{5}{64} \sin 5a + \frac{1}{64} \sin 7a,$$

$$\sin a \cos^7 a = \frac{7}{64} \sin 2a + \frac{7}{64} \sin 4a + \frac{3}{64} \sin 6a + \frac{1}{128} \sin 8a.$$

LATITUDE TRANSFORMATION.

*Geodetic to geocentric.*

| Geodetic latitude. | Geodetic minus geocentric. | Geocentric latitude. | Geodetic latitude. | Geodetic minus geocentric. | Geocentric latitude. |
|--------------------|----------------------------|----------------------|--------------------|----------------------------|----------------------|
| $\varphi$          | $\varphi - \psi$           | $\psi$               | $\varphi$          | $\varphi - \psi$           | $\psi$               |
| 0 00               | 0 00.000                   | 0 00 00.00           | 22 30              | 8 14.097                   | 22 21 45.90          |
| 0 30               | 0 12.183                   | 0 29 47.82           | 23 00              | 8 22.666                   | 22 51 37.33          |
| 1 00               | 0 24.362                   | 0 59 35.64           | 23 30              | 8 31.064                   | 23 21 28.92          |
| 1 30               | 0 36.534                   | 1 29 23.47           | 24 00              | 8 39.346                   | 23 51 20.65          |
| 2 00               | 0 48.695                   | 1 59 11.30           | 24 30              | 8 47.451                   | 24 21 12.55          |
| 2 30               | 1 00.841                   | 2 28 59.16           | 25 00              | 8 55.397                   | 24 51 04.60          |
| 3 00               | 1 12.966                   | 2 58 47.02           | 25 30              | 9 03.181                   | 25 20 56.82          |
| 3 30               | 1 25.075                   | 3 28 34.92           | 26 00              | 9 10.800                   | 25 50 49.20          |
| 4 00               | 1 37.156                   | 3 58 22.84           | 26 30              | 9 18.253                   | 26 20 41.75          |
| 4 30               | 1 49.206                   | 4 28 10.76           | 27 00              | 9 25.536                   | 26 50 34.46          |
| 5 00               | 2 01.224                   | 4 57 58.78           | 27 30              | 9 32.649                   | 27 20 27.35          |
| 5 30               | 2 13.206                   | 5 27 46.79           | 28 00              | 9 39.582                   | 27 50 20.41          |
| 6 00               | 2 25.147                   | 5 57 34.85           | 28 30              | 9 46.351                   | 28 20 13.65          |
| 6 30               | 2 37.045                   | 6 27 22.96           | 29 00              | 9 52.937                   | 28 50 07.06          |
| 7 00               | 2 48.895                   | 6 57 11.11           | 29 30              | 9 59.343                   | 29 20 00.66          |
| 7 30               | 3 00.694                   | 7 26 59.31           | 30 00              | 10 05.568                  | 29 49 54.43          |
| 8 00               | 3 12.430                   | 7 56 47.56           | 30 30              | 10 11.609                  | 30 19 48.36          |
| 8 30               | 3 24.126                   | 8 26 35.87           | 31 00              | 10 17.464                  | 30 49 42.54          |
| 9 00               | 3 35.750                   | 8 56 24.25           | 31 30              | 10 23.133                  | 31 19 36.87          |
| 9 30               | 3 47.311                   | 9 26 12.66           | 32 00              | 10 28.612                  | 31 49 31.39          |
| 10 00              | 3 58.802                   | 9 56 01.20           | 32 30              | 10 33.901                  | 32 19 26.10          |
| 10 30              | 4 10.221                   | 10 25 49.78          | 33 00              | 10 39.998                  | 32 49 21.00          |
| 11 00              | 4 21.565                   | 10 55 38.43          | 33 30              | 10 43.900                  | 33 19 16.10          |
| 11 30              | 4 32.830                   | 11 25 27.17          | 34 00              | 10 48.608                  | 33 49 11.39          |
| 12 00              | 4 44.013                   | 11 55 15.99          | 34 30              | 10 53.119                  | 34 19 06.88          |
| 12 30              | 4 55.110                   | 12 25 04.89          | 35 00              | 10 57.431                  | 34 49 02.57          |
| 13 00              | 5 06.117                   | 12 54 53.88          | 35 30              | 11 01.544                  | 35 18 58.46          |
| 13 30              | 5 17.033                   | 13 24 42.97          | 36 00              | 11 05.456                  | 35 48 54.54          |
| 14 00              | 5 27.853                   | 13 54 32.15          | 36 30              | 11 09.166                  | 36 18 50.83          |
| 14 30              | 5 38.573                   | 14 24 21.43          | 37 00              | 11 12.673                  | 36 48 47.33          |
| 15 00              | 5 49.192                   | 14 54 10.81          | 37 30              | 11 15.975                  | 37 18 44.02          |
| 15 30              | 5 59.705                   | 15 24 00.29          | 38 00              | 11 19.072                  | 37 48 40.93          |
| 16 00              | 6 10.110                   | 15 53 49.89          | 38 30              | 11 21.963                  | 38 18 38.04          |
| 16 30              | 6 20.402                   | 16 23 39.60          | 39 00              | 11 24.646                  | 38 48 35.35          |
| 17 00              | 6 30.590                   | 16 53 29.42          | 39 30              | 11 27.122                  | 39 18 32.88          |
| 17 30              | 6 40.640                   | 17 23 19.36          | 40 00              | 11 29.388                  | 39 48 30.61          |
| 18 00              | 6 50.579                   | 17 53 09.42          | 40 30              | 11 31.445                  | 40 18 28.56          |
| 18 30              | 7 00.394                   | 18 22 59.61          | 41 00              | 11 33.292                  | 40 48 26.71          |
| 19 00              | 7 10.082                   | 18 52 49.92          | 41 30              | 11 34.927                  | 41 18 25.07          |
| 19 30              | 7 19.639                   | 19 22 40.36          | 42 00              | 11 36.352                  | 41 48 23.65          |
| 20 00              | 7 29.064                   | 19 52 30.94          | 42 30              | 11 37.564                  | 42 18 22.44          |
| 20 30              | 7 38.354                   | 20 22 21.65          | 43 00              | 11 38.564                  | 42 48 21.44          |
| 21 00              | 7 47.504                   | 20 52 12.50          | 43 30              | 11 39.352                  | 43 18 20.65          |
| 21 30              | 7 56.513                   | 21 22 03.49          | 44 00              | 11 39.928                  | 43 48 20.07          |
| 22 00              | 8 05.379                   | 21 51 54.62          | 44 30              | 11 40.288                  | 44 18 19.77          |
| 22 30              | 8 14.097                   | 22 21 45.90          | 45 00              | 11 40.436                  | 44 48 19.50          |

$$\varphi - \psi = +700'4385 \sin 2\varphi - 17'1893 \sin 4\varphi + 0'0027 \sin 6\varphi.$$

$$\varphi - \psi = [2.8453700] \sin 2\varphi - [0.075285] \sin 4\varphi + [7.430 - 10] \sin 6\varphi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geodetic to geocentric—Continued.*

| Geodetic latitude. |    |    | Geodetic minus geocentric. |     |     | Geocentric latitude. |    |       | Geodetic latitude. |    |    | Geodetic minus geocentric. |     |     | Geocentric latitude. |    |       |
|--------------------|----|----|----------------------------|-----|-----|----------------------|----|-------|--------------------|----|----|----------------------------|-----|-----|----------------------|----|-------|
| $\varphi$          |    |    | $\varphi - \psi$           |     |     | $\psi$               |    |       | $\varphi$          |    |    | $\varphi - \psi$           |     |     | $\psi$               |    |       |
| °                  | '  | '' | °                          | '   | ''  | °                    | '  | ''    | °                  | '  | '' | °                          | '   | ''  | °                    | '  | ''    |
| 45                 | 00 |    | 11                         | 40. | 436 | 44                   | 48 | 19.56 | 67                 | 30 |    | 8                          | 16. | 476 | 67                   | 21 | 43.52 |
| 45                 | 30 |    | 11                         | 40. | 371 | 45                   | 18 | 19.63 | 68                 | 00 |    | 8                          | 07. | 756 | 67                   | 51 | 52.24 |
| 46                 | 00 |    | 11                         | 40. | 092 | 45                   | 48 | 19.91 | 68                 | 30 |    | 7                          | 58. | 886 | 68                   | 22 | 01.11 |
| 46                 | 30 |    | 11                         | 39. | 600 | 46                   | 18 | 20.40 | 69                 | 00 |    | 7                          | 49. | 870 | 68                   | 52 | 10.13 |
| 47                 | 00 |    | 11                         | 38. | 895 | 46                   | 48 | 21.10 | 69                 | 30 |    | 7                          | 40. | 709 | 69                   | 22 | 19.29 |
| 47                 | 30 |    | 11                         | 37. | 977 | 47                   | 18 | 22.02 | 70                 | 00 |    | 7                          | 31. | 407 | 69                   | 52 | 28.59 |
| 48                 | 00 |    | 11                         | 36. | 846 | 47                   | 48 | 23.15 | 70                 | 30 |    | 7                          | 21. | 966 | 70                   | 22 | 38.03 |
| 48                 | 30 |    | 11                         | 35. | 503 | 48                   | 18 | 24.50 | 71                 | 00 |    | 7                          | 12. | 390 | 70                   | 52 | 47.61 |
| 49                 | 00 |    | 11                         | 33. | 947 | 48                   | 48 | 26.05 | 71                 | 30 |    | 7                          | 02. | 680 | 71                   | 22 | 57.32 |
| 49                 | 30 |    | 11                         | 32. | 180 | 49                   | 18 | 27.82 | 72                 | 00 |    | 6                          | 52. | 841 | 71                   | 53 | 07.16 |
| 50                 | 00 |    | 11                         | 30. | 202 | 49                   | 48 | 29.80 | 72                 | 30 |    | 6                          | 42. | 675 | 72                   | 23 | 17.12 |
| 50                 | 30 |    | 11                         | 28. | 013 | 50                   | 18 | 31.99 | 73                 | 00 |    | 6                          | 32. | 786 | 72                   | 53 | 27.21 |
| 51                 | 00 |    | 11                         | 25. | 614 | 50                   | 48 | 34.39 | 73                 | 30 |    | 6                          | 22. | 575 | 73                   | 23 | 37.42 |
| 51                 | 30 |    | 11                         | 23. | 006 | 51                   | 18 | 36.99 | 74                 | 00 |    | 6                          | 12. | 248 | 73                   | 53 | 47.75 |
| 52                 | 00 |    | 11                         | 20. | 189 | 51                   | 48 | 39.81 | 74                 | 30 |    | 6                          | 01. | 805 | 74                   | 23 | 58.19 |
| 52                 | 30 |    | 11                         | 17. | 164 | 52                   | 18 | 42.84 | 75                 | 00 |    | 5                          | 51. | 252 | 74                   | 54 | 08.75 |
| 53                 | 00 |    | 11                         | 13. | 933 | 52                   | 48 | 46.07 | 75                 | 30 |    | 5                          | 40. | 591 | 75                   | 24 | 19.41 |
| 53                 | 30 |    | 11                         | 10. | 496 | 53                   | 18 | 49.50 | 76                 | 00 |    | 5                          | 29. | 825 | 75                   | 54 | 30.17 |
| 54                 | 00 |    | 11                         | 06. | 854 | 53                   | 48 | 53.15 | 76                 | 30 |    | 5                          | 18. | 957 | 76                   | 24 | 41.04 |
| 54                 | 30 |    | 11                         | 03. | 008 | 54                   | 18 | 56.99 | 77                 | 00 |    | 5                          | 07. | 992 | 76                   | 54 | 52.01 |
| 55                 | 00 |    | 10                         | 58. | 980 | 54                   | 49 | 01.04 | 77                 | 30 |    | 4                          | 56. | 932 | 77                   | 25 | 03.07 |
| 55                 | 30 |    | 10                         | 54. | 710 | 55                   | 19 | 05.29 | 78                 | 00 |    | 4                          | 45. | 790 | 77                   | 55 | 14.22 |
| 56                 | 00 |    | 10                         | 50. | 260 | 55                   | 49 | 09.74 | 78                 | 30 |    | 4                          | 34. | 541 | 78                   | 25 | 25.46 |
| 56                 | 30 |    | 10                         | 45. | 612 | 56                   | 19 | 14.39 | 79                 | 00 |    | 4                          | 23. | 218 | 78                   | 55 | 36.78 |
| 57                 | 00 |    | 10                         | 40. | 765 | 56                   | 49 | 19.23 | 79                 | 30 |    | 4                          | 11. | 813 | 79                   | 25 | 48.19 |
| 57                 | 30 |    | 10                         | 35. | 723 | 57                   | 19 | 24.28 | 80                 | 00 |    | 4                          | 00. | 331 | 79                   | 55 | 59.67 |
| 58                 | 00 |    | 10                         | 30. | 487 | 57                   | 49 | 29.51 | 80                 | 30 |    | 3                          | 48. | 775 | 80                   | 26 | 11.22 |
| 58                 | 30 |    | 10                         | 25. | 057 | 58                   | 19 | 34.94 | 81                 | 00 |    | 3                          | 37. | 149 | 80                   | 56 | 22.85 |
| 59                 | 00 |    | 10                         | 19. | 436 | 58                   | 49 | 40.56 | 81                 | 30 |    | 3                          | 25. | 456 | 81                   | 26 | 34.54 |
| 59                 | 30 |    | 10                         | 13. | 626 | 59                   | 19 | 46.37 | 82                 | 00 |    | 3                          | 13. | 699 | 81                   | 56 | 46.30 |
| 60                 | 00 |    | 10                         | 07. | 628 | 59                   | 49 | 52.37 | 82                 | 30 |    | 3                          | 01. | 843 | 82                   | 26 | 58.12 |
| 60                 | 30 |    | 10                         | 01. | 443 | 60                   | 19 | 58.56 | 83                 | 00 |    | 2                          | 50. | 012 | 82                   | 57 | 09.99 |
| 61                 | 00 |    | 9                          | 55. | 075 | 60                   | 50 | 04.93 | 83                 | 30 |    | 2                          | 38. | 088 | 83                   | 27 | 21.91 |
| 61                 | 30 |    | 9                          | 48. | 524 | 61                   | 20 | 11.48 | 84                 | 00 |    | 2                          | 26. | 115 | 83                   | 57 | 33.88 |
| 62                 | 00 |    | 9                          | 41. | 793 | 61                   | 50 | 18.21 | 84                 | 30 |    | 2                          | 14. | 097 | 84                   | 27 | 45.90 |
| 62                 | 30 |    | 9                          | 34. | 884 | 62                   | 20 | 25.12 | 85                 | 00 |    | 2                          | 02. | 038 | 84                   | 57 | 57.96 |
| 63                 | 00 |    | 9                          | 27. | 799 | 62                   | 50 | 32.20 | 85                 | 30 |    | 1                          | 49. | 941 | 85                   | 28 | 10.06 |
| 63                 | 30 |    | 9                          | 20. | 539 | 63                   | 20 | 39.46 | 86                 | 00 |    | 1                          | 37. | 811 | 85                   | 58 | 22.19 |
| 64                 | 00 |    | 9                          | 13. | 108 | 63                   | 50 | 46.89 | 86                 | 30 |    | 1                          | 25. | 651 | 86                   | 28 | 34.35 |
| 64                 | 30 |    | 9                          | 05. | 508 | 64                   | 20 | 54.49 | 87                 | 00 |    | 1                          | 13. | 464 | 86                   | 58 | 46.54 |
| 65                 | 00 |    | 8                          | 57. | 740 | 64                   | 51 | 02.26 | 87                 | 30 |    | 1                          | 01. | 254 | 87                   | 28 | 58.75 |
| 65                 | 30 |    | 8                          | 49. | 807 | 65                   | 21 | 10.19 | 88                 | 00 |    | 0                          | 49. | 026 | 87                   | 59 | 10.97 |
| 66                 | 00 |    | 8                          | 41. | 712 | 65                   | 51 | 18.29 | 88                 | 30 |    | 0                          | 36. | 783 | 88                   | 29 | 23.22 |
| 66                 | 30 |    | 8                          | 33. | 456 | 66                   | 21 | 26.54 | 89                 | 00 |    | 0                          | 24. | 528 | 88                   | 59 | 35.47 |
| 67                 | 00 |    | 8                          | 25. | 044 | 66                   | 51 | 34.96 | 89                 | 30 |    | 0                          | 12. | 266 | 89                   | 29 | 47.73 |
| 67                 | 30 |    | 8                          | 16. | 476 | 67                   | 21 | 43.52 | 90                 | 00 |    | 0                          | 00. | 000 | 90                   | 00 | 00.00 |

$$\varphi - \psi = +700''.4385 \sin 2\varphi - 1''.1893 \sin 4\varphi + 0''.0027 \sin 6\varphi.$$

$$\varphi - \psi = [2.8453700] \sin 2\varphi - [0.075285] \sin 4\varphi + [7.430 - 10] \sin 6\varphi.$$

LATITUDE TRANSFORMATION—Continued.

*Geocentric to geodetic.*

| Geocentric latitude. | Geodetic minus geocentric. | Geodetic latitude. | Geocentric latitude. | Geodetic minus geocentric. | Geodetic latitude. |
|----------------------|----------------------------|--------------------|----------------------|----------------------------|--------------------|
| $\psi$               | $\phi - \psi$              | $\phi$             | $\psi$               | $\phi - \psi$              | $\phi$             |
| 0 00                 | 0 00.000                   | 0 00 00.00         | 22 30                | 8 16.476                   | 22 38 16.48        |
| 0 30                 | 0 12.266                   | 0 30 12.27         | 23 00                | 8 25.044                   | 23 08 25.04        |
| 1 00                 | 0 24.528                   | 1 00 24.53         | 23 30                | 8 33.456                   | 23 38 33.46        |
| 1 30                 | 0 36.783                   | 1 30 36.78         | 24 00                | 8 41.712                   | 24 08 41.71        |
| 2 00                 | 0 49.026                   | 2 00 49.03         | 24 30                | 8 49.807                   | 24 38 49.81        |
| 2 30                 | 1 01.254                   | 2 31 01.25         | 25 00                | 8 57.740                   | 25 08 57.74        |
| 3 00                 | 1 13.464                   | 3 01 13.46         | 25 30                | 9 05.508                   | 25 39 05.51        |
| 3 30                 | 1 25.651                   | 3 31 25.65         | 26 00                | 9 13.108                   | 26 09 13.11        |
| 4 00                 | 1 37.811                   | 4 01 37.81         | 26 30                | 9 20.539                   | 26 39 20.54        |
| 4 30                 | 1 49.941                   | 4 31 49.94         | 27 00                | 9 27.799                   | 27 09 27.80        |
| 5 00                 | 2 02.038                   | 5 02 02.04         | 27 30                | 9 34.884                   | 27 39 34.88        |
| 5 30                 | 2 14.097                   | 5 32 14.10         | 28 00                | 9 41.793                   | 28 09 41.79        |
| 6 00                 | 2 26.115                   | 6 02 26.12         | 28 30                | 9 48.524                   | 28 39 48.52        |
| 6 30                 | 2 38.088                   | 6 32 38.09         | 29 00                | 9 55.075                   | 29 09 55.07        |
| 7 00                 | 2 50.012                   | 7 02 50.01         | 29 30                | 10 01.443                  | 29 40 01.44        |
| 7 30                 | 3 01.883                   | 7 33 01.88         | 30 00                | 10 07.628                  | 30 10 07.63        |
| 8 00                 | 3 13.699                   | 8 03 13.70         | 30 30                | 10 13.626                  | 30 40 13.63        |
| 8 30                 | 3 25.456                   | 8 33 25.46         | 31 00                | 10 19.430                  | 31 10 19.44        |
| 9 00                 | 3 37.149                   | 9 03 37.15         | 31 30                | 10 25.057                  | 31 40 25.06        |
| 9 30                 | 3 48.775                   | 9 33 48.78         | 32 00                | 10 30.437                  | 32 10 30.49        |
| 10 00                | 4 00.331                   | 10 04 00.33        | 32 30                | 10 35.723                  | 32 40 35.72        |
| 10 30                | 4 11.813                   | 10 34 11.81        | 33 00                | 10 40.765                  | 33 10 40.77        |
| 11 00                | 4 23.218                   | 11 04 23.22        | 33 30                | 10 45.612                  | 33 40 45.61        |
| 11 30                | 4 34.541                   | 11 34 34.54        | 34 00                | 10 50.260                  | 34 10 50.26        |
| 12 00                | 4 45.780                   | 12 04 45.78        | 34 30                | 10 54.710                  | 34 40 54.71        |
| 12 30                | 4 56.932                   | 12 34 56.93        | 35 00                | 10 58.960                  | 35 10 58.96        |
| 13 00                | 5 07.992                   | 13 05 07.99        | 35 30                | 11 03.008                  | 35 41 03.01        |
| 13 30                | 5 18.957                   | 13 35 18.96        | 36 00                | 11 06.854                  | 36 11 06.85        |
| 14 00                | 5 29.825                   | 14 05 29.83        | 36 30                | 11 10.496                  | 36 41 10.50        |
| 14 30                | 5 40.591                   | 14 35 40.59        | 37 00                | 11 13.933                  | 37 11 13.93        |
| 15 00                | 5 51.252                   | 15 05 51.25        | 37 30                | 11 17.164                  | 37 41 17.16        |
| 15 30                | 6 01.805                   | 15 36 01.81        | 38 00                | 11 20.189                  | 38 11 20.19        |
| 16 00                | 6 12.248                   | 16 06 12.25        | 38 30                | 11 23.006                  | 38 41 23.01        |
| 16 30                | 6 22.575                   | 16 36 22.58        | 39 00                | 11 25.614                  | 39 11 25.61        |
| 17 00                | 6 32.786                   | 17 06 32.79        | 39 30                | 11 28.013                  | 39 41 28.01        |
| 17 30                | 6 42.875                   | 17 36 42.88        | 40 00                | 11 30.202                  | 40 11 30.20        |
| 18 00                | 6 52.841                   | 18 06 52.84        | 40 30                | 11 32.180                  | 40 41 32.18        |
| 18 30                | 7 02.680                   | 18 37 02.68        | 41 00                | 11 33.947                  | 41 11 33.95        |
| 19 00                | 7 12.390                   | 19 07 12.39        | 41 30                | 11 35.503                  | 41 41 35.50        |
| 19 30                | 7 21.966                   | 19 37 21.97        | 42 00                | 11 36.846                  | 42 11 36.85        |
| 20 00                | 7 31.407                   | 20 07 31.41        | 42 30                | 11 37.977                  | 42 41 37.98        |
| 20 30                | 7 40.709                   | 20 37 40.71        | 43 00                | 11 38.895                  | 43 11 38.90        |
| 21 00                | 7 49.870                   | 21 07 49.87        | 43 30                | 11 39.600                  | 43 41 39.60        |
| 21 30                | 7 58.886                   | 21 37 58.89        | 44 00                | 11 40.092                  | 44 11 40.09        |
| 22 00                | 8 07.758                   | 22 08 07.76        | 44 30                | 11 40.371                  | 44 41 40.37        |
| 22 30                | 8 16.476                   | 22 38 16.48        | 45 00                | 11 40.436                  | 45 11 40.44        |

$$\phi - \psi = +700'' 4385 \sin 2\psi + 1'' 1893 \sin 4\psi + 0'' 0027 \sin 6\psi.$$

$$\phi - \psi = [2.8453700] \sin 2\psi + [0.0752855] \sin 4\psi + [7.430 - 10] \sin 6\psi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geocentric to geodetic—Continued.*

| Geocen-<br>tric lati-<br>tude. | Geodetic<br>minus<br>geocentric. | Geodetic<br>latitude. | Geocen-<br>tric lati-<br>tude. | Geodetic<br>minus<br>geocentric. | Geodetic<br>latitude. |
|--------------------------------|----------------------------------|-----------------------|--------------------------------|----------------------------------|-----------------------|
| $\psi$                         | $\varphi - \psi$                 | $\varphi$             | $\psi$                         | $\varphi - \psi$                 | $\varphi$             |
| ° ' "                          | ' "                              | ° ' "                 | ° ' "                          | ' "                              | ° ' "                 |
| 45 00                          | 11 40.436                        | 45 11 40.44           | 67 30                          | 8 14.097                         | 67 38 14.10           |
| 45 30                          | 11 40.298                        | 45 41 40.29           | 68 00                          | 8 05.379                         | 68 08 05.38           |
| 46 00                          | 11 39.926                        | 46 11 39.93           | 68 30                          | 7 56.513                         | 68 37 56.51           |
| 46 30                          | 11 39.352                        | 46 41 39.35           | 69 00                          | 7 47.504                         | 69 07 47.50           |
| 47 00                          | 11 38.564                        | 47 11 38.56           | 69 30                          | 7 38.354                         | 69 37 38.35           |
| 47 30                          | 11 37.564                        | 47 41 37.56           | 70 00                          | 7 29.064                         | 70 07 29.06           |
| 48 00                          | 11 36.352                        | 48 11 36.35           | 70 30                          | 7 19.639                         | 70 37 19.64           |
| 48 30                          | 11 34.927                        | 48 41 34.93           | 71 00                          | 7 10.082                         | 71 07 10.08           |
| 49 00                          | 11 33.292                        | 49 11 33.29           | 71 30                          | 7 00.394                         | 71 37 00.39           |
| 49 30                          | 11 31.445                        | 49 41 31.44           | 72 00                          | 6 50.579                         | 72 06 50.58           |
| 50 00                          | 11 29.388                        | 50 11 29.39           | 72 30                          | 6 40.640                         | 72 36 40.64           |
| 50 30                          | 11 27.122                        | 50 41 27.12           | 73 00                          | 6 30.580                         | 73 06 30.58           |
| 51 00                          | 11 24.646                        | 51 11 24.65           | 73 30                          | 6 20.402                         | 73 36 20.40           |
| 51 30                          | 11 21.963                        | 51 41 21.96           | 74 00                          | 6 10.110                         | 74 06 10.11           |
| 52 00                          | 11 19.072                        | 52 11 19.07           | 74 30                          | 5 59.705                         | 74 35 59.71           |
| 52 30                          | 11 15.975                        | 52 41 15.98           | 75 00                          | 5 49.192                         | 75 05 49.19           |
| 53 00                          | 11 12.673                        | 53 11 12.67           | 75 30                          | 5 38.573                         | 75 35 38.57           |
| 53 30                          | 11 09.166                        | 53 41 09.17           | 76 00                          | 5 27.833                         | 76 05 27.83           |
| 54 00                          | 11 05.456                        | 54 11 05.46           | 76 30                          | 5 17.033                         | 76 35 17.03           |
| 54 30                          | 11 01.544                        | 54 41 01.54           | 77 00                          | 5 06.117                         | 77 05 06.12           |
| 55 00                          | 10 57.431                        | 55 10 57.43           | 77 30                          | 4 55.110                         | 77 34 55.11           |
| 55 30                          | 10 53.119                        | 55 40 53.12           | 78 00                          | 4 44.013                         | 78 04 44.01           |
| 56 00                          | 10 48.508                        | 56 10 48.51           | 78 30                          | 4 32.830                         | 78 34 32.83           |
| 56 30                          | 10 43.900                        | 56 40 43.90           | 79 00                          | 4 21.565                         | 79 04 21.57           |
| 57 00                          | 10 38.998                        | 57 10 39.00           | 79 30                          | 4 10.221                         | 79 34 10.22           |
| 57 30                          | 10 33.901                        | 57 40 33.90           | 80 00                          | 3 58.802                         | 80 03 58.80           |
| 58 00                          | 10 28.612                        | 58 10 28.61           | 80 30                          | 3 47.311                         | 80 33 47.31           |
| 58 30                          | 10 23.133                        | 58 40 23.13           | 81 00                          | 3 35.750                         | 81 03 35.75           |
| 59 00                          | 10 17.464                        | 59 10 17.46           | 81 30                          | 3 24.126                         | 81 33 24.13           |
| 59 30                          | 10 11.609                        | 59 40 11.61           | 82 00                          | 3 12.439                         | 82 03 12.44           |
| 60 00                          | 10 05.568                        | 60 10 05.57           | 82 30                          | 3 00.694                         | 82 33 00.69           |
| 60 30                          | 9 59.343                         | 60 39 59.34           | 83 00                          | 2 48.895                         | 83 02 48.89           |
| 61 00                          | 9 52.937                         | 61 09 52.94           | 83 30                          | 2 37.045                         | 83 32 37.04           |
| 61 30                          | 9 46.351                         | 61 39 46.35           | 84 00                          | 2 25.147                         | 84 02 25.15           |
| 62 00                          | 9 39.588                         | 62 09 39.59           | 84 30                          | 2 13.206                         | 84 32 13.21           |
| 62 30                          | 9 32.649                         | 62 39 32.65           | 85 00                          | 2 01.224                         | 85 02 01.22           |
| 63 00                          | 9 25.536                         | 63 09 25.54           | 85 30                          | 1 49.206                         | 85 31 49.21           |
| 63 30                          | 9 18.253                         | 63 39 18.25           | 86 00                          | 1 37.156                         | 86 01 37.16           |
| 64 00                          | 9 10.800                         | 64 09 10.80           | 86 30                          | 1 25.075                         | 86 31 25.08           |
| 64 30                          | 9 03.181                         | 64 39 03.18           | 87 00                          | 1 12.969                         | 87 01 12.97           |
| 65 00                          | 8 55.397                         | 65 08 55.40           | 87 30                          | 1 00.841                         | 87 31 00.84           |
| 65 30                          | 8 47.451                         | 65 38 47.45           | 88 00                          | 0 48.695                         | 88 00 48.70           |
| 66 00                          | 8 39.346                         | 66 08 39.35           | 88 30                          | 0 36.534                         | 88 30 36.53           |
| 66 30                          | 8 31.084                         | 66 38 31.08           | 89 00                          | 0 24.362                         | 89 00 24.36           |
| 67 00                          | 8 22.666                         | 67 08 22.67           | 89 30                          | 0 12.183                         | 89 30 12.18           |
| 67 30                          | 8 14.097                         | 67 38 14.10           | 90 00                          | 0 00.000                         | 90 00 00.00           |

$$\varphi - \psi = +700''.4385 \sin 2\psi + 1''.1893 \sin 4\psi + 0''.0027 \sin 6\psi.$$

$$\varphi - \psi = [2.8453700] \sin 2\psi + [0.075285] \sin 4\psi + [7.430 - 10] \sin 6\psi.$$

LATITUDE TRANSFORMATION—Continued.

*Geodetic to parametric.*

| Geodetic latitude. |    | Geodetic minus parametric. |        | Parametric latitude. |    | Geodetic latitude. |            | Geodetic minus parametric. |   | Parametric latitude. |    |    |       |
|--------------------|----|----------------------------|--------|----------------------|----|--------------------|------------|----------------------------|---|----------------------|----|----|-------|
| $\varphi$          |    | $\varphi - \theta$         |        | $\theta$             |    | $\varphi$          |            | $\varphi - \theta$         |   | $\theta$             |    |    |       |
| $^{\circ}$         | '  | '                          | "      | $^{\circ}$           | '  | "                  | $^{\circ}$ | '                          | " | $^{\circ}$           | '  | "  |       |
| 0                  | 00 | 0                          | 00.000 | 0                    | 00 | 00.00              | 22         | 30                         | 4 | 07.346               | 22 | 25 | 52.65 |
| 0                  | 30 | 0                          | 06.103 | 0                    | 29 | 53.90              | 23         | 00                         | 4 | 11.630               | 22 | 55 | 48.37 |
| 1                  | 00 | 0                          | 12.202 | 0                    | 59 | 47.80              | 23         | 30                         | 4 | 15.898               | 23 | 25 | 44.16 |
| 1                  | 30 | 0                          | 18.298 | 1                    | 29 | 41.70              | 24         | 00                         | 4 | 19.959               | 23 | 55 | 40.03 |
| 2                  | 00 | 0                          | 24.389 | 1                    | 59 | 35.61              | 24         | 30                         | 4 | 24.020               | 24 | 25 | 35.98 |
| 2                  | 30 | 0                          | 30.472 | 2                    | 29 | 29.53              | 25         | 00                         | 4 | 27.992               | 24 | 55 | 32.01 |
| 3                  | 00 | 0                          | 36.546 | 2                    | 59 | 23.45              | 25         | 30                         | 4 | 31.882               | 25 | 25 | 28.12 |
| 3                  | 30 | 0                          | 42.609 | 3                    | 29 | 17.39              | 26         | 00                         | 4 | 35.689               | 25 | 55 | 24.31 |
| 4                  | 00 | 0                          | 48.659 | 3                    | 59 | 11.34              | 26         | 30                         | 4 | 39.413               | 26 | 25 | 20.59 |
| 4                  | 30 | 0                          | 54.695 | 4                    | 29 | 05.31              | 27         | 00                         | 4 | 43.052               | 26 | 55 | 16.95 |
| 5                  | 00 | 1                          | 00.714 | 4                    | 58 | 59.29              | 27         | 30                         | 4 | 4' 604               | 27 | 25 | 13.40 |
| 5                  | 30 | 1                          | 06.714 | 5                    | 28 | 53.29              | 28         | 00                         | 4 | 50.070               | 27 | 55 | 09.93 |
| 6                  | 00 | 1                          | 12.694 | 5                    | 58 | 47.31              | 28         | 30                         | 4 | 53.448               | 28 | 25 | 06.55 |
| 6                  | 30 | 1                          | 18.652 | 6                    | 28 | 41.35              | 29         | 00                         | 4 | 56.736               | 28 | 55 | 03.26 |
| 7                  | 00 | 1                          | 24.587 | 6                    | 58 | 35.41              | 29         | 30                         | 4 | 59.935               | 29 | 25 | 00.06 |
| 7                  | 30 | 1                          | 30.495 | 7                    | 28 | 29.50              | 30         | 00                         | 5 | 03.042               | 29 | 54 | 56.96 |
| 8                  | 00 | 1                          | 36.377 | 7                    | 58 | 23.62              | 30         | 30                         | 5 | 06.057               | 30 | 24 | 53.94 |
| 8                  | 30 | 1                          | 42.228 | 8                    | 28 | 17.77              | 31         | 00                         | 5 | 08.980               | 30 | 54 | 51.02 |
| 9                  | 00 | 1                          | 48.050 | 8                    | 58 | 11.95              | 31         | 30                         | 5 | 11.808               | 31 | 24 | 48.19 |
| 9                  | 30 | 1                          | 53.838 | 9                    | 28 | 06.16              | 32         | 00                         | 5 | 14.541               | 31 | 54 | 45.46 |
| 10                 | 00 | 1                          | 59.592 | 9                    | 58 | 00.41              | 32         | 30                         | 5 | 17.180               | 32 | 24 | 42.82 |
| 10                 | 30 | 2                          | 05.309 | 10                   | 27 | 54.69              | 33         | 00                         | 5 | 19.721               | 32 | 54 | 40.28 |
| 11                 | 00 | 2                          | 10.989 | 10                   | 57 | 49.01              | 33         | 30                         | 5 | 22.165               | 33 | 24 | 37.84 |
| 11                 | 30 | 2                          | 16.628 | 11                   | 27 | 43.37              | 34         | 00                         | 5 | 24.512               | 33 | 54 | 35.49 |
| 12                 | 00 | 2                          | 22.227 | 11                   | 57 | 37.77              | 34         | 30                         | 5 | 26.760               | 34 | 24 | 33.24 |
| 12                 | 30 | 2                          | 27.782 | 12                   | 27 | 32.22              | 35         | 00                         | 5 | 28.908               | 34 | 54 | 31.09 |
| 13                 | 00 | 2                          | 33.292 | 12                   | 57 | 26.71              | 35         | 30                         | 5 | 30.957               | 35 | 24 | 29.04 |
| 13                 | 30 | 2                          | 38.756 | 13                   | 27 | 21.24              | 36         | 00                         | 5 | 32.904               | 35 | 54 | 27.10 |
| 14                 | 00 | 2                          | 44.172 | 13                   | 57 | 15.83              | 36         | 30                         | 5 | 34.751               | 36 | 24 | 25.25 |
| 14                 | 30 | 2                          | 49.538 | 14                   | 27 | 10.46              | 37         | 00                         | 5 | 36.496               | 36 | 54 | 23.50 |
| 15                 | 00 | 2                          | 54.853 | 14                   | 57 | 05.15              | 37         | 30                         | 5 | 38.138               | 37 | 24 | 21.86 |
| 15                 | 30 | 3                          | 00.114 | 15                   | 26 | 59.89              | 38         | 00                         | 5 | 39.677               | 37 | 54 | 20.32 |
| 16                 | 00 | 3                          | 05.321 | 15                   | 56 | 54.68              | 38         | 30                         | 5 | 41.114               | 38 | 24 | 18.89 |
| 16                 | 30 | 3                          | 10.472 | 16                   | 26 | 49.53              | 39         | 00                         | 5 | 42.446               | 38 | 54 | 17.55 |
| 17                 | 00 | 3                          | 15.565 | 16                   | 56 | 44.43              | 39         | 30                         | 5 | 43.674               | 39 | 24 | 16.33 |
| 17                 | 30 | 3                          | 20.599 | 17                   | 26 | 39.40              | 40         | 00                         | 5 | 44.798               | 39 | 54 | 15.20 |
| 18                 | 00 | 3                          | 25.572 | 17                   | 56 | 34.43              | 40         | 30                         | 5 | 45.816               | 40 | 24 | 14.18 |
| 18                 | 30 | 3                          | 30.482 | 18                   | 26 | 29.52              | 41         | 00                         | 5 | 46.730               | 40 | 54 | 13.27 |
| 19                 | 00 | 3                          | 35.329 | 18                   | 56 | 24.67              | 41         | 30                         | 5 | 47.538               | 41 | 24 | 12.46 |
| 19                 | 30 | 3                          | 40.110 | 19                   | 26 | 19.59              | 42         | 00                         | 5 | 48.240               | 41 | 54 | 11.76 |
| 20                 | 00 | 3                          | 44.825 | 19                   | 56 | 15.18              | 42         | 30                         | 5 | 48.836               | 42 | 24 | 11.16 |
| 20                 | 30 | 3                          | 49.471 | 20                   | 26 | 10.53              | 43         | 00                         | 5 | 49.325               | 42 | 54 | 10.67 |
| 21                 | 00 | 3                          | 54.048 | 20                   | 56 | 05.95              | 43         | 30                         | 5 | 49.709               | 43 | 24 | 10.29 |
| 21                 | 30 | 3                          | 58.553 | 21                   | 26 | 01.45              | 44         | 00                         | 5 | 49.986               | 43 | 54 | 10.01 |
| 22                 | 00 | 4                          | 02.987 | 21                   | 55 | 57.01              | 44         | 30                         | 5 | 50.156               | 44 | 24 | 09.84 |
| 22                 | 30 | 4                          | 07.346 | 22                   | 25 | 52.65              | 45         | 00                         | 5 | 50.220               | 44 | 54 | 09.78 |

$$\varphi - \theta = +350''.2203 \sin 2\varphi - 0''.2973 \sin 4\varphi + 0''.0003 \sin 6\varphi.$$

$$\varphi - \theta = [2.5443412] \sin 2\varphi - [0.47323 - 10] \sin 4\varphi + [0.537 - 10] \sin 6\varphi.$$



## LATITUDE TRANSFORMATION—Continued.

*Geodetic to parametric—Continued.*

| Geodetic latitude. | Geodetic minus parametric. | Parametric latitude. | Geodetic latitude. | Geodetic minus parametric. | Parametric latitude. |
|--------------------|----------------------------|----------------------|--------------------|----------------------------|----------------------|
| $\varphi$          | $\varphi - \theta$         | $\theta$             | $\varphi$          | $\varphi - \theta$         | $\theta$             |
| 45 00              | 5 50.220                   | 44 54 09.78          | 67 30              | 4 07.941                   | 67 25 52.06          |
| 45 30              | 5 50.177                   | 45 24 09.82          | 68 00              | 4 03.581                   | 67 55 58.42          |
| 46 00              | 5 50.027                   | 45 54 09.97          | 68 30              | 3 59.146                   | 68 26 00.85          |
| 46 30              | 5 49.771                   | 46 24 10.23          | 69 00              | 3 54.639                   | 68 56 05.30          |
| 47 00              | 5 49.408                   | 46 54 10.59          | 69 30              | 3 50.060                   | 69 26 09.94          |
| 47 30              | 5 48.939                   | 47 24 11.06          | 70 00              | 3 45.410                   | 69 56 14.59          |
| 48 00              | 5 48.363                   | 47 54 11.64          | 70 30              | 3 40.692                   | 70 26 19.31          |
| 48 30              | 5 47.681                   | 48 24 12.32          | 71 00              | 3 35.906                   | 70 56 24.09          |
| 49 00              | 5 46.894                   | 48 54 13.11          | 71 30              | 3 31.054                   | 71 26 28.95          |
| 49 30              | 5 46.000                   | 49 24 14.00          | 72 00              | 3 26.137                   | 71 56 33.86          |
| 50 00              | 5 45.001                   | 49 54 15.00          | 72 30              | 3 21.158                   | 72 26 38.84          |
| 50 30              | 5 43.897                   | 50 24 16.10          | 73 00              | 3 16.117                   | 72 56 43.88          |
| 51 00              | 5 42.688                   | 50 54 17.31          | 73 30              | 3 11.016                   | 73 26 48.98          |
| 51 30              | 5 41.374                   | 51 24 18.63          | 74 00              | 3 05.856                   | 73 56 54.14          |
| 52 00              | 5 39.957                   | 51 54 20.04          | 74 30              | 3 00.640                   | 74 26 59.36          |
| 52 30              | 5 38.435                   | 52 24 21.56          | 75 00              | 2 55.368                   | 74 57 04.63          |
| 53 00              | 5 36.811                   | 52 54 23.19          | 75 30              | 2 50.042                   | 75 27 09.96          |
| 53 30              | 5 35.083                   | 53 24 24.92          | 76 00              | 2 44.665                   | 75 57 15.34          |
| 54 00              | 5 33.254                   | 53 54 26.75          | 76 30              | 2 39.237                   | 76 27 20.76          |
| 54 30              | 5 31.322                   | 54 24 28.68          | 77 00              | 2 33.761                   | 76 57 26.24          |
| 55 00              | 5 29.290                   | 54 54 30.71          | 77 30              | 2 28.238                   | 77 27 31.76          |
| 55 30              | 5 27.158                   | 55 24 32.84          | 78 00              | 2 22.669                   | 77 57 37.33          |
| 56 00              | 5 24.925                   | 55 54 35.08          | 78 30              | 2 17.056                   | 78 27 42.94          |
| 56 30              | 5 22.593                   | 56 24 37.41          | 79 00              | 2 11.402                   | 78 57 48.60          |
| 57 00              | 5 20.163                   | 56 54 39.84          | 79 30              | 2 05.707                   | 79 27 54.29          |
| 57 30              | 5 17.635                   | 57 24 42.36          | 80 00              | 1 59.974                   | 79 58 00.03          |
| 58 00              | 5 15.010                   | 57 54 44.99          | 80 30              | 1 54.204                   | 80 28 05.80          |
| 58 30              | 5 12.289                   | 58 24 47.71          | 81 00              | 1 48.399                   | 80 58 11.60          |
| 59 00              | 5 09.473                   | 58 54 50.53          | 81 30              | 1 42.561                   | 81 28 17.44          |
| 59 30              | 5 06.562                   | 59 24 53.44          | 82 00              | 1 36.692                   | 81 58 23.31          |
| 60 00              | 5 03.557                   | 59 54 56.44          | 82 30              | 1 30.792                   | 82 28 29.21          |
| 60 30              | 5 00.460                   | 60 24 59.54          | 83 00              | 1 24.866                   | 82 58 35.13          |
| 61 00              | 4 57.271                   | 60 55 02.73          | 83 30              | 1 18.913                   | 83 28 41.09          |
| 61 30              | 4 53.991                   | 61 25 06.01          | 84 00              | 1 12.936                   | 83 58 47.06          |
| 62 00              | 4 50.622                   | 61 55 09.38          | 84 30              | 1 06.937                   | 84 28 53.06          |
| 62 30              | 4 47.163                   | 62 25 12.84          | 85 00              | 1 00.917                   | 84 58 59.08          |
| 63 00              | 4 43.617                   | 62 55 16.38          | 85 30              | 0 54.878                   | 85 29 05.12          |
| 63 30              | 4 39.984                   | 63 25 20.02          | 86 00              | 0 48.823                   | 85 59 11.18          |
| 64 00              | 4 36.266                   | 63 55 23.73          | 86 30              | 0 42.753                   | 86 29 17.25          |
| 64 30              | 4 32.463                   | 64 25 27.54          | 87 00              | 0 36.670                   | 86 59 23.33          |
| 65 00              | 4 28.577                   | 64 55 31.42          | 87 30              | 0 30.575                   | 87 29 29.42          |
| 65 30              | 4 24.600                   | 65 25 35.39          | 88 00              | 0 24.472                   | 87 59 35.53          |
| 66 00              | 4 20.560                   | 65 55 39.44          | 88 30              | 0 18.360                   | 88 29 41.64          |
| 66 30              | 4 16.432                   | 66 25 43.57          | 89 00              | 0 12.243                   | 88 59 47.76          |
| 67 00              | 4 12.225                   | 66 55 47.78          | 89 30              | 0 06.123                   | 89 29 53.88          |
| 67 30              | 4 07.941                   | 67 25 52.06          | 90 00              | 0 00.000                   | 90 00 00.00          |

$$\varphi - \theta = +350''.2202 \sin 2\varphi - 0''.2973 \sin 4\varphi + 0''.0003 \sin 6\varphi.$$

$$\varphi - \theta = [2.5443412] \sin 2\varphi - [9.47823 - 10] \sin 4\varphi + [0.527 - 10] \sin 6\varphi.$$

LATITUDE TRANSFORMATION—Continued.

*Parametric to geodetic.*

| Para-<br>metric<br>latitude. | Geodetic<br>minus<br>parametric. | Geodetic<br>latitude. | Para-<br>metric<br>latitude. | Geodetic<br>minus<br>parametric. | Geodetic<br>latitude. |
|------------------------------|----------------------------------|-----------------------|------------------------------|----------------------------------|-----------------------|
| $\theta$                     | $\varphi-\theta$                 | $\varphi$             | $\theta$                     | $\varphi-\theta$                 | $\varphi$             |
| 0 00                         | 0 00.000                         | 0 00 00.00            | 22 30                        | 4 07.941                         | 22 34 07.94           |
| 0 30                         | 0 06.123                         | 0 30 06.12            | 23 00                        | 4 12.225                         | 23 04 12.22           |
| 1 00                         | 0 12.243                         | 1 00 12.24            | 23 30                        | 4 16.432                         | 23 34 16.43           |
| 1 30                         | 0 18.360                         | 1 30 18.36            | 24 00                        | 4 20.560                         | 24 04 20.56           |
| 2 00                         | 0 24.472                         | 2 00 24.47            | 24 30                        | 4 24.609                         | 24 34 24.61           |
| 2 30                         | 6 30.575                         | 2 30 30.58            | 25 00                        | 4 28.577                         | 25 04 28.58           |
| 3 00                         | 0 36.670                         | 3 00 36.67            | 25 30                        | 4 32.463                         | 25 34 32.46           |
| 3 30                         | 0 42.753                         | 3 30 42.75            | 26 00                        | 4 36.266                         | 26 04 36.27           |
| 4 00                         | 0 48.823                         | 4 00 48.82            | 26 30                        | 4 39.984                         | 26 34 39.98           |
| 4 30                         | 0 54.878                         | 4 30 54.88            | 27 00                        | 4 43.617                         | 27 04 43.62           |
| 5 00                         | 1 00.917                         | 5 01 00.92            | 27 30                        | 4 47.163                         | 27 34 47.16           |
| 5 30                         | 1 06.937                         | 5 31 06.94            | 28 00                        | 4 50.622                         | 28 04 50.62           |
| 6 00                         | 1 12.936                         | 6 01 12.94            | 28 30                        | 4 53.991                         | 28 34 53.99           |
| 6 30                         | 1 18.913                         | 6 31 18.91            | 29 00                        | 4 57.271                         | 29 04 57.27           |
| 7 00                         | 1 24.866                         | 7 01 24.87            | 29 30                        | 5 00.460                         | 29 35 00.46           |
| 7 30                         | 1 30.792                         | 7 31 30.79            | 30 00                        | 5 03.557                         | 30 05 03.56           |
| 8 00                         | 1 36.692                         | 8 01 36.69            | 30 30                        | 5 06.562                         | 30 35 06.56           |
| 8 30                         | 1 42.561                         | 8 31 42.56            | 31 00                        | 5 09.473                         | 31 05 09.47           |
| 9 00                         | 1 48.399                         | 9 01 48.40            | 31 30                        | 5 12.289                         | 31 35 12.29           |
| 9 30                         | 1 54.204                         | 9 31 54.20            | 32 00                        | 5 15.010                         | 32 05 15.01           |
| 10 00                        | 1 59.974                         | 10 01 59.97           | 32 30                        | 5 17.635                         | 32 35 17.64           |
| 10 30                        | 2 05.707                         | 10 32 05.71           | 33 00                        | 5 20.163                         | 33 05 20.16           |
| 11 00                        | 2 11.402                         | 11 02 11.40           | 33 30                        | 5 22.593                         | 33 35 22.59           |
| 11 30                        | 2 17.056                         | 11 32 17.06           | 34 00                        | 5 24.925                         | 34 05 24.92           |
| 12 00                        | 2 22.669                         | 12 02 22.67           | 34 30                        | 5 27.158                         | 34 35 27.16           |
| 12 30                        | 2 28.238                         | 12 32 28.24           | 35 00                        | 5 29.290                         | 35 05 29.29           |
| 13 00                        | 2 33.761                         | 13 02 33.76           | 35 30                        | 5 31.322                         | 35 35 31.32           |
| 13 30                        | 2 39.237                         | 13 32 39.24           | 36 00                        | 5 33.254                         | 36 05 33.25           |
| 14 00                        | 2 44.665                         | 14 02 44.66           | 36 30                        | 5 35.083                         | 36 35 35.08           |
| 14 30                        | 2 50.042                         | 14 32 50.04           | 37 00                        | 5 36.811                         | 37 05 36.81           |
| 15 00                        | 2 55.368                         | 15 02 55.37           | 37 30                        | 5 38.435                         | 37 35 38.44           |
| 15 30                        | 3 00.610                         | 15 33 00.64           | 38 00                        | 5 39.957                         | 38 05 39.96           |
| 16 00                        | 3 05.856                         | 16 03 05.86           | 38 30                        | 5 41.374                         | 38 35 41.37           |
| 16 30                        | 3 11.016                         | 16 33 11.02           | 39 00                        | 5 42.688                         | 39 05 42.69           |
| 17 00                        | 3 16.117                         | 17 03 16.12           | 39 30                        | 5 43.897                         | 39 35 43.90           |
| 17 30                        | 3 21.158                         | 17 33 21.16           | 40 00                        | 5 45.001                         | 40 05 45.00           |
| 18 00                        | 3 26.137                         | 18 03 26.14           | 40 30                        | 5 46.000                         | 40 35 46.00           |
| 18 30                        | 3 31.054                         | 18 33 31.05           | 41 00                        | 5 46.894                         | 41 05 46.89           |
| 19 00                        | 3 35.906                         | 19 03 35.91           | 41 30                        | 5 47.681                         | 41 35 47.68           |
| 19 30                        | 3 40.692                         | 19 33 40.69           | 42 00                        | 5 48.363                         | 42 05 48.36           |
| 20 00                        | 3 45.410                         | 20 03 45.41           | 42 30                        | 5 48.939                         | 42 35 48.94           |
| 20 30                        | 3 50.060                         | 20 33 50.06           | 43 00                        | 5 49.408                         | 43 05 49.41           |
| 21 00                        | 3 54.639                         | 21 03 54.64           | 43 30                        | 5 49.771                         | 43 35 49.77           |
| 21 30                        | 3 59.146                         | 21 33 59.15           | 44 00                        | 5 50.027                         | 44 05 50.03           |
| 22 00                        | 4 03.581                         | 22 04 03.58           | 44 30                        | 5 50.177                         | 44 35 50.18           |
| 22 30                        | 4 07.941                         | 22 34 07.94           | 45 00                        | 5 50.220                         | 45 05 50.22           |

$$\varphi-\theta = +350^{\circ}2202 \sin 2\theta + 0^{\circ}2973 \sin 4\theta + 0^{\circ}0003 \sin 6\theta.$$

$$\varphi-\theta = [2.5443412] \sin 2\theta + [0.47323-10] \sin 4\theta + [6.527-10] \sin 6\theta.$$

## LATITUDE TRANSFORMATION—Continued.

Parametric to geodetic—Continued.

| Parametric latitude. | Geodetic minus parametric. | Geodetic latitude. | Parametric latitude. | Geodetic minus parametric. | Geodetic latitude. |
|----------------------|----------------------------|--------------------|----------------------|----------------------------|--------------------|
| $\theta$             | $\varphi - \theta$         | $\varphi$          | $\theta$             | $\varphi - \theta$         | $\varphi$          |
| ° ' "                | ' "                        | ° ' "              | ° ' "                | ' "                        | ° ' "              |
| 45 00                | 5 50.220                   | 45 05 50.22        | 67 30                | 4 07.346                   | 67 34 07.35        |
| 45 30                | 5 50.156                   | 45 35 50.16        | 68 00                | 4 02.987                   | 68 04 02.99        |
| 46 00                | 5 49.986                   | 46 05 49.99        | 68 30                | 3 58.553                   | 68 33 58.55        |
| 46 30                | 5 49.709                   | 46 35 49.71        | 69 00                | 3 54.048                   | 69 03 54.05        |
| 47 00                | 5 49.325                   | 47 05 49.33        | 69 30                | 3 49.471                   | 69 33 49.47        |
| 47 30                | 5 48.836                   | 47 35 48.84        | 70 00                | 3 44.825                   | 70 03 44.82        |
| 48 00                | 5 48.240                   | 48 05 48.24        | 70 30                | 3 40.110                   | 70 33 40.11        |
| 48 30                | 5 47.538                   | 48 35 47.54        | 71 00                | 3 35.329                   | 71 03 35.33        |
| 49 00                | 5 46.730                   | 49 05 46.73        | 71 30                | 3 30.482                   | 71 33 30.48        |
| 49 30                | 5 45.816                   | 49 35 45.82        | 72 00                | 3 25.572                   | 72 03 25.57        |
| 50 00                | 5 44.798                   | 50 05 44.80        | 72 30                | 3 20.569                   | 72 33 20.60        |
| 50 30                | 5 43.674                   | 50 35 43.67        | 73 00                | 3 15.565                   | 73 03 15.57        |
| 51 00                | 5 42.446                   | 51 05 42.45        | 73 30                | 3 10.472                   | 73 33 10.47        |
| 51 30                | 5 41.114                   | 51 35 41.11        | 74 00                | 3 05.321                   | 74 03 05.32        |
| 52 00                | 5 39.677                   | 52 05 39.68        | 74 30                | 3 00.114                   | 74 33 00.11        |
| 52 30                | 5 38.138                   | 52 35 38.14        | 75 00                | 2 54.853                   | 75 02 54.85        |
| 53 00                | 5 36.496                   | 53 05 36.50        | 75 30                | 2 49.538                   | 75 32 49.54        |
| 53 30                | 5 34.751                   | 53 35 34.75        | 76 00                | 2 44.172                   | 76 02 44.17        |
| 54 00                | 5 32.904                   | 54 05 32.90        | 76 30                | 2 38.756                   | 76 32 38.76        |
| 54 30                | 5 30.957                   | 54 35 30.96        | 77 00                | 2 33.292                   | 77 02 33.29        |
| 55 00                | 5 28.908                   | 55 05 28.91        | 77 30                | 2 27.782                   | 77 32 27.78        |
| 55 30                | 5 26.760                   | 55 35 26.76        | 78 00                | 2 22.227                   | 78 02 22.23        |
| 56 00                | 5 24.512                   | 56 05 24.51        | 78 30                | 2 16.628                   | 78 32 16.63        |
| 56 30                | 5 22.165                   | 56 35 22.16        | 79 00                | 2 10.989                   | 79 02 10.99        |
| 57 00                | 5 19.721                   | 57 05 19.72        | 79 30                | 2 05.309                   | 79 32 05.31        |
| 57 30                | 5 17.180                   | 57 35 17.18        | 80 00                | 1 59.592                   | 80 01 59.59        |
| 58 00                | 5 14.541                   | 58 05 14.54        | 80 30                | 1 53.838                   | 80 31 53.84        |
| 58 30                | 5 11.808                   | 58 35 11.81        | 81 00                | 1 48.050                   | 81 01 48.05        |
| 59 00                | 5 08.980                   | 59 05 08.98        | 81 30                | 1 42.228                   | 81 31 42.23        |
| 59 30                | 5 06.057                   | 59 35 06.06        | 82 00                | 1 36.377                   | 82 01 36.38        |
| 60 00                | 5 03.042                   | 60 05 03.04        | 82 30                | 1 30.495                   | 82 31 30.50        |
| 60 30                | 4 59.935                   | 60 34 59.94        | 83 00                | 1 24.587                   | 83 01 24.59        |
| 61 00                | 4 56.736                   | 61 04 56.74        | 83 30                | 1 18.652                   | 83 31 18.65        |
| 61 30                | 4 53.448                   | 61 34 53.45        | 84 00                | 1 12.694                   | 84 01 12.69        |
| 62 00                | 4 50.070                   | 62 04 50.07        | 84 30                | 1 06.714                   | 84 31 06.71        |
| 62 30                | 4 46.604                   | 62 34 46.60        | 85 00                | 1 00.714                   | 85 01 00.71        |
| 63 00                | 4 43.052                   | 63 04 43.05        | 85 30                | 0 54.695                   | 85 30 54.69        |
| 63 30                | 4 39.413                   | 63 34 39.41        | 86 00                | 0 48.659                   | 86 00 48.66        |
| 64 00                | 4 35.689                   | 64 04 35.69        | 86 30                | 0 42.609                   | 86 30 42.61        |
| 64 30                | 4 31.882                   | 64 34 31.88        | 87 00                | 0 36.546                   | 87 00 36.55        |
| 65 00                | 4 27.992                   | 65 04 27.99        | 87 30                | 0 30.472                   | 87 30 30.47        |
| 65 30                | 4 24.020                   | 65 34 24.02        | 88 00                | 0 24.389                   | 88 00 24.39        |
| 66 00                | 4 19.969                   | 66 04 19.97        | 88 30                | 0 18.298                   | 88 30 18.30        |
| 66 30                | 4 15.838                   | 66 34 15.84        | 89 00                | 0 12.202                   | 89 00 12.20        |
| 67 00                | 4 11.630                   | 67 04 11.63        | 89 30                | 0 06.102                   | 89 30 06.10        |
| 67 30                | 4 07.346                   | 67 34 07.35        | 90 00                | 0 00.000                   | 90 00 00.00        |

$$\varphi - \theta = +35^{\circ} 22' 02'' \sin 2\theta + 0^{\circ} 29' 73'' \sin 4\theta + 0^{\circ} 00' 03'' \sin 6\theta.$$

$$\varphi - \theta = [2.5443412] \sin 2\theta + [9.47323 - 10] \sin 4\theta + [6.527 - 10] \sin 6\theta.$$

LATITUDE TRANSFORMATION—Continued.

*Parametric to geocentric.*

| Parametric latitude. | Parametric minus geocentric. | Geocentric latitude. | Parametric latitude. | Parametric minus geocentric. | Geocentric latitude. |
|----------------------|------------------------------|----------------------|----------------------|------------------------------|----------------------|
| $\theta$             | $\theta - \psi$              | $\psi$               | $\theta$             | $\theta - \psi$              | $\psi$               |
| 0 00                 | 0 00.000                     | 0 00 00.00           | 22 30                | 4 07.346                     | 22 25 52.65          |
| 0 30                 | 0 06.102                     | 0 29 53.90           | 23 00                | 4 11.630                     | 22 55 49.37          |
| 1 00                 | 0 12.202                     | 0 59 47.80           | 23 30                | 4 15.838                     | 23 25 44.16          |
| 1 30                 | 0 18.298                     | 1 29 41.70           | 24 00                | 4 19.969                     | 23 55 40.03          |
| 2 00                 | 0 24.389                     | 1 59 35.61           | 24 30                | 4 24.020                     | 24 25 35.06          |
| 2 30                 | 0 30.472                     | 2 29 29.53           | 25 00                | 4 27.992                     | 24 55 32.01          |
| 3 00                 | 0 36.546                     | 2 59 23.45           | 25 30                | 4 31.882                     | 25 25 28.12          |
| 3 30                 | 0 42.609                     | 3 29 17.39           | 26 00                | 4 35.689                     | 25 55 24.31          |
| 4 00                 | 0 48.659                     | 3 59 11.34           | 26 30                | 4 39.413                     | 26 25 20.59          |
| 4 30                 | 0 54.695                     | 4 29 05.31           | 27 00                | 4 43.052                     | 26 55 16.95          |
| 5 00                 | 1 00.714                     | 4 58 59.29           | 27 30                | 4 46.604                     | 27 25 13.40          |
| 5 30                 | 1 06.714                     | 5 28 53.29           | 28 00                | 4 50.070                     | 27 55 09.93          |
| 6 00                 | 1 12.694                     | 5 58 47.31           | 28 30                | 4 53.448                     | 28 25 06.55          |
| 6 30                 | 1 18.652                     | 6 28 41.35           | 29 00                | 4 56.736                     | 28 55 03.26          |
| 7 00                 | 1 24.587                     | 6 58 35.41           | 29 30                | 4 59.935                     | 29 25 00.06          |
| 7 30                 | 1 30.495                     | 7 28 29.50           | 30 00                | 5 03.042                     | 29 54 56.96          |
| 8 00                 | 1 36.377                     | 7 58 23.62           | 30 30                | 5 06.057                     | 30 24 53.94          |
| 8 30                 | 1 42.228                     | 8 28 17.77           | 31 00                | 5 08.980                     | 30 54 51.02          |
| 9 00                 | 1 48.050                     | 8 58 11.95           | 31 30                | 5 11.808                     | 31 24 48.19          |
| 9 30                 | 1 53.838                     | 9 28 06.16           | 32 00                | 5 14.541                     | 31 54 45.46          |
| 10 00                | 1 59.592                     | 9 58 00.41           | 32 30                | 5 17.180                     | 32 24 42.82          |
| 10 30                | 2 05.309                     | 10 27 54.69          | 33 00                | 5 19.721                     | 32 54 40.28          |
| 11 00                | 2 10.989                     | 10 57 49.01          | 33 30                | 5 22.165                     | 33 24 37.84          |
| 11 30                | 2 16.628                     | 11 27 43.37          | 34 00                | 5 24.512                     | 33 54 35.49          |
| 12 00                | 2 22.227                     | 11 57 37.77          | 34 30                | 5 26.760                     | 34 24 33.24          |
| 12 30                | 2 27.782                     | 12 27 32.22          | 35 00                | 5 28.908                     | 34 54 31.09          |
| 13 00                | 2 33.292                     | 12 57 26.71          | 35 30                | 5 30.957                     | 35 24 29.04          |
| 13 30                | 2 38.756                     | 13 27 21.24          | 36 00                | 5 32.904                     | 35 54 27.10          |
| 14 00                | 2 44.172                     | 13 57 15.83          | 36 30                | 5 34.751                     | 36 24 25.25          |
| 14 30                | 2 49.538                     | 14 27 10.46          | 37 00                | 5 36.496                     | 36 54 23.50          |
| 15 00                | 2 54.853                     | 14 57 05.15          | 37 30                | 5 38.138                     | 37 24 21.86          |
| 15 30                | 3 00.114                     | 15 26 59.89          | 38 00                | 5 39.677                     | 37 54 20.32          |
| 16 00                | 3 05.321                     | 15 56 54.68          | 38 30                | 5 41.114                     | 38 24 18.89          |
| 16 30                | 3 10.472                     | 16 26 49.53          | 39 00                | 5 42.446                     | 38 54 17.55          |
| 17 00                | 3 15.565                     | 16 56 44.43          | 39 30                | 5 43.674                     | 39 24 16.33          |
| 17 30                | 3 20.599                     | 17 26 39.40          | 40 00                | 5 44.798                     | 39 54 15.20          |
| 18 00                | 3 25.572                     | 17 56 34.43          | 40 30                | 5 45.816                     | 40 24 14.18          |
| 18 30                | 3 30.482                     | 18 26 29.52          | 41 00                | 5 46.730                     | 40 54 13.27          |
| 19 00                | 3 35.329                     | 18 56 24.67          | 41 30                | 5 47.538                     | 41 24 12.46          |
| 19 30                | 3 40.110                     | 19 26 19.89          | 42 00                | 5 48.240                     | 41 54 11.76          |
| 20 00                | 3 44.825                     | 19 56 15.18          | 42 30                | 5 48.836                     | 42 24 11.16          |
| 20 30                | 3 49.471                     | 20 26 10.53          | 43 00                | 5 49.325                     | 42 54 10.67          |
| 21 00                | 3 54.048                     | 20 56 05.95          | 43 30                | 5 49.709                     | 43 24 10.29          |
| 21 30                | 3 58.553                     | 21 26 01.45          | 44 00                | 5 49.986                     | 43 54 10.01          |
| 22 00                | 4 02.987                     | 21 55 57.01          | 44 30                | 5 50.156                     | 44 24 09.84          |
| 22 30                | 4 07.346                     | 22 25 52.65          | 45 00                | 5 50.220                     | 44 54 09.78          |

$$\theta - \psi = +350^{\circ}22'02'' \sin 2\theta - 0^{\circ}20'73'' \sin 4\theta + 0^{\circ}00'03'' \sin 6\theta.$$

$$\theta - \psi = [2.5443412] \sin 2\theta - [9.47323 - 10] \sin 4\theta + [6.527 - 10] \sin 6\theta.$$

## LATITUDE TRANSFORMATION—Continued.

*Parametric to geocentric—Continued.*

| Para-<br>metric<br>latitude. | Parametric<br>minus<br>geocentric. | Geocentric<br>latitude. | Para-<br>metric<br>latitude. | Parametric<br>minus<br>geocentric. | Geocentric<br>latitude. |
|------------------------------|------------------------------------|-------------------------|------------------------------|------------------------------------|-------------------------|
| $\theta$                     | $\theta-\psi$                      | $\psi$                  | $\theta$                     | $\theta-\psi$                      | $\psi$                  |
| ° ' "                        | ' "                                | ° ' "                   | ° ' "                        | ' "                                | ° ' "                   |
| 45 00                        | 5 50.220                           | 44 54 09.78             | 67 30                        | 4 07.941                           | 67 25 52.06             |
| 45 30                        | 5 50.177                           | 45 24 09.82             | 68 00                        | 4 03.581                           | 67 55 56.42             |
| 46 00                        | 5 50.027                           | 45 54 09.97             | 68 30                        | 3 59.146                           | 68 26 00.85             |
| 46 30                        | 5 49.771                           | 46 24 10.23             | 69 00                        | 3 54.639                           | 68 56 05.36             |
| 47 00                        | 5 49.408                           | 46 54 10.59             | 69 30                        | 3 50.060                           | 69 26 09.94             |
| 47 30                        | 5 48.939                           | 47 24 11.06             | 70 00                        | 3 45.410                           | 69 56 14.59             |
| 48 00                        | 5 48.363                           | 47 54 11.64             | 70 30                        | 3 40.692                           | 70 26 19.31             |
| 48 30                        | 5 47.681                           | 48 24 12.32             | 71 00                        | 3 35.906                           | 70 56 24.09             |
| 49 00                        | 5 46.894                           | 48 54 13.11             | 71 30                        | 3 31.054                           | 71 26 28.05             |
| 49 30                        | 5 46.000                           | 49 24 14.00             | 72 00                        | 3 26.137                           | 71 56 33.86             |
| 50 00                        | 5 45.001                           | 49 54 15.00             | 72 30                        | 3 21.158                           | 72 26 38.84             |
| 50 30                        | 5 43.897                           | 50 24 16.10             | 73 00                        | 3 16.117                           | 72 56 43.83             |
| 51 00                        | 5 42.688                           | 50 54 17.31             | 73 30                        | 3 11.016                           | 73 26 48.98             |
| 51 30                        | 5 41.374                           | 51 24 18.63             | 74 00                        | 3 05.856                           | 73 56 54.14             |
| 52 00                        | 5 39.957                           | 51 54 20.04             | 74 30                        | 3 00.640                           | 74 26 59.36             |
| 52 30                        | 5 38.435                           | 52 24 21.56             | 75 00                        | 2 55.368                           | 74 57 04.63             |
| 53 00                        | 5 36.811                           | 52 54 23.19             | 75 30                        | 2 50.042                           | 75 27 00.96             |
| 53 30                        | 5 35.083                           | 53 24 24.92             | 76 00                        | 2 44.665                           | 75 57 15.34             |
| 54 00                        | 5 33.254                           | 53 54 26.75             | 76 30                        | 2 39.237                           | 76 27 20.76             |
| 54 30                        | 5 31.322                           | 54 24 28.68             | 77 00                        | 2 33.761                           | 76 57 26.24             |
| 55 00                        | 5 29.290                           | 54 54 30.71             | 77 30                        | 2 28.238                           | 77 27 31.76             |
| 55 30                        | 5 27.158                           | 55 24 32.84             | 78 00                        | 2 22.669                           | 77 57 37.33             |
| 56 00                        | 5 24.925                           | 55 54 35.06             | 78 30                        | 2 17.056                           | 78 27 42.94             |
| 56 30                        | 5 22.593                           | 56 24 37.41             | 79 00                        | 2 11.402                           | 78 57 48.60             |
| 57 00                        | 5 20.163                           | 56 54 39.84             | 79 30                        | 2 05.707                           | 79 27 54.29             |
| 57 30                        | 5 17.635                           | 57 24 42.36             | 80 00                        | 1 59.974                           | 79 58 00.03             |
| 58 00                        | 5 15.010                           | 57 54 44.99             | 80 30                        | 1 54.204                           | 80 28 05.80             |
| 58 30                        | 5 12.289                           | 58 24 47.71             | 81 00                        | 1 48.399                           | 80 58 11.60             |
| 59 00                        | 5 09.473                           | 58 54 50.53             | 81 30                        | 1 42.561                           | 81 28 17.44             |
| 59 30                        | 5 06.562                           | 59 24 53.44             | 82 00                        | 1 36.692                           | 81 58 23.31             |
| 60 00                        | 5 03.557                           | 59 54 56.44             | 82 30                        | 1 30.792                           | 82 28 29.21             |
| 60 30                        | 5 00.460                           | 60 24 59.54             | 83 00                        | 1 24.866                           | 82 58 35.13             |
| 61 00                        | 4 57.271                           | 60 55 02.73             | 83 30                        | 1 18.913                           | 83 28 41.09             |
| 61 30                        | 4 53.991                           | 61 25 06.01             | 84 00                        | 1 12.936                           | 83 58 47.06             |
| 62 00                        | 4 50.622                           | 61 55 09.38             | 84 30                        | 1 06.937                           | 84 28 53.06             |
| 62 30                        | 4 47.163                           | 62 25 12.84             | 85 00                        | 1 00.917                           | 84 58 59.08             |
| 63 00                        | 4 43.617                           | 62 55 16.38             | 85 30                        | 0 54.878                           | 85 29 05.12             |
| 63 30                        | 4 39.984                           | 63 25 20.02             | 86 00                        | 0 48.823                           | 85 59 11.18             |
| 64 00                        | 4 36.266                           | 63 55 23.73             | 86 30                        | 0 42.753                           | 86 29 17.25             |
| 64 30                        | 4 32.463                           | 64 25 27.54             | 87 00                        | 0 36.670                           | 86 59 23.33             |
| 65 00                        | 4 28.577                           | 64 55 31.42             | 87 30                        | 0 30.575                           | 87 29 29.42             |
| 65 30                        | 4 24.609                           | 65 25 35.39             | 88 00                        | 0 24.472                           | 87 59 35.53             |
| 66 00                        | 4 20.560                           | 65 55 39.44             | 88 30                        | 0 18.360                           | 88 29 41.64             |
| 66 30                        | 4 16.432                           | 66 25 43.57             | 89 00                        | 0 12.243                           | 88 59 47.76             |
| 67 00                        | 4 12.225                           | 66 55 47.78             | 89 30                        | 0 06.123                           | 89 29 53.88             |
| 67 30                        | 4 07.941                           | 67 25 52.06             | 90 00                        | 0 00.000                           | 90 00 00.00             |

$$\theta-\psi = +350^{\circ}2202 \sin 2\theta - 0^{\circ}2973 \sin 4\theta + 0^{\circ}0003 \sin 6\theta.$$

$$\theta-\psi = [2.5443412] \sin 2\theta - [9.47323-10] \sin 4\theta + [6.527-10] \sin 6\theta.$$

LATITUDE TRANSFORMATION—Continued.

*Geocentric to parametric.*

| Geocentric latitude. | Parametric minus geocentric. | Parametric latitude. | Geocentric latitude. | Parametric minus geocentric. | Parametric latitude. |
|----------------------|------------------------------|----------------------|----------------------|------------------------------|----------------------|
| $\psi$               | $\theta - \psi$              | $\theta$             | $\psi$               | $\theta - \psi$              | $\theta$             |
| 0 00                 | 0 00.000                     | 0 00 00.00           | 22 30                | 4 07.941                     | 22 34 07.94          |
| 0 30                 | 0 06.123                     | 0 30 06.12           | 23 00                | 4 12.225                     | 23 04 12.22          |
| 1 00                 | 0 12.243                     | 1 00 12.24           | 23 30                | 4 16.432                     | 23 34 16.43          |
| 1 30                 | 0 18.360                     | 1 30 18.36           | 24 00                | 4 20.560                     | 24 04 20.56          |
| 2 00                 | 0 24.472                     | 2 00 24.47           | 24 30                | 4 24.699                     | 24 34 24.61          |
| 2 30                 | 0 30.575                     | 2 30 30.58           | 25 00                | 4 28.577                     | 25 04 28.58          |
| 3 00                 | 0 36.670                     | 3 00 36.67           | 25 30                | 4 32.463                     | 25 34 32.46          |
| 3 30                 | 0 42.753                     | 3 30 42.75           | 26 00                | 4 36.266                     | 26 04 36.27          |
| 4 00                 | 0 48.823                     | 4 00 48.82           | 26 30                | 4 39.984                     | 26 34 39.98          |
| 4 30                 | 0 54.878                     | 4 30 54.88           | 27 00                | 4 43.617                     | 27 04 43.62          |
| 5 00                 | 1 00.917                     | 5 01 00.92           | 27 30                | 4 47.163                     | 27 34 47.16          |
| 5 30                 | 1 06.937                     | 5 31 06.94           | 28 00                | 4 50.622                     | 28 04 50.62          |
| 6 00                 | 1 12.936                     | 6 01 12.94           | 28 30                | 4 53.991                     | 28 34 53.99          |
| 6 30                 | 1 18.913                     | 6 31 18.91           | 29 00                | 4 57.271                     | 29 04 57.27          |
| 7 00                 | 1 24.896                     | 7 01 24.87           | 29 30                | 5 00.460                     | 29 35 00.46          |
| 7 30                 | 1 30.792                     | 7 31 30.79           | 30 00                | 5 03.557                     | 30 05 03.56          |
| 8 00                 | 1 36.692                     | 8 01 36.69           | 30 30                | 5 06.562                     | 30 35 06.56          |
| 8 30                 | 1 42.561                     | 8 31 42.56           | 31 00                | 5 09.473                     | 31 05 09.47          |
| 9 00                 | 1 48.399                     | 9 01 48.40           | 31 30                | 5 12.289                     | 31 35 12.29          |
| 9 30                 | 1 54.204                     | 9 31 54.20           | 32 00                | 5 15.010                     | 32 05 15.01          |
| 10 00                | 1 59.974                     | 10 01 59.97          | 32 30                | 5 17.635                     | 32 35 17.64          |
| 10 30                | 2 05.707                     | 10 32 05.71          | 33 00                | 5 20.163                     | 33 05 20.16          |
| 11 00                | 2 11.402                     | 11 02 11.40          | 33 30                | 5 22.593                     | 33 35 22.59          |
| 11 30                | 2 17.056                     | 11 32 17.06          | 34 00                | 5 24.925                     | 34 05 24.92          |
| 12 00                | 2 22.669                     | 12 02 22.67          | 34 30                | 5 27.158                     | 34 35 27.16          |
| 12 30                | 2 28.238                     | 12 32 28.24          | 35 00                | 5 29.290                     | 35 05 29.29          |
| 13 00                | 2 33.761                     | 13 02 33.76          | 35 30                | 5 31.322                     | 35 35 31.32          |
| 13 30                | 2 39.237                     | 13 32 39.24          | 36 00                | 5 33.254                     | 36 05 33.25          |
| 14 00                | 2 44.665                     | 14 02 44.66          | 36 30                | 5 35.083                     | 36 35 35.08          |
| 14 30                | 2 50.042                     | 14 32 50.04          | 37 00                | 5 36.811                     | 37 05 36.81          |
| 15 00                | 2 55.368                     | 15 02 55.37          | 37 30                | 5 38.435                     | 37 35 38.44          |
| 15 30                | 3 00.640                     | 15 33 00.64          | 38 00                | 5 39.957                     | 38 05 39.96          |
| 16 00                | 3 05.866                     | 16 03 05.86          | 38 30                | 5 41.374                     | 38 35 41.37          |
| 16 30                | 3 11.016                     | 16 33 11.02          | 39 00                | 5 42.688                     | 39 05 42.69          |
| 17 00                | 3 16.117                     | 17 03 16.12          | 39 30                | 5 43.897                     | 39 35 43.90          |
| 17 30                | 3 21.158                     | 17 33 21.16          | 40 00                | 5 45.001                     | 40 05 45.00          |
| 18 00                | 3 26.137                     | 18 03 26.14          | 40 30                | 5 46.000                     | 40 35 46.00          |
| 18 30                | 3 31.054                     | 18 33 31.05          | 41 00                | 5 46.894                     | 41 05 46.89          |
| 19 00                | 3 35.906                     | 19 03 35.91          | 41 30                | 5 47.681                     | 41 35 47.68          |
| 19 30                | 3 40.692                     | 19 33 40.69          | 42 00                | 5 48.363                     | 42 05 48.36          |
| 20 00                | 3 45.410                     | 20 03 45.41          | 42 30                | 5 48.939                     | 42 35 48.94          |
| 20 30                | 3 50.060                     | 20 33 50.06          | 43 00                | 5 49.408                     | 43 05 49.41          |
| 21 00                | 3 54.639                     | 21 03 54.64          | 43 30                | 5 49.771                     | 43 35 49.77          |
| 21 30                | 3 59.146                     | 21 33 59.15          | 44 00                | 5 50.027                     | 44 05 50.03          |
| 22 00                | 4 03.581                     | 22 04 03.58          | 44 30                | 5 50.177                     | 44 35 50.18          |
| 22 30                | 4 07.941                     | 22 34 07.94          | 45 00                | 5 50.220                     | 45 05 50.22          |

$$\theta - \psi = +350''.2023 \sin 2\psi + 0''.2973 \sin 4\psi + 0''.0003 \sin 6\psi.$$

$$\theta - \psi = [2.5443412] \sin 2\psi + [9.47323 - 10] \sin 4\psi + [6.527 - 10] \sin 6\psi.$$

## LATITUDE TRANSFORMATION—Continued.

## Geocentric to parametric—Continued.

| Geocentric latitude. |    |    | Parametric minus geocentric. |    |     | Parametric latitude. |    |       | Geocentric latitude. |    |    | Parametric minus geocentric. |        |    | Parametric latitude. |       |    |
|----------------------|----|----|------------------------------|----|-----|----------------------|----|-------|----------------------|----|----|------------------------------|--------|----|----------------------|-------|----|
| $\psi$               |    |    | $\theta - \psi$              |    |     | $\theta$             |    |       | $\psi$               |    |    | $\theta - \psi$              |        |    | $\theta$             |       |    |
| °                    | '  | '' | °                            | '  | ''  | °                    | '  | ''    | °                    | '  | '' | °                            | '      | '' | °                    | '     | '' |
| 45                   | 00 |    | 5                            | 50 | 220 | 45                   | 05 | 50.22 | 67                   | 30 |    | 4                            | 07.346 | 67 | 34                   | 07.35 |    |
| 45                   | 30 |    | 5                            | 50 | 156 | 45                   | 35 | 50.16 | 68                   | 00 |    | 4                            | 02.987 | 68 | 04                   | 02.99 |    |
| 46                   | 00 |    | 5                            | 49 | 986 | 46                   | 05 | 49.96 | 68                   | 30 |    | 3                            | 58.563 | 68 | 33                   | 58.55 |    |
| 46                   | 30 |    | 5                            | 49 | 709 | 46                   | 35 | 49.71 | 69                   | 00 |    | 3                            | 54.045 | 69 | 03                   | 54.05 |    |
| 47                   | 00 |    | 5                            | 49 | 325 | 47                   | 05 | 49.33 | 69                   | 30 |    | 3                            | 49.471 | 69 | 33                   | 49.47 |    |
| 47                   | 30 |    | 5                            | 48 | 836 | 47                   | 35 | 48.84 | 70                   | 00 |    | 3                            | 44.825 | 70 | 03                   | 44.82 |    |
| 48                   | 00 |    | 5                            | 48 | 240 | 48                   | 05 | 48.24 | 70                   | 30 |    | 3                            | 40.110 | 70 | 33                   | 40.11 |    |
| 48                   | 30 |    | 5                            | 47 | 538 | 48                   | 35 | 47.54 | 71                   | 00 |    | 3                            | 35.329 | 71 | 03                   | 35.33 |    |
| 49                   | 00 |    | 5                            | 46 | 730 | 49                   | 05 | 46.73 | 71                   | 30 |    | 3                            | 30.482 | 71 | 33                   | 30.48 |    |
| 49                   | 30 |    | 5                            | 45 | 816 | 49                   | 35 | 45.82 | 72                   | 00 |    | 3                            | 25.572 | 72 | 03                   | 25.57 |    |
| 50                   | 00 |    | 5                            | 44 | 708 | 50                   | 05 | 44.80 | 72                   | 30 |    | 3                            | 20.599 | 72 | 33                   | 20.60 |    |
| 50                   | 30 |    | 5                            | 43 | 674 | 50                   | 35 | 43.67 | 73                   | 00 |    | 3                            | 15.565 | 73 | 03                   | 15.57 |    |
| 51                   | 00 |    | 5                            | 42 | 440 | 51                   | 05 | 42.45 | 73                   | 30 |    | 3                            | 10.472 | 73 | 33                   | 10.47 |    |
| 51                   | 30 |    | 5                            | 41 | 114 | 51                   | 35 | 41.11 | 74                   | 00 |    | 3                            | 05.321 | 74 | 03                   | 05.32 |    |
| 52                   | 00 |    | 5                            | 39 | 677 | 52                   | 05 | 39.69 | 74                   | 30 |    | 3                            | 00.114 | 74 | 33                   | 00.11 |    |
| 52                   | 30 |    | 5                            | 38 | 138 | 52                   | 35 | 38.14 | 75                   | 00 |    | 2                            | 54.853 | 75 | 02                   | 54.85 |    |
| 53                   | 00 |    | 5                            | 36 | 496 | 53                   | 05 | 36.50 | 75                   | 30 |    | 2                            | 49.538 | 75 | 32                   | 49.54 |    |
| 53                   | 30 |    | 5                            | 34 | 751 | 53                   | 35 | 34.75 | 76                   | 00 |    | 2                            | 44.172 | 76 | 02                   | 44.17 |    |
| 54                   | 00 |    | 5                            | 32 | 904 | 54                   | 05 | 32.90 | 76                   | 30 |    | 2                            | 38.756 | 76 | 32                   | 38.76 |    |
| 54                   | 30 |    | 5                            | 30 | 957 | 54                   | 35 | 30.96 | 77                   | 00 |    | 2                            | 33.292 | 77 | 02                   | 33.29 |    |
| 55                   | 00 |    | 5                            | 28 | 908 | 55                   | 05 | 28.01 | 77                   | 30 |    | 2                            | 27.782 | 77 | 32                   | 27.78 |    |
| 55                   | 30 |    | 5                            | 26 | 760 | 55                   | 35 | 26.76 | 78                   | 00 |    | 2                            | 22.227 | 78 | 02                   | 22.23 |    |
| 56                   | 00 |    | 5                            | 24 | 512 | 56                   | 05 | 24.51 | 78                   | 30 |    | 2                            | 16.628 | 78 | 32                   | 16.63 |    |
| 56                   | 30 |    | 5                            | 22 | 165 | 56                   | 35 | 22.18 | 79                   | 00 |    | 2                            | 10.989 | 79 | 02                   | 10.99 |    |
| 57                   | 00 |    | 5                            | 19 | 721 | 57                   | 05 | 19.72 | 79                   | 30 |    | 2                            | 05.309 | 79 | 32                   | 05.31 |    |
| 57                   | 30 |    | 5                            | 17 | 180 | 57                   | 35 | 17.18 | 80                   | 00 |    | 1                            | 59.592 | 80 | 01                   | 59.59 |    |
| 58                   | 00 |    | 5                            | 14 | 541 | 58                   | 05 | 14.54 | 80                   | 30 |    | 1                            | 53.838 | 80 | 31                   | 53.84 |    |
| 58                   | 30 |    | 5                            | 11 | 898 | 58                   | 35 | 11.81 | 81                   | 00 |    | 1                            | 48.050 | 81 | 01                   | 48.05 |    |
| 59                   | 00 |    | 5                            | 08 | 980 | 59                   | 05 | 08.98 | 81                   | 30 |    | 1                            | 42.223 | 81 | 31                   | 42.23 |    |
| 59                   | 30 |    | 5                            | 06 | 057 | 59                   | 35 | 06.06 | 82                   | 00 |    | 1                            | 36.377 | 82 | 01                   | 36.38 |    |
| 60                   | 00 |    | 5                            | 03 | 042 | 60                   | 05 | 03.04 | 82                   | 30 |    | 1                            | 30.495 | 82 | 31                   | 30.50 |    |
| 60                   | 30 |    | 4                            | 59 | 935 | 60                   | 34 | 59.94 | 83                   | 00 |    | 1                            | 24.587 | 83 | 01                   | 24.59 |    |
| 61                   | 00 |    | 4                            | 56 | 736 | 61                   | 04 | 56.74 | 83                   | 30 |    | 1                            | 18.652 | 83 | 31                   | 18.65 |    |
| 61                   | 30 |    | 4                            | 53 | 448 | 61                   | 34 | 53.45 | 84                   | 00 |    | 1                            | 12.694 | 84 | 01                   | 12.69 |    |
| 62                   | 00 |    | 4                            | 50 | 070 | 62                   | 04 | 50.07 | 84                   | 30 |    | 1                            | 06.714 | 84 | 31                   | 06.71 |    |
| 62                   | 30 |    | 4                            | 46 | 604 | 62                   | 34 | 46.60 | 85                   | 00 |    | 1                            | 00.714 | 85 | 01                   | 00.71 |    |
| 63                   | 00 |    | 4                            | 43 | 052 | 63                   | 04 | 43.05 | 85                   | 30 |    | 0                            | 54.695 | 85 | 30                   | 54.69 |    |
| 63                   | 30 |    | 4                            | 39 | 413 | 63                   | 34 | 39.41 | 86                   | 00 |    | 0                            | 48.659 | 86 | 00                   | 48.66 |    |
| 64                   | 00 |    | 4                            | 35 | 689 | 64                   | 04 | 35.69 | 86                   | 30 |    | 0                            | 42.609 | 86 | 30                   | 42.61 |    |
| 64                   | 30 |    | 4                            | 31 | 882 | 64                   | 34 | 31.88 | 87                   | 00 |    | 0                            | 36.546 | 87 | 00                   | 36.55 |    |
| 65                   | 00 |    | 4                            | 27 | 982 | 65                   | 04 | 27.99 | 87                   | 30 |    | 0                            | 80.472 | 87 | 30                   | 80.47 |    |
| 65                   | 30 |    | 4                            | 24 | 020 | 65                   | 34 | 24.02 | 88                   | 00 |    | 0                            | 24.389 | 88 | 00                   | 24.39 |    |
| 66                   | 00 |    | 4                            | 19 | 969 | 66                   | 04 | 19.97 | 88                   | 30 |    | 0                            | 18.298 | 88 | 30                   | 18.30 |    |
| 66                   | 30 |    | 4                            | 15 | 838 | 66                   | 34 | 15.84 | 89                   | 00 |    | 0                            | 12.202 | 89 | 00                   | 12.20 |    |
| 67                   | 00 |    | 4                            | 11 | 630 | 67                   | 04 | 11.63 | 89                   | 30 |    | 0                            | 06.102 | 89 | 30                   | 06.10 |    |
| 67                   | 30 |    | 4                            | 07 | 346 | 67                   | 34 | 07.35 | 90                   | 00 |    | 0                            | 00.000 | 90 | 00                   | 00.00 |    |

$$\theta - \psi = +350''.2022 \sin 2\psi + 0''.2973 \sin 4\psi + 0''.0003 \sin 6\psi.$$

$$\theta - \psi = [2.5443412] \sin 2\psi + [9.47323-10] \sin 4\psi + [6.527-10] \sin 6\psi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geodetic to isometric.*

| Geodetic latitude. | Geodetic colatitude | Geodetic minus isometric. | Isometric colatitude. | $\frac{z}{2}$ |
|--------------------|---------------------|---------------------------|-----------------------|---------------|
| $\varphi$          | $p$                 | $\varphi - \chi$          | $z$                   |               |
| ° ' "              | ° ' "               | ' "                       | ° ' "                 | ° ' "         |
| 0 00               | 90 00               | 0 00.000                  | 90 00 00.00           | 45 00 00.00   |
| 0 30               | 89 30               | 0 12.183                  | 89 30 12.18           | 44 45 06.09   |
| 1 00               | 89 00               | 0 24.362                  | 89 00 24.36           | 44 30 12.18   |
| 1 30               | 88 30               | 0 36.534                  | 88 30 36.53           | 44 15 18.27   |
| 2 00               | 88 00               | 0 48.695                  | 88 00 48.70           | 44 00 24.35   |
| 2 30               | 87 30               | 1 00.841                  | 87 31 00.84           | 43 45 30.42   |
| 3 00               | 87 00               | 1 12.969                  | 87 01 12.97           | 43 30 36.48   |
| 3 30               | 86 30               | 1 25.075                  | 86 31 25.08           | 43 15 42.54   |
| 4 00               | 86 00               | 1 37.155                  | 86 01 37.16           | 43 00 48.58   |
| 4 30               | 85 30               | 1 49.206                  | 85 31 49.21           | 42 45 54.60   |
| 5 00               | 85 00               | 2 01.223                  | 85 02 01.22           | 42 31 00.61   |
| 5 30               | 84 30               | 2 13.204                  | 84 32 13.20           | 42 16 06.60   |
| 6 00               | 84 00               | 2 25.145                  | 84 02 25.14           | 42 01 12.57   |
| 6 30               | 83 30               | 2 37.042                  | 83 32 37.04           | 41 46 18.52   |
| 7 00               | 83 00               | 2 48.892                  | 83 02 48.89           | 41 31 24.45   |
| 7 30               | 82 30               | 3 00.691                  | 82 33 00.69           | 41 16 30.35   |
| 8 00               | 82 00               | 3 12.435                  | 82 03 12.44           | 41 01 36.22   |
| 8 30               | 81 30               | 3 24.120                  | 81 33 24.12           | 40 46 42.06   |
| 9 00               | 81 00               | 3 35.746                  | 81 03 35.75           | 40 31 47.87   |
| 9 30               | 80 30               | 3 47.304                  | 80 33 47.30           | 40 16 53.65   |
| 10 00              | 80 00               | 3 58.794                  | 80 03 58.79           | 40 01 59.40   |
| 10 30              | 79 30               | 4 10.212                  | 79 34 10.21           | 39 47 05.11   |
| 11 00              | 79 00               | 4 21.554                  | 79 04 21.55           | 39 32 10.78   |
| 11 30              | 78 30               | 4 32.818                  | 78 34 32.82           | 39 17 16.41   |
| 12 00              | 78 00               | 4 43.999                  | 78 04 44.00           | 39 02 22.00   |
| 12 30              | 77 30               | 4 55.094                  | 77 34 55.09           | 38 47 27.55   |
| 13 00              | 77 00               | 5 06.100                  | 77 05 06.10           | 38 32 33.03   |
| 13 30              | 76 30               | 5 17.014                  | 76 35 17.01           | 38 17 38.51   |
| 14 00              | 76 00               | 5 27.831                  | 76 05 27.83           | 38 02 43.92   |
| 14 30              | 75 30               | 5 38.550                  | 75 35 38.55           | 37 47 49.28   |
| 15 00              | 75 00               | 5 49.166                  | 75 05 49.17           | 37 32 54.58   |
| 15 30              | 74 30               | 5 59.676                  | 74 35 59.68           | 37 17 59.84   |
| 16 00              | 74 00               | 6 10.075                  | 74 06 10.08           | 37 03 05.04   |
| 16 30              | 73 30               | 6 20.368                  | 73 36 20.37           | 36 48 10.18   |
| 17 00              | 73 00               | 6 30.543                  | 73 06 30.54           | 36 33 15.27   |
| 17 30              | 72 30               | 6 40.599                  | 72 36 40.60           | 36 18 20.30   |
| 18 00              | 72 00               | 6 50.535                  | 72 06 50.54           | 36 03 25.27   |
| 18 30              | 71 30               | 7 00.346                  | 71 37 00.35           | 35 48 30.17   |
| 19 00              | 71 00               | 7 10.030                  | 71 07 10.03           | 35 33 35.02   |
| 19 30              | 70 30               | 7 19.584                  | 70 37 19.58           | 35 18 39.79   |
| 20 00              | 70 00               | 7 29.005                  | 70 07 29.00           | 35 03 44.50   |
| 20 30              | 69 30               | 7 38.290                  | 69 37 38.29           | 34 48 49.15   |
| 21 00              | 69 00               | 7 47.437                  | 69 07 47.44           | 34 33 53.72   |
| 21 30              | 68 30               | 7 56.442                  | 68 37 56.44           | 34 18 58.22   |
| 22 00              | 68 00               | 8 05.302                  | 68 08 05.30           | 34 04 02.65   |
| 22 30              | 67 30               | 8 14.016                  | 67 38 14.02           | 33 49 07.01   |

$$\varphi - \chi = +700^{\circ}0427 \sin 2\varphi - 0^{\circ}9300 \sin 4\varphi + 0^{\circ}0017 \sin 6\varphi,$$

$$\varphi - \chi = [2.34512455] \sin 2\varphi - [9.99563 - 10] \sin 4\varphi + [7.238 - 10] \sin 6\varphi.$$



## LATITUDE TRANSFORMATION—Continued.

Geodetic to isometric—Continued.

| Geodetic latitude. | Geodetic colatitude | Geodetic minus isometric. | Isometric colatitude. | $\frac{z}{2}$ |
|--------------------|---------------------|---------------------------|-----------------------|---------------|
| $\varphi$          | $p$                 | $\varphi-x$               | $z$                   |               |
| ° ' "              | ° ' "               | ' "                       | ° ' "                 | ° ' "         |
| 22 30              | 67 30               | 8 14.016                  | 67 38 14.02           | 33 49 07.01   |
| 23 00              | 67 00               | 8 22.580                  | 67 08 22.58           | 33 34 11.29   |
| 23 30              | 66 30               | 8 30.992                  | 66 38 30.99           | 33 19 15.50   |
| 24 00              | 66 00               | 8 39.250                  | 66 08 39.25           | 33 04 19.62   |
| 24 30              | 65 30               | 8 47.349                  | 65 38 47.35           | 32 49 23.67   |
| 25 00              | 65 00               | 8 55.290                  | 65 08 55.29           | 32 34 27.64   |
| 25 30              | 64 30               | 9 03.068                  | 64 39 03.07           | 32 19 31.53   |
| 26 00              | 64 00               | 9 10.681                  | 64 09 10.68           | 32 04 35.34   |
| 26 30              | 63 30               | 9 18.128                  | 63 39 18.13           | 31 49 39.06   |
| 27 00              | 63 00               | 9 25.405                  | 63 09 25.41           | 31 34 42.70   |
| 27 30              | 62 30               | 9 32.512                  | 62 39 32.51           | 31 19 46.26   |
| 28 00              | 62 00               | 9 39.444                  | 62 09 39.44           | 31 04 49.72   |
| 28 30              | 61 30               | 9 46.201                  | 61 39 46.20           | 30 49 53.10   |
| 29 00              | 61 00               | 9 52.780                  | 61 09 52.78           | 30 34 56.39   |
| 29 30              | 60 30               | 9 59.179                  | 60 39 59.18           | 30 19 59.59   |
| 30 00              | 60 00               | 10 05.397                 | 60 10 05.40           | 30 05 02.70   |
| 30 30              | 59 30               | 10 11.431                 | 59 40 11.43           | 29 50 05.72   |
| 31 00              | 59 00               | 10 17.280                 | 59 10 17.28           | 29 35 08.64   |
| 31 30              | 58 30               | 10 22.941                 | 58 40 22.94           | 29 20 11.47   |
| 32 00              | 58 00               | 10 28.414                 | 58 10 28.41           | 29 05 14.21   |
| 32 30              | 57 30               | 10 33.695                 | 57 40 33.70           | 28 50 16.85   |
| 33 00              | 57 00               | 10 38.785                 | 57 10 38.78           | 28 35 19.39   |
| 33 30              | 56 30               | 10 43.680                 | 56 40 43.68           | 28 20 21.84   |
| 34 00              | 56 00               | 10 48.380                 | 56 10 48.38           | 28 05 24.19   |
| 34 30              | 55 30               | 10 52.883                 | 55 40 52.88           | 27 50 26.44   |
| 35 00              | 55 00               | 10 57.188                 | 55 10 57.19           | 27 35 28.59   |
| 35 30              | 54 30               | 11 01.293                 | 54 41 01.29           | 27 20 30.65   |
| 36 00              | 54 00               | 11 05.198                 | 54 11 05.20           | 27 05 32.60   |
| 36 30              | 53 30               | 11 08.900                 | 53 41 08.90           | 26 50 34.45   |
| 37 00              | 53 00               | 11 12.398                 | 53 11 12.40           | 26 35 36.20   |
| 37 30              | 52 30               | 11 15.603                 | 52 41 15.69           | 26 20 37.85   |
| 38 00              | 52 00               | 11 18.782                 | 52 11 18.78           | 26 05 39.39   |
| 38 30              | 51 30               | 11 21.665                 | 51 41 21.66           | 25 50 40.83   |
| 39 00              | 51 00               | 11 24.341                 | 51 11 24.34           | 25 35 42.17   |
| 39 30              | 50 30               | 11 26.809                 | 50 41 26.81           | 25 20 43.40   |
| 40 00              | 50 00               | 11 29.067                 | 50 11 29.07           | 25 05 44.53   |
| 40 30              | 49 30               | 11 31.117                 | 49 41 31.12           | 24 50 45.56   |
| 41 00              | 49 00               | 11 32.955                 | 49 11 32.96           | 24 35 46.48   |
| 41 30              | 48 30               | 11 34.584                 | 48 41 34.58           | 24 20 47.29   |
| 42 00              | 48 00               | 11 36.000                 | 48 11 36.00           | 24 05 48.00   |
| 42 30              | 47 30               | 11 37.205                 | 47 41 37.20           | 23 50 48.60   |
| 43 00              | 47 00               | 11 38.198                 | 47 11 38.20           | 23 35 49.10   |
| 43 30              | 46 30               | 11 38.978                 | 46 41 38.98           | 23 20 49.49   |
| 44 00              | 46 00               | 11 39.546                 | 46 11 39.55           | 23 05 49.77   |
| 44 30              | 45 30               | 11 39.900                 | 45 41 39.90           | 22 50 49.95   |
| 45 00              | 45 00               | 11 40.041                 | 45 11 40.04           | 22 35 50.02   |

$$\varphi-x = +700^{\circ}0427 \sin 2\varphi - 0^{\circ}9900 \sin 4\varphi + 0^{\circ}0017 \sin 6\varphi.$$

$$\varphi-x = [2.84512455] \sin 2\varphi - [9.99563-10] \sin 4\varphi + [7.238-10] \sin 6\varphi.$$

LATITUDE TRANSFORMATION—Continued.

Geodetic to isometric—Continued.

| Geodetic latitude. | Geodetic colatitude | Geodetic minus isometric. | Isometric colatitude. | $z$         |
|--------------------|---------------------|---------------------------|-----------------------|-------------|
| $\varphi$          | $p$                 | $\varphi - x$             | $z$                   | $z$         |
| ° /                | ° /                 | ' "                       | ° / "                 | ° / "       |
| 45 00              | 45 00               | 11 40.041                 | 45 11 40.04           | 22 35 50.02 |
| 45 30              | 44 30               | 11 39.989                 | 44 41 39.97           | 22 20 49.98 |
| 46 00              | 44 00               | 11 39.684                 | 44 11 39.68           | 22 05 49.84 |
| 46 30              | 43 30               | 11 39.185                 | 43 41 39.18           | 21 50 49.59 |
| 47 00              | 43 00               | 11 38.474                 | 43 11 38.47           | 21 35 49.24 |
| 47 30              | 42 30               | 11 37.549                 | 42 41 37.55           | 21 20 48.77 |
| 48 00              | 42 00               | 11 36.412                 | 42 11 36.41           | 21 05 48.21 |
| 48 30              | 41 30               | 11 35.063                 | 41 41 35.06           | 20 50 47.53 |
| 49 00              | 41 00               | 11 33.501                 | 41 11 33.50           | 20 35 46.75 |
| 49 30              | 40 30               | 11 31.723                 | 40 41 31.73           | 20 20 45.86 |
| 50 00              | 40 00               | 11 29.745                 | 40 11 29.74           | 20 05 44.87 |
| 50 30              | 39 30               | 11 27.550                 | 39 41 27.55           | 19 50 43.78 |
| 51 00              | 39 00               | 11 25.146                 | 39 11 25.15           | 19 35 42.57 |
| 51 30              | 38 30               | 11 22.533                 | 38 41 22.53           | 19 20 41.27 |
| 52 00              | 38 00               | 11 19.712                 | 38 11 19.71           | 19 05 39.86 |
| 52 30              | 37 30               | 11 16.683                 | 37 41 16.68           | 18 50 38.34 |
| 53 00              | 37 00               | 11 13.448                 | 37 11 13.45           | 18 35 36.72 |
| 53 30              | 36 30               | 11 10.007                 | 36 41 10.01           | 18 20 35.00 |
| 54 00              | 36 00               | 11 06.360                 | 36 11 06.36           | 18 05 33.18 |
| 54 30              | 35 30               | 11 02.512                 | 35 41 02.51           | 17 50 31.26 |
| 55 00              | 35 00               | 10 58.461                 | 35 10 58.46           | 17 35 29.23 |
| 55 30              | 34 30               | 10 54.208                 | 34 40 54.21           | 17 20 27.10 |
| 56 00              | 34 00               | 10 49.755                 | 34 10 49.76           | 17 05 24.88 |
| 56 30              | 33 30               | 10 45.104                 | 33 40 45.10           | 16 50 22.55 |
| 57 00              | 33 00               | 10 40.256                 | 33 10 40.26           | 16 35 20.13 |
| 57 30              | 32 30               | 10 35.212                 | 32 40 35.21           | 16 20 17.61 |
| 58 00              | 32 00               | 10 29.974                 | 32 10 29.97           | 16 05 14.99 |
| 58 30              | 31 30               | 10 24.548                 | 31 40 24.54           | 15 50 12.27 |
| 59 00              | 31 00               | 10 18.922                 | 31 10 18.92           | 15 35 09.46 |
| 59 30              | 30 30               | 10 13.111                 | 30 40 13.11           | 15 20 06.56 |
| 60 00              | 30 00               | 10 07.112                 | 30 10 07.11           | 15 05 03.56 |
| 60 30              | 29 30               | 10 00.928                 | 29 40 00.93           | 14 50 00.46 |
| 61 00              | 29 00               | 9 54.560                  | 29 09 54.56           | 14 34 57.28 |
| 61 30              | 28 30               | 9 48.010                  | 28 39 48.01           | 14 19 54.00 |
| 62 00              | 28 00               | 9 41.280                  | 28 09 41.28           | 14 04 50.64 |
| 62 30              | 27 30               | 9 34.372                  | 27 39 34.37           | 13 49 47.19 |
| 63 00              | 27 00               | 9 27.288                  | 27 09 27.29           | 13 34 43.64 |
| 63 30              | 26 30               | 9 20.031                  | 26 39 20.03           | 13 19 40.02 |
| 64 00              | 26 00               | 9 12.602                  | 26 09 12.60           | 13 04 36.30 |
| 64 30              | 25 30               | 9 05.005                  | 25 39 05.00           | 12 49 32.50 |
| 65 00              | 25 00               | 8 57.240                  | 25 08 57.24           | 12 34 28.62 |
| 65 30              | 24 30               | 8 49.310                  | 24 38 49.31           | 12 19 24.66 |
| 66 00              | 24 00               | 8 41.219                  | 24 08 41.22           | 12 04 20.61 |
| 66 30              | 23 30               | 8 32.968                  | 23 38 32.97           | 11 49 16.48 |
| 67 00              | 23 00               | 8 24.559                  | 23 08 24.56           | 11 34 12.28 |
| 67 30              | 22 30               | 8 15.996                  | 22 38 16.00           | 11 19 08.00 |

$$\varphi - x = +700^{\circ}0427 \sin 2\varphi - 0^{\circ}9900 \sin 4\varphi + 0^{\circ}0017 \sin 6\varphi.$$

$$\varphi - x = [2.84512455] \sin 2\varphi - [9.99563 - 10] \sin 4\varphi + [7.238 - 10] \sin 6\varphi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geodetic to isometric—Continued.*

| Geodetic latitude. | Geodetic colatitude | Geodetic minus isometric. | Isometric colatitude. | $\frac{z}{2}$ |
|--------------------|---------------------|---------------------------|-----------------------|---------------|
| $\phi$             | $p$                 | $\phi - x$                | $z$                   |               |
| 67 30              | 22 30               | 8 15.996                  | 22 38 16.00           | 11 19 08.00   |
| 68 00              | 22 00               | 8 07.281                  | 22 08 07.28           | 11 04 03.64   |
| 68 30              | 21 30               | 7 58.417                  | 21 37 58.42           | 10 45 59.21   |
| 69 00              | 21 00               | 7 49.406                  | 21 07 49.41           | 10 33 54.70   |
| 69 30              | 20 30               | 7 40.251                  | 20 37 40.25           | 10 18 50.13   |
| 70 00              | 20 00               | 7 30.955                  | 20 07 30.96           | 10 03 45.48   |
| 70 30              | 19 30               | 7 21.521                  | 19 37 21.52           | 9 48 40.76    |
| 71 00              | 19 00               | 7 11.952                  | 19 07 11.95           | 9 33 35.98    |
| 71 30              | 18 30               | 7 02.249                  | 18 37 02.25           | 9 18 31.12    |
| 72 00              | 18 00               | 6 52.418                  | 18 06 52.42           | 9 03 26.21    |
| 72 30              | 17 30               | 6 42.460                  | 17 36 42.46           | 8 48 21.23    |
| 73 00              | 17 00               | 6 32.378                  | 17 06 32.38           | 8 33 16.19    |
| 73 30              | 16 30               | 6 22.177                  | 16 36 22.18           | 8 18 11.09    |
| 74 00              | 16 00               | 6 11.858                  | 16 06 11.86           | 8 03 05.93    |
| 74 30              | 15 30               | 6 01.424                  | 15 36 01.42           | 7 48 00.71    |
| 75 00              | 15 00               | 5 50.890                  | 15 05 50.88           | 7 32 55.44    |
| 75 30              | 14 30               | 5 40.229                  | 14 35 40.23           | 7 17 50.11    |
| 76 00              | 14 00               | 5 29.472                  | 14 05 29.47           | 7 02 44.74    |
| 76 30              | 13 30               | 5 18.615                  | 13 35 18.62           | 6 47 39.31    |
| 77 00              | 13 00               | 5 07.660                  | 13 05 07.66           | 6 32 33.83    |
| 77 30              | 12 30               | 4 56.611                  | 12 34 56.61           | 6 17 28.31    |
| 78 00              | 12 00               | 4 45.470                  | 12 04 45.47           | 6 02 22.74    |
| 78 30              | 11 30               | 4 34.242                  | 11 34 34.24           | 5 47 17.12    |
| 79 00              | 11 00               | 4 22.930                  | 11 04 22.93           | 5 32 11.46    |
| 79 30              | 10 30               | 4 11.537                  | 10 34 11.54           | 5 17 05.77    |
| 80 00              | 10 00               | 4 00.067                  | 10 04 00.07           | 5 02 00.03    |
| 80 30              | 9 30                | 3 48.522                  | 9 33 48.52            | 4 46 54.26    |
| 81 00              | 9 00                | 3 36.907                  | 9 03 36.91            | 4 31 48.45    |
| 81 30              | 8 30                | 3 25.228                  | 8 33 25.23            | 4 16 42.61    |
| 82 00              | 8 00                | 3 13.484                  | 8 03 13.48            | 4 01 36.74    |
| 82 30              | 7 30                | 3 01.681                  | 7 33 01.68            | 3 46 30.84    |
| 83 00              | 7 00                | 2 49.822                  | 7 02 49.82            | 3 31 24.91    |
| 83 30              | 6 30                | 2 37.910                  | 6 32 37.91            | 3 16 18.96    |
| 84 00              | 6 00                | 2 25.951                  | 6 02 25.95            | 3 01 12.98    |
| 84 30              | 5 30                | 2 13.945                  | 5 32 13.94            | 2 46 06.97    |
| 85 00              | 5 00                | 2 01.900                  | 5 02 01.90            | 2 31 00.95    |
| 85 30              | 4 30                | 1 49.818                  | 4 31 49.82            | 2 15 54.91    |
| 86 00              | 4 00                | 1 37.701                  | 4 01 37.70            | 2 00 48.85    |
| 86 30              | 3 30                | 1 25.554                  | 3 31 25.55            | 1 45 42.78    |
| 87 00              | 3 00                | 1 13.381                  | 3 01 13.38            | 1 30 36.69    |
| 87 30              | 2 30                | 1 01.184                  | 2 31 01.18            | 1 15 30.59    |
| 88 00              | 2 00                | 0 48.971                  | 2 00 48.97            | 1 00 24.49    |
| 88 30              | 1 30                | 0 36.741                  | 1 30 36.74            | 0 45 18.37    |
| 89 00              | 1 00                | 0 24.500                  | 1 00 24.50            | 0 30 12.25    |
| 89 30              | 0 30                | 0 12.252                  | 0 30 12.25            | 0 15 06.13    |
| 90 00              | 0 00                | 0 00.000                  | 0 00 00.00            | 0 00 00.00    |

$$\phi - x = +700^{\circ}0427 \sin 2\phi - 0^{\circ}9900 \sin 4\phi + 0^{\circ}0017 \sin 6\phi.$$

$$\phi - x = [2.84512455] \sin 2\phi - [9.99563 - 10] \sin 4\phi + [7.238 - 10] \sin 6\phi.$$

LATITUDE TRANSFORMATION—Continued.

*Isometric to geodetic.*

| Isometric latitude. | Geodetic minus isometric. | Geodetic latitude. | Isometric latitude. | Geodetic minus isometric. | Geodetic latitude. |
|---------------------|---------------------------|--------------------|---------------------|---------------------------|--------------------|
| $x$                 | $\varphi-x$               | $\varphi$          | $x$                 | $\varphi-x$               | $\varphi$          |
| ° ' "               | ' "                       | ° ' "              | ° ' "               | ' "                       | ° ' "              |
| 0 00                | 0 00.000                  | 0 00 00.00         | 22 30               | 8 16.393                  | 22 38 16.39        |
| 0 30                | 0 12.266                  | 0 30 12.27         | 23 00               | 8 24.956                  | 23 08 24.96        |
| 1 00                | 0 24.528                  | 1 00 24.53         | 23 30               | 8 33.363                  | 23 38 33.36        |
| 1 30                | 0 36.783                  | 1 30 36.78         | 24 00               | 8 41.613                  | 24 08 41.61        |
| 2 00                | 0 49.026                  | 2 00 49.03         | 24 30               | 8 49.703                  | 24 38 49.70        |
| 2 30                | 1 01.254                  | 2 31 01.25         | 25 00               | 8 57.630                  | 25 08 57.63        |
| 3 00                | 1 13.463                  | 3 01 13.46         | 25 30               | 9 05.392                  | 25 39 05.39        |
| 3 30                | 1 25.650                  | 3 31 25.65         | 26 00               | 9 12.987                  | 26 09 12.99        |
| 4 00                | 1 37.810                  | 4 01 37.81         | 26 30               | 9 20.412                  | 26 39 20.41        |
| 4 30                | 1 49.941                  | 4 31 49.94         | 27 00               | 9 27.665                  | 27 09 27.66        |
| 5 00                | 2 02.037                  | 5 02 02.04         | 27 30               | 9 34.744                  | 27 39 34.74        |
| 5 30                | 2 14.097                  | 5 32 14.10         | 28 00               | 9 41.647                  | 28 09 41.65        |
| 6 00                | 2 26.113                  | 6 02 26.11         | 28 30               | 9 48.371                  | 28 39 48.37        |
| 6 30                | 2 38.085                  | 6 32 38.08         | 29 00               | 9 54.915                  | 29 09 54.92        |
| 7 00                | 2 50.009                  | 7 02 50.01         | 29 30               | 10 01.277                 | 29 40 01.28        |
| 7 30                | 3 01.880                  | 7 33 01.88         | 30 00               | 10 07.454                 | 30 10 07.45        |
| 8 00                | 3 13.695                  | 8 03 13.70         | 30 30               | 10 13.440                 | 30 40 13.45        |
| 8 30                | 3 25.450                  | 8 33 25.45         | 31 00               | 10 19.249                 | 31 10 19.25        |
| 9 00                | 3 37.142                  | 9 03 37.14         | 31 30               | 10 24.863                 | 31 40 24.86        |
| 9 30                | 3 48.768                  | 9 33 48.77         | 32 00               | 10 30.285                 | 32 10 30.28        |
| 10 00               | 4 00.322                  | 10 04 00.32        | 32 30               | 10 35.514                 | 32 40 35.51        |
| 10 30               | 4 11.803                  | 10 34 11.80        | 33 00               | 10 40.549                 | 33 10 40.55        |
| 11 00               | 4 23.206                  | 11 04 23.21        | 33 30               | 10 45.388                 | 33 40 45.39        |
| 11 30               | 4 34.529                  | 11 34 34.53        | 34 00               | 10 50.029                 | 34 10 50.03        |
| 12 00               | 4 45.766                  | 12 04 45.77        | 34 30               | 10 54.471                 | 34 40 54.47        |
| 12 30               | 4 56.916                  | 12 34 56.92        | 35 00               | 10 58.713                 | 35 10 58.71        |
| 13 00               | 5 07.974                  | 13 05 07.97        | 35 30               | 11 02.754                 | 35 41 02.75        |
| 13 30               | 5 18.937                  | 13 35 18.94        | 36 00               | 11 06.592                 | 36 11 06.59        |
| 14 00               | 5 29.802                  | 14 05 29.80        | 36 30               | 11 10.226                 | 36 41 10.23        |
| 14 30               | 5 40.566                  | 14 35 40.57        | 37 00               | 11 13.656                 | 37 11 13.66        |
| 15 00               | 5 51.225                  | 15 05 51.22        | 37 30               | 11 16.879                 | 37 41 16.88        |
| 15 30               | 6 01.776                  | 15 36 01.78        | 38 00               | 11 19.896                 | 38 11 19.90        |
| 16 00               | 6 12.215                  | 16 06 12.22        | 38 30               | 11 22.705                 | 38 41 22.70        |
| 16 30               | 6 22.540                  | 16 36 22.54        | 39 00               | 11 25.305                 | 39 11 25.30        |
| 17 00               | 6 32.747                  | 17 06 32.75        | 39 30               | 11 27.696                 | 39 41 27.70        |
| 17 30               | 6 42.834                  | 17 36 42.83        | 40 00               | 11 29.878                 | 40 11 29.88        |
| 18 00               | 6 52.796                  | 18 06 52.80        | 40 30               | 11 31.848                 | 40 41 31.85        |
| 18 30               | 7 02.631                  | 18 37 02.63        | 41 00               | 11 33.607                 | 41 11 33.61        |
| 19 00               | 7 12.337                  | 19 07 12.34        | 41 30               | 11 35.156                 | 41 41 35.16        |
| 19 30               | 7 21.910                  | 19 37 21.91        | 42 00               | 11 36.492                 | 42 11 36.49        |
| 20 00               | 7 31.346                  | 20 07 31.35        | 42 30               | 11 37.615                 | 42 41 37.62        |
| 20 30               | 7 40.644                  | 20 37 40.64        | 43 00               | 11 38.523                 | 43 11 38.53        |
| 21 00               | 7 49.801                  | 21 07 49.80        | 43 30               | 11 39.224                 | 43 41 39.22        |
| 21 30               | 7 58.813                  | 21 37 58.81        | 44 00               | 11 39.709                 | 44 11 39.71        |
| 22 00               | 8 07.678                  | 22 08 07.68        | 44 30               | 11 39.980                 | 44 41 39.98        |
| 22 30               | 8 16.393                  | 22 38 16.39        | 45 00               | 11 40.038                 | 45 11 40.04        |

$$\varphi-x = +700^{\circ}0420 \sin 2x + 1^{\circ}3859 \sin 4x + 0^{\circ}0037 \sin 6x.$$

$$\varphi-x = [2.84512413] \sin 2x + [0.141723] \sin 4x + [7.572-10] \sin 6x.$$

## LATITUDE TRANSFORMATION—Continued.

*Isonnetric to geodetic—Continued.*

| Isometric latitude. |    | Geodetic minus isometric. |        | Geodetic latitude. |    | Isometric latitude. |    | Geodetic minus isometric. |   | Geodetic latitude. |    |    |       |
|---------------------|----|---------------------------|--------|--------------------|----|---------------------|----|---------------------------|---|--------------------|----|----|-------|
| x                   |    | φ-x                       |        | φ                  |    | x                   |    | φ-x                       |   | φ                  |    |    |       |
| °                   | '  | °                         | '      | °                  | '  | °                   | '  | °                         | ' | °                  | '  |    |       |
| 45                  | 00 | 11                        | 40.038 | 45                 | 11 | 40.04               | 67 | 30                        | 8 | 13.621             | 67 | 38 | 13.62 |
| 45                  | 30 | 11                        | 39.883 | 45                 | 41 | 39.88               | 68 | 00                        | 8 | 04.908             | 68 | 08 | 04.91 |
| 46                  | 00 | 11                        | 39.515 | 46                 | 11 | 39.52               | 68 | 30                        | 7 | 56.048             | 68 | 37 | 56.05 |
| 46                  | 30 | 11                        | 38.934 | 46                 | 41 | 38.93               | 69 | 00                        | 7 | 47.044             | 69 | 07 | 47.04 |
| 47                  | 00 | 11                        | 38.140 | 47                 | 11 | 38.14               | 69 | 30                        | 7 | 37.900             | 69 | 37 | 37.90 |
| 47                  | 30 | 11                        | 37.134 | 47                 | 41 | 37.13               | 70 | 00                        | 7 | 28.617             | 70 | 07 | 28.62 |
| 48                  | 00 | 11                        | 35.916 | 48                 | 11 | 35.92               | 70 | 30                        | 7 | 19.108             | 70 | 37 | 19.20 |
| 48                  | 30 | 11                        | 34.485 | 48                 | 41 | 34.48               | 71 | 00                        | 7 | 09.848             | 71 | 07 | 09.65 |
| 49                  | 00 | 11                        | 32.844 | 49                 | 11 | 32.84               | 71 | 30                        | 6 | 59.967             | 71 | 36 | 59.97 |
| 49                  | 30 | 11                        | 30.992 | 49                 | 41 | 30.99               | 72 | 00                        | 6 | 50.160             | 72 | 06 | 50.16 |
| 50                  | 00 | 11                        | 28.930 | 50                 | 11 | 28.93               | 72 | 30                        | 6 | 40.229             | 72 | 36 | 40.23 |
| 50                  | 30 | 11                        | 26.658 | 50                 | 41 | 26.66               | 73 | 00                        | 6 | 30.177             | 73 | 06 | 30.18 |
| 51                  | 00 | 11                        | 24.178 | 51                 | 11 | 24.18               | 73 | 30                        | 6 | 20.008             | 73 | 36 | 20.01 |
| 51                  | 30 | 11                        | 21.490 | 51                 | 41 | 21.49               | 74 | 00                        | 6 | 09.724             | 74 | 06 | 09.72 |
| 52                  | 00 | 11                        | 18.595 | 52                 | 11 | 18.60               | 74 | 30                        | 5 | 59.328             | 74 | 35 | 59.33 |
| 52                  | 30 | 11                        | 15.493 | 52                 | 41 | 15.49               | 75 | 00                        | 5 | 48.824             | 75 | 05 | 48.82 |
| 53                  | 00 | 11                        | 12.187 | 53                 | 11 | 12.19               | 75 | 30                        | 5 | 38.216             | 75 | 35 | 38.22 |
| 53                  | 30 | 11                        | 08.676 | 53                 | 41 | 08.68               | 76 | 00                        | 5 | 27.504             | 76 | 05 | 27.50 |
| 54                  | 00 | 11                        | 04.963 | 54                 | 11 | 04.96               | 76 | 30                        | 5 | 16.695             | 76 | 35 | 16.70 |
| 54                  | 30 | 11                        | 01.048 | 54                 | 41 | 01.05               | 77 | 00                        | 5 | 05.790             | 77 | 05 | 05.79 |
| 55                  | 00 | 10                        | 56.932 | 55                 | 10 | 56.93               | 77 | 30                        | 4 | 54.792             | 77 | 34 | 54.79 |
| 55                  | 30 | 10                        | 52.617 | 55                 | 40 | 52.62               | 78 | 00                        | 4 | 43.706             | 78 | 04 | 43.71 |
| 56                  | 00 | 10                        | 48.103 | 56                 | 10 | 48.10               | 78 | 30                        | 4 | 32.535             | 78 | 34 | 32.54 |
| 56                  | 30 | 10                        | 43.391 | 56                 | 40 | 43.39               | 79 | 00                        | 4 | 21.281             | 79 | 04 | 21.28 |
| 57                  | 00 | 10                        | 38.489 | 57                 | 10 | 38.49               | 79 | 30                        | 4 | 09.940             | 79 | 34 | 09.95 |
| 57                  | 30 | 10                        | 33.391 | 57                 | 40 | 33.39               | 80 | 00                        | 3 | 58.541             | 80 | 03 | 58.54 |
| 58                  | 00 | 10                        | 28.101 | 58                 | 10 | 28.10               | 80 | 30                        | 3 | 47.061             | 80 | 32 | 47.06 |
| 58                  | 30 | 10                        | 22.620 | 58                 | 40 | 22.62               | 81 | 00                        | 3 | 35.513             | 81 | 03 | 35.51 |
| 59                  | 00 | 10                        | 16.951 | 59                 | 10 | 16.95               | 81 | 30                        | 3 | 23.900             | 81 | 32 | 23.90 |
| 59                  | 30 | 10                        | 11.095 | 59                 | 40 | 11.10               | 82 | 00                        | 3 | 12.226             | 82 | 03 | 12.23 |
| 60                  | 00 | 10                        | 05.054 | 60                 | 10 | 05.05               | 82 | 30                        | 3 | 00.494             | 82 | 33 | 00.49 |
| 60                  | 30 | 9                         | 58.830 | 60                 | 30 | 58.83               | 83 | 00                        | 2 | 48.707             | 83 | 02 | 48.71 |
| 61                  | 00 | 9                         | 52.424 | 61                 | 00 | 52.42               | 83 | 30                        | 2 | 36.870             | 83 | 32 | 36.87 |
| 61                  | 30 | 9                         | 45.839 | 61                 | 30 | 45.84               | 84 | 00                        | 2 | 24.985             | 84 | 02 | 24.99 |
| 62                  | 00 | 9                         | 39.077 | 62                 | 00 | 39.08               | 84 | 30                        | 2 | 13.057             | 84 | 32 | 13.06 |
| 62                  | 30 | 9                         | 32.140 | 62                 | 30 | 32.14               | 85 | 00                        | 2 | 01.089             | 85 | 02 | 01.09 |
| 63                  | 00 | 9                         | 25.029 | 63                 | 00 | 25.03               | 85 | 30                        | 1 | 49.084             | 85 | 31 | 49.08 |
| 63                  | 30 | 9                         | 17.748 | 63                 | 30 | 17.75               | 86 | 00                        | 1 | 37.046             | 86 | 01 | 37.05 |
| 64                  | 00 | 9                         | 10.297 | 64                 | 00 | 10.30               | 86 | 30                        | 1 | 24.980             | 86 | 31 | 24.98 |
| 64                  | 30 | 9                         | 02.681 | 64                 | 30 | 02.68               | 87 | 00                        | 1 | 12.887             | 87 | 01 | 12.89 |
| 65                  | 00 | 8                         | 54.900 | 65                 | 00 | 54.90               | 87 | 30                        | 1 | 00.773             | 87 | 31 | 00.77 |
| 65                  | 30 | 8                         | 46.958 | 65                 | 30 | 46.96               | 88 | 00                        | 0 | 48.640             | 88 | 00 | 48.64 |
| 66                  | 00 | 8                         | 38.857 | 66                 | 00 | 38.86               | 88 | 30                        | 0 | 36.493             | 88 | 30 | 36.49 |
| 66                  | 30 | 8                         | 30.598 | 66                 | 30 | 30.60               | 89 | 00                        | 0 | 24.335             | 89 | 00 | 24.34 |
| 67                  | 00 | 8                         | 22.186 | 67                 | 00 | 22.19               | 89 | 30                        | 0 | 12.169             | 89 | 30 | 12.17 |
| 67                  | 30 | 8                         | 13.621 | 67                 | 30 | 13.62               | 90 | 00                        | 0 | 00.000             | 90 | 00 | 00.00 |

$$\begin{aligned} \phi-x &= +700^{\circ}0420 \sin 2x + 1^{\circ}3859 \sin 4x + 0^{\circ}0037 \sin 6x. \\ \phi-x &= [2.84512413] \sin 2x + [0.141720] \sin 4x + [7.573-10] \sin 6x. \end{aligned}$$

LATITUDE TRANSFORMATION—Continued.

*Geodetic to authalic.*

| Geodetic latitude. |    | Geodetic minus authalic. |        | Authalic latitude. |    | Geodetic latitude. |    | Geodetic minus authalic. |   | Authalic latitude. |    |    |       |
|--------------------|----|--------------------------|--------|--------------------|----|--------------------|----|--------------------------|---|--------------------|----|----|-------|
| $\varphi$          |    | $\varphi - \beta$        |        | $\beta$            |    | $\varphi$          |    | $\varphi - \beta$        |   | $\beta$            |    |    |       |
| °                  | '  | '                        | "      | °                  | '  | "                  | °  | '                        | " | °                  | '  | "  |       |
| 0                  | 00 | 0                        | 00.000 | 0                  | 00 | 00.00              | 22 | 30                       | 5 | 29.779             | 22 | 24 | 30.22 |
| 0                  | 30 | 0                        | 08.135 | 0                  | 29 | 51.87              | 23 | 00                       | 5 | 35.492             | 23 | 54 | 24.51 |
| 1                  | 00 | 0                        | 16.287 | 0                  | 59 | 43.73              | 23 | 30                       | 5 | 41.104             | 23 | 24 | 18.90 |
| 1                  | 30 | 0                        | 24.395 | 1                  | 29 | 35.61              | 24 | 00                       | 5 | 46.612             | 23 | 54 | 13.39 |
| 2                  | 00 | 0                        | 32.515 | 1                  | 59 | 27.49              | 24 | 30                       | 5 | 52.014             | 24 | 24 | 07.99 |
| 2                  | 30 | 0                        | 40.625 | 2                  | 29 | 19.38              | 25 | 00                       | 5 | 57.310             | 24 | 54 | 02.69 |
| 3                  | 00 | 0                        | 48.723 | 2                  | 59 | 11.28              | 25 | 30                       | 6 | 02.498             | 25 | 23 | 57.50 |
| 3                  | 30 | 0                        | 56.806 | 3                  | 29 | 03.19              | 26 | 00                       | 6 | 07.575             | 25 | 53 | 52.42 |
| 4                  | 00 | 1                        | 04.872 | 3                  | 58 | 55.13              | 26 | 30                       | 6 | 12.541             | 26 | 23 | 47.46 |
| 4                  | 30 | 1                        | 12.918 | 4                  | 28 | 47.08              | 27 | 00                       | 6 | 17.394             | 26 | 53 | 42.61 |
| 5                  | 00 | 1                        | 20.942 | 4                  | 58 | 39.06              | 27 | 30                       | 6 | 22.132             | 27 | 23 | 37.87 |
| 5                  | 30 | 1                        | 28.942 | 5                  | 28 | 31.06              | 28 | 00                       | 6 | 26.755             | 27 | 53 | 33.24 |
| 6                  | 00 | 1                        | 36.915 | 5                  | 58 | 23.08              | 28 | 30                       | 6 | 31.260             | 28 | 23 | 28.74 |
| 6                  | 30 | 1                        | 44.858 | 6                  | 28 | 15.14              | 29 | 00                       | 6 | 35.646             | 28 | 53 | 24.35 |
| 7                  | 00 | 1                        | 52.770 | 6                  | 58 | 07.23              | 29 | 30                       | 6 | 39.911             | 29 | 23 | 20.09 |
| 7                  | 30 | 2                        | 00.648 | 7                  | 27 | 59.35              | 30 | 00                       | 6 | 44.056             | 29 | 53 | 15.94 |
| 8                  | 00 | 2                        | 08.488 | 7                  | 57 | 51.51              | 30 | 30                       | 6 | 48.078             | 30 | 23 | 11.92 |
| 8                  | 30 | 2                        | 16.290 | 8                  | 27 | 43.71              | 31 | 00                       | 6 | 51.975             | 30 | 53 | 08.02 |
| 9                  | 00 | 2                        | 24.051 | 8                  | 57 | 35.95              | 31 | 30                       | 6 | 55.748             | 31 | 23 | 04.25 |
| 9                  | 30 | 2                        | 31.788 | 9                  | 27 | 28.23              | 32 | 00                       | 6 | 59.394             | 31 | 53 | 00.61 |
| 10                 | 00 | 2                        | 39.439 | 9                  | 57 | 20.56              | 32 | 30                       | 7 | 02.913             | 32 | 22 | 57.09 |
| 10                 | 30 | 2                        | 47.062 | 10                 | 27 | 12.94              | 33 | 00                       | 7 | 06.303             | 32 | 52 | 53.70 |
| 11                 | 00 | 2                        | 54.634 | 10                 | 57 | 05.37              | 33 | 30                       | 7 | 09.564             | 33 | 22 | 50.44 |
| 11                 | 30 | 3                        | 02.154 | 11                 | 26 | 57.85              | 34 | 00                       | 7 | 12.694             | 33 | 52 | 47.31 |
| 12                 | 00 | 3                        | 09.618 | 11                 | 56 | 50.38              | 34 | 30                       | 7 | 15.693             | 34 | 22 | 44.31 |
| 12                 | 30 | 3                        | 17.024 | 12                 | 26 | 42.98              | 35 | 00                       | 7 | 18.560             | 34 | 52 | 41.44 |
| 13                 | 00 | 3                        | 24.371 | 12                 | 56 | 35.63              | 35 | 30                       | 7 | 21.292             | 35 | 22 | 38.71 |
| 13                 | 30 | 3                        | 31.656 | 13                 | 26 | 28.34              | 36 | 00                       | 7 | 23.891             | 35 | 52 | 36.11 |
| 14                 | 00 | 3                        | 38.877 | 13                 | 56 | 21.12              | 36 | 30                       | 7 | 26.355             | 36 | 22 | 33.64 |
| 14                 | 30 | 3                        | 46.032 | 14                 | 26 | 13.97              | 37 | 00                       | 7 | 28.683             | 36 | 52 | 31.32 |
| 15                 | 00 | 3                        | 53.118 | 14                 | 56 | 06.88              | 37 | 30                       | 7 | 30.875             | 37 | 22 | 29.12 |
| 15                 | 30 | 4                        | 00.133 | 15                 | 25 | 59.87              | 38 | 00                       | 7 | 32.929             | 37 | 52 | 27.07 |
| 16                 | 00 | 4                        | 07.076 | 15                 | 55 | 52.92              | 38 | 30                       | 7 | 34.846             | 38 | 22 | 25.15 |
| 16                 | 30 | 4                        | 13.944 | 16                 | 25 | 46.06              | 39 | 00                       | 7 | 36.624             | 38 | 52 | 23.38 |
| 17                 | 00 | 4                        | 20.734 | 16                 | 55 | 39.27              | 39 | 30                       | 7 | 38.264             | 39 | 22 | 21.74 |
| 17                 | 30 | 4                        | 27.446 | 17                 | 25 | 32.55              | 40 | 00                       | 7 | 39.764             | 39 | 52 | 20.24 |
| 18                 | 00 | 4                        | 34.076 | 17                 | 55 | 25.92              | 40 | 30                       | 7 | 41.124             | 40 | 22 | 18.88 |
| 18                 | 30 | 4                        | 40.624 | 18                 | 25 | 19.38              | 41 | 00                       | 7 | 42.344             | 40 | 52 | 17.66 |
| 19                 | 00 | 4                        | 47.098 | 18                 | 55 | 12.91              | 41 | 30                       | 7 | 43.423             | 41 | 22 | 16.58 |
| 19                 | 30 | 4                        | 53.462 | 19                 | 25 | 06.54              | 42 | 00                       | 7 | 44.361             | 41 | 52 | 15.64 |
| 20                 | 00 | 4                        | 59.748 | 19                 | 55 | 00.25              | 42 | 30                       | 7 | 45.157             | 42 | 22 | 14.84 |
| 20                 | 30 | 5                        | 05.944 | 20                 | 24 | 54.06              | 43 | 00                       | 7 | 45.812             | 42 | 52 | 14.19 |
| 21                 | 00 | 5                        | 12.046 | 20                 | 54 | 47.95              | 43 | 30                       | 7 | 46.325             | 43 | 22 | 13.68 |
| 21                 | 30 | 5                        | 18.054 | 21                 | 24 | 41.95              | 44 | 00                       | 7 | 46.696             | 43 | 52 | 13.30 |
| 22                 | 00 | 5                        | 23.966 | 21                 | 54 | 36.03              | 44 | 30                       | 7 | 46.926             | 44 | 22 | 13.07 |
| 22                 | 30 | 5                        | 29.779 | 22                 | 24 | 30.22              | 45 | 00                       | 7 | 47.012             | 44 | 52 | 12.99 |

$$\varphi - \beta = +.467^{\circ}0129 \sin 2\varphi - 0^{\circ}4494 \sin 4\varphi + 0^{\circ}0005 \sin 6\varphi.$$

$$\varphi - \beta = [2.6993289] \sin 2\varphi - [0.65258 - 10] \sin 4\varphi + [6.732 - 10] \sin 6\varphi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geodetic to authalic—Continued.*

| Geodetic latitude. | Geodetic minus authalic. | Authalic latitude. | Geodetic latitude. | Geodetic minus authalic. | Authalic latitude. |
|--------------------|--------------------------|--------------------|--------------------|--------------------------|--------------------|
| $\varphi$          | $\varphi-\beta$          | $\beta$            | $\varphi$          | $\varphi-\beta$          | $\beta$            |
| 45 00              | 7 47.012                 | 44 52 12.99        | 67 30              | 5 30.678                 | 67 24 29.32        |
| 45 30              | 7 46.957                 | 45 22 13.04        | 68 00              | 5 24.964                 | 67 54 35.14        |
| 46 00              | 7 46.759                 | 45 52 13.24        | 68 30              | 5 18.951                 | 68 24 41.05        |
| 46 30              | 7 46.419                 | 46 22 13.58        | 69 00              | 5 12.940                 | 68 54 47.00        |
| 47 00              | 7 45.937                 | 46 52 14.00        | 69 30              | 5 06.833                 | 69 24 53.17        |
| 47 30              | 7 45.313                 | 47 22 14.60        | 70 00              | 5 00.633                 | 69 54 59.37        |
| 48 00              | 7 44.547                 | 47 52 15.45        | 70 30              | 4 54.341                 | 70 25 05.66        |
| 48 30              | 7 43.640                 | 48 22 16.36        | 71 00              | 4 47.958                 | 70 55 12.04        |
| 49 00              | 7 42.591                 | 48 52 17.41        | 71 30              | 4 41.488                 | 71 25 18.51        |
| 49 30              | 7 41.402                 | 49 22 18.60        | 72 00              | 4 34.931                 | 71 55 25.07        |
| 50 00              | 7 40.071                 | 49 52 19.93        | 72 30              | 4 28.296                 | 72 25 31.71        |
| 50 30              | 7 38.600                 | 50 22 21.40        | 73 00              | 4 21.567                 | 72 55 38.43        |
| 51 00              | 7 36.990                 | 50 52 23.01        | 73 30              | 4 14.764                 | 73 25 45.24        |
| 51 30              | 7 35.240                 | 51 22 24.76        | 74 00              | 4 07.883                 | 73 55 52.12        |
| 52 00              | 7 33.351                 | 51 52 26.65        | 74 30              | 4 00.927                 | 74 25 59.07        |
| 52 30              | 7 31.324                 | 52 22 28.68        | 75 00              | 3 53.896                 | 74 56 06.10        |
| 53 00              | 7 29.159                 | 52 52 30.84        | 75 30              | 3 46.794                 | 75 26 13.21        |
| 53 30              | 7 26.858                 | 53 22 33.14        | 76 00              | 3 39.622                 | 75 56 20.38        |
| 54 00              | 7 24.419                 | 53 52 35.58        | 76 30              | 3 32.383                 | 76 26 27.62        |
| 54 30              | 7 21.846                 | 54 22 38.15        | 77 00              | 3 25.080                 | 76 56 34.92        |
| 55 00              | 7 19.137                 | 54 52 40.86        | 77 30              | 3 17.713                 | 77 26 42.29        |
| 55 30              | 7 16.291                 | 55 22 43.71        | 78 00              | 3 10.286                 | 77 56 49.71        |
| 56 00              | 7 13.319                 | 55 52 46.68        | 78 30              | 3 02.806                 | 78 26 57.20        |
| 56 30              | 7 10.216                 | 56 22 49.79        | 79 00              | 2 55.259                 | 78 57 04.74        |
| 57 00              | 7 06.971                 | 56 52 53.03        | 79 30              | 2 47.663                 | 79 27 12.34        |
| 57 30              | 7 03.591                 | 57 22 56.50        | 80 00              | 2 40.017                 | 79 57 19.98        |
| 58 00              | 7 00.102                 | 57 52 59.90        | 80 30              | 2 32.322                 | 80 27 27.68        |
| 58 30              | 6 56.475                 | 58 23 03.52        | 81 00              | 2 24.579                 | 80 57 35.42        |
| 59 00              | 6 52.720                 | 58 53 07.28        | 81 30              | 2 16.793                 | 81 27 43.21        |
| 59 30              | 6 48.840                 | 59 23 11.16        | 82 00              | 2 08.965                 | 81 57 51.04        |
| 60 00              | 6 44.834                 | 59 53 15.17        | 82 30              | 2 01.097                 | 82 27 58.90        |
| 60 30              | 6 40.705                 | 60 23 19.30        | 83 00              | 1 53.192                 | 82 58 06.81        |
| 61 00              | 6 36.453                 | 60 53 23.55        | 83 30              | 1 45.252                 | 83 28 14.75        |
| 61 30              | 6 32.080                 | 61 23 27.92        | 84 00              | 1 37.280                 | 83 58 22.72        |
| 62 00              | 6 27.588                 | 61 53 32.41        | 84 30              | 1 29.279                 | 84 28 30.72        |
| 62 30              | 6 22.977                 | 62 23 37.02        | 85 00              | 1 21.250                 | 84 58 38.75        |
| 63 00              | 6 18.249                 | 62 53 41.75        | 85 30              | 1 13.196                 | 85 28 46.80        |
| 63 30              | 6 13.405                 | 63 23 46.60        | 86 00              | 1 05.120                 | 85 58 54.88        |
| 64 00              | 6 08.447                 | 63 53 51.55        | 86 30              | 0 57.023                 | 86 29 02.98        |
| 64 30              | 6 03.377                 | 64 23 56.62        | 87 00              | 0 48.910                 | 86 59 11.09        |
| 65 00              | 5 58.195                 | 64 54 01.80        | 87 30              | 0 40.781                 | 87 29 19.22        |
| 65 30              | 5 52.904                 | 65 24 07.10        | 88 00              | 0 32.646                 | 87 59 27.36        |
| 66 00              | 5 47.505                 | 65 54 12.50        | 88 30              | 0 24.498                 | 88 29 35.51        |
| 66 30              | 5 42.000                 | 66 24 18.00        | 89 00              | 0 16.330                 | 88 59 43.67        |
| 67 00              | 5 36.390                 | 66 54 23.61        | 89 30              | 0 08.166                 | 89 29 51.87        |
| 67 30              | 5 30.678                 | 67 24 29.32        | 90 00              | 0 00.000                 | 90 00 00.00        |

$$\varphi - \beta = +467''.0129 \sin 2\varphi - 0''.4494 \sin 4\varphi + 0''.0005 \sin 6\varphi.$$

$$\varphi - \beta = [2.6693289] \sin 2\varphi - [9.65258 - 10] \sin 4\varphi + [6.732 - 10] \sin 6\varphi.$$

LATITUDE TRANSFORMATION—Continued.

*Authalic to geodetic.*

| Authalic latitude. |    | Geodetic minus authalic. |        | Geodetic latitude. |    | Authalic latitude. |    | Geodetic minus authalic. |   | Geodetic latitude. |    |    |       |
|--------------------|----|--------------------------|--------|--------------------|----|--------------------|----|--------------------------|---|--------------------|----|----|-------|
| $\beta$            |    | $\varphi - \beta$        |        | $\varphi$          |    | $\beta$            |    | $\varphi - \beta$        |   | $\varphi$          |    |    |       |
| °                  | '  | '                        | ''     | °                  | '  | ''                 | °  | '                        | ' | ''                 | °  | '  | ''    |
| 0                  | 00 | 0                        | 00.000 | 0                  | 00 | 00.00              | 22 | 30                       | 5 | 30.837             | 22 | 35 | 30.84 |
| 0                  | 30 | 0                        | 08.172 | 0                  | 30 | 08.17              | 23 | 00                       | 5 | 36.549             | 23 | 05 | 36.55 |
| 1                  | 00 | 0                        | 16.341 | 1                  | 00 | 16.34              | 23 | 30                       | 5 | 42.159             | 23 | 35 | 42.16 |
| 1                  | 30 | 0                        | 24.505 | 1                  | 30 | 24.50              | 24 | 00                       | 5 | 47.663             | 24 | 05 | 47.66 |
| 2                  | 00 | 0                        | 32.662 | 2                  | 00 | 32.66              | 24 | 30                       | 5 | 53.062             | 24 | 35 | 53.06 |
| 2                  | 30 | 0                        | 40.809 | 2                  | 30 | 40.81              | 25 | 00                       | 5 | 58.352             | 25 | 05 | 58.35 |
| 3                  | 00 | 0                        | 48.943 | 3                  | 00 | 48.94              | 25 | 30                       | 6 | 03.532             | 25 | 35 | 03.53 |
| 3                  | 30 | 0                        | 57.062 | 3                  | 30 | 57.06              | 26 | 00                       | 6 | 08.601             | 26 | 05 | 08.60 |
| 4                  | 00 | 1                        | 05.164 | 4                  | 01 | 05.16              | 26 | 30                       | 6 | 13.558             | 26 | 35 | 13.59 |
| 4                  | 30 | 1                        | 13.245 | 4                  | 31 | 13.24              | 27 | 00                       | 6 | 18.400             | 27 | 05 | 18.40 |
| 5                  | 00 | 1                        | 21.304 | 5                  | 01 | 21.30              | 27 | 30                       | 6 | 23.126             | 27 | 35 | 23.13 |
| 5                  | 30 | 1                        | 29.339 | 5                  | 31 | 29.34              | 28 | 00                       | 6 | 27.735             | 28 | 05 | 27.74 |
| 6                  | 00 | 1                        | 37.345 | 6                  | 01 | 37.34              | 28 | 30                       | 6 | 32.225             | 28 | 35 | 32.22 |
| 6                  | 30 | 1                        | 45.322 | 6                  | 31 | 45.32              | 29 | 00                       | 6 | 36.596             | 29 | 05 | 36.60 |
| 7                  | 00 | 1                        | 53.267 | 7                  | 01 | 53.27              | 29 | 30                       | 6 | 40.845             | 29 | 35 | 40.84 |
| 7                  | 30 | 2                        | 01.177 | 7                  | 32 | 01.18              | 30 | 00                       | 6 | 44.871             | 30 | 05 | 44.97 |
| 8                  | 00 | 2                        | 09.049 | 8                  | 02 | 09.05              | 30 | 30                       | 6 | 48.974             | 30 | 35 | 48.97 |
| 8                  | 30 | 2                        | 16.882 | 8                  | 32 | 16.88              | 31 | 00                       | 6 | 52.852             | 31 | 05 | 52.85 |
| 9                  | 00 | 2                        | 24.673 | 9                  | 02 | 24.67              | 31 | 30                       | 6 | 56.603             | 31 | 35 | 56.60 |
| 9                  | 30 | 2                        | 32.420 | 9                  | 32 | 32.42              | 32 | 00                       | 7 | 00.227             | 32 | 05 | 00.23 |
| 10                 | 00 | 2                        | 40.120 | 10                 | 02 | 40.12              | 32 | 30                       | 7 | 03.723             | 32 | 35 | 03.73 |
| 10                 | 30 | 2                        | 47.770 | 10                 | 32 | 47.77              | 33 | 00                       | 7 | 07.089             | 33 | 05 | 07.09 |
| 11                 | 00 | 2                        | 55.369 | 11                 | 02 | 55.37              | 33 | 30                       | 7 | 10.324             | 33 | 35 | 10.32 |
| 11                 | 30 | 3                        | 02.915 | 11                 | 33 | 02.92              | 34 | 00                       | 7 | 13.429             | 34 | 05 | 13.43 |
| 12                 | 00 | 3                        | 10.404 | 12                 | 03 | 10.40              | 34 | 30                       | 7 | 16.400             | 34 | 35 | 16.40 |
| 12                 | 30 | 3                        | 17.835 | 12                 | 33 | 17.84              | 35 | 00                       | 7 | 19.239             | 35 | 05 | 19.24 |
| 13                 | 00 | 3                        | 25.205 | 13                 | 03 | 25.20              | 35 | 30                       | 7 | 21.943             | 35 | 35 | 21.94 |
| 13                 | 30 | 3                        | 32.512 | 13                 | 33 | 32.51              | 36 | 00                       | 7 | 24.512             | 36 | 05 | 24.51 |
| 14                 | 00 | 3                        | 39.754 | 14                 | 03 | 39.75              | 36 | 30                       | 7 | 26.946             | 36 | 35 | 26.95 |
| 14                 | 30 | 3                        | 46.929 | 14                 | 33 | 46.93              | 37 | 00                       | 7 | 29.243             | 37 | 05 | 29.24 |
| 15                 | 00 | 3                        | 54.034 | 15                 | 03 | 54.03              | 37 | 30                       | 7 | 31.403             | 37 | 35 | 31.40 |
| 15                 | 30 | 4                        | 01.067 | 15                 | 34 | 01.07              | 38 | 00                       | 7 | 33.425             | 38 | 05 | 33.42 |
| 16                 | 00 | 4                        | 08.027 | 16                 | 04 | 08.03              | 38 | 30                       | 7 | 35.309             | 38 | 35 | 35.31 |
| 16                 | 30 | 4                        | 14.910 | 16                 | 34 | 14.91              | 39 | 00                       | 7 | 37.054             | 39 | 05 | 37.05 |
| 17                 | 00 | 4                        | 21.715 | 17                 | 04 | 21.72              | 39 | 30                       | 7 | 38.659             | 39 | 35 | 38.66 |
| 17                 | 30 | 4                        | 28.440 | 17                 | 34 | 28.44              | 40 | 00                       | 7 | 40.125             | 40 | 05 | 40.12 |
| 18                 | 00 | 4                        | 35.082 | 18                 | 04 | 35.08              | 40 | 30                       | 7 | 41.450             | 40 | 35 | 41.45 |
| 18                 | 30 | 4                        | 41.641 | 18                 | 34 | 41.64              | 41 | 00                       | 7 | 42.634             | 41 | 05 | 42.63 |
| 19                 | 00 | 4                        | 48.113 | 19                 | 04 | 48.11              | 41 | 30                       | 7 | 43.678             | 41 | 35 | 43.68 |
| 19                 | 30 | 4                        | 54.496 | 19                 | 34 | 54.50              | 42 | 00                       | 7 | 44.580             | 42 | 05 | 44.58 |
| 20                 | 00 | 5                        | 00.790 | 20                 | 05 | 00.79              | 42 | 30                       | 7 | 45.340             | 42 | 35 | 45.34 |
| 20                 | 30 | 5                        | 06.991 | 20                 | 35 | 06.99              | 43 | 00                       | 7 | 45.959             | 43 | 05 | 45.96 |
| 21                 | 00 | 5                        | 13.098 | 21                 | 05 | 13.10              | 43 | 30                       | 7 | 46.435             | 43 | 35 | 46.44 |
| 21                 | 30 | 5                        | 19.109 | 21                 | 35 | 19.11              | 44 | 00                       | 7 | 46.770             | 44 | 05 | 46.77 |
| 22                 | 00 | 5                        | 25.023 | 22                 | 05 | 25.02              | 44 | 30                       | 7 | 46.962             | 44 | 35 | 46.96 |
| 22                 | 30 | 5                        | 30.837 | 22                 | 35 | 30.84              | 45 | 00                       | 7 | 47.012             | 45 | 05 | 47.01 |

$$\varphi - \beta = +467^{\circ}0127 \sin 2\beta + 0^{\circ}6080 \sin 4\beta + 0^{\circ}0011 \sin 6\beta.$$

$$\varphi - \beta = [2.6693287] \sin 2\beta + [9.78390 - 10] \sin 4\beta + [7.031 - 10] \sin 6\beta.$$



## LATITUDE TRANSFORMATION—Continued.

*Authalic to geodetic—Continued.*

| Authalic latitude. | Geodetic minus authalic. | Geodetic latitude. | Authalic latitude. | Geodetic minus authalic. | Geodetic latitude. |
|--------------------|--------------------------|--------------------|--------------------|--------------------------|--------------------|
| $\beta$            | $\varphi - \beta$        | $\varphi$          | $\beta$            | $\varphi - \beta$        | $\varphi$          |
| 45 00              | 7 47.012                 | 45 07 47.01        | 67 30              | 5 29.621                 | 67 35 29.62        |
| 45 30              | 7 46.919                 | 45 37 46.92        | 68 00              | 5 23.808                 | 68 05 23.81        |
| 46 00              | 7 46.685                 | 46 07 46.68        | 68 30              | 5 17.896                 | 68 35 17.90        |
| 46 30              | 7 46.308                 | 46 37 46.31        | 69 00              | 5 11.889                 | 69 05 11.89        |
| 47 00              | 7 45.790                 | 47 07 45.79        | 69 30              | 5 05.787                 | 69 35 05.79        |
| 47 30              | 7 45.129                 | 47 37 45.13        | 70 00              | 4 59.592                 | 70 04 59.59        |
| 48 00              | 7 44.327                 | 48 07 44.33        | 70 30              | 4 53.307                 | 70 34 53.31        |
| 48 30              | 7 43.384                 | 48 37 43.38        | 71 00              | 4 46.933                 | 71 04 46.93        |
| 49 00              | 7 42.299                 | 49 07 42.30        | 71 30              | 4 40.472                 | 71 34 40.47        |
| 49 30              | 7 41.074                 | 49 37 41.07        | 72 00              | 4 33.926                 | 72 04 33.93        |
| 50 00              | 7 39.709                 | 50 07 39.71        | 72 30              | 4 27.297                 | 72 34 27.30        |
| 50 30              | 7 38.205                 | 50 37 38.20        | 73 00              | 4 20.588                 | 73 04 20.59        |
| 51 00              | 7 36.559                 | 51 07 36.56        | 73 30              | 4 13.799                 | 73 34 13.80        |
| 51 30              | 7 34.776                 | 51 37 34.78        | 74 00              | 4 06.934                 | 74 04 06.93        |
| 52 00              | 7 32.854                 | 52 07 32.85        | 74 30              | 3 59.994                 | 74 33 59.99        |
| 52 30              | 7 30.795                 | 52 37 30.80        | 75 00              | 3 52.981                 | 75 03 52.98        |
| 53 00              | 7 28.599                 | 53 07 28.60        | 75 30              | 3 45.808                 | 75 33 45.81        |
| 53 30              | 7 26.266                 | 53 37 26.27        | 76 00              | 3 38.746                 | 76 03 38.75        |
| 54 00              | 7 23.798                 | 54 07 23.80        | 76 30              | 3 31.529                 | 76 33 31.53        |
| 54 30              | 7 21.194                 | 54 37 21.19        | 77 00              | 3 24.247                 | 77 03 24.25        |
| 55 00              | 7 18.457                 | 55 07 18.46        | 77 30              | 3 16.903                 | 77 33 16.90        |
| 55 30              | 7 15.587                 | 55 37 15.59        | 78 00              | 3 09.500                 | 78 03 09.50        |
| 56 00              | 7 12.584                 | 56 07 12.58        | 78 30              | 3 02.040                 | 78 33 02.04        |
| 56 30              | 7 09.450                 | 56 37 09.45        | 79 00              | 2 54.525                 | 79 03 54.52        |
| 57 00              | 7 06.185                 | 57 07 06.18        | 79 30              | 2 46.957                 | 79 32 46.96        |
| 57 30              | 7 02.791                 | 57 37 02.79        | 80 00              | 2 39.338                 | 80 02 39.34        |
| 58 00              | 6 59.269                 | 58 06 59.27        | 80 30              | 2 31.671                 | 80 32 31.67        |
| 58 30              | 6 55.619                 | 58 36 55.62        | 81 00              | 2 23.958                 | 81 02 23.96        |
| 59 00              | 6 51.844                 | 59 06 51.84        | 81 30              | 2 16.202                 | 81 32 16.20        |
| 59 30              | 6 47.943                 | 59 36 47.94        | 82 00              | 2 08.405                 | 82 02 08.40        |
| 60 00              | 6 43.918                 | 60 06 43.92        | 82 30              | 2 00.563                 | 82 32 00.57        |
| 60 30              | 6 39.771                 | 60 36 39.77        | 83 00              | 1 52.696                 | 83 02 52.70        |
| 61 00              | 6 35.503                 | 61 06 35.50        | 83 30              | 1 44.789                 | 83 31 44.79        |
| 61 30              | 6 31.115                 | 61 36 31.12        | 84 00              | 1 36.851                 | 84 01 36.85        |
| 62 00              | 6 26.608                 | 62 06 26.61        | 84 30              | 1 28.883                 | 84 31 28.88        |
| 62 30              | 6 21.983                 | 62 36 21.98        | 85 00              | 1 20.889                 | 85 01 20.89        |
| 63 00              | 6 17.243                 | 63 06 17.24        | 85 30              | 1 12.870                 | 85 31 12.87        |
| 63 30              | 6 12.389                 | 63 36 12.39        | 86 00              | 1 04.828                 | 86 01 04.83        |
| 64 00              | 6 07.422                 | 64 06 07.42        | 86 30              | 0 56.768                 | 86 30 56.77        |
| 64 30              | 6 02.343                 | 64 36 02.34        | 87 00              | 0 48.690                 | 87 00 48.69        |
| 65 00              | 5 57.154                 | 65 05 57.15        | 87 30              | 0 40.598                 | 87 30 40.60        |
| 65 30              | 5 51.858                 | 65 35 51.86        | 88 00              | 0 32.493                 | 88 00 32.49        |
| 66 00              | 5 46.454                 | 66 05 46.45        | 88 30              | 0 24.378                 | 88 30 24.38        |
| 66 30              | 5 40.946                 | 66 35 40.95        | 89 00              | 0 16.256                 | 89 00 16.26        |
| 67 00              | 5 35.334                 | 67 05 35.33        | 89 30              | 0 08.129                 | 89 30 08.13        |
| 67 30              | 5 29.621                 | 67 35 29.62        | 90 00              | 0 00.000                 | 90 00 00.00        |

$$\varphi - \beta = +467^{\circ}0127 \sin 2\beta + 0^{\circ}6080 \sin 4\beta + 0^{\circ}0011 \sin 6\beta.$$

$$\varphi - \beta = [2.6693287] \sin 2\beta + [9.78390 - 10] \sin 4\beta + [7.031 - 10] \sin 6\beta.$$

**TRANSFORMATION FROM GEOGRAPHICAL TO AZIMUTHAL  
COORDINATES—CENTER ON THE EQUATOR.**

*Values of the great circle central distance,  $\zeta$ .  $\cos \zeta = \cos \lambda \cos \varphi$ .*

| Long. | Lat. 0°.   | Lat. 5°.   | Lat. 10°.  | Lat. 15°.  | Lat. 20°.  |
|-------|------------|------------|------------|------------|------------|
| 0...  | 0 00 00.0  | 5 00 00.0  | 10 00 00.0 | 15 00 00.0 | 20 00 00.0 |
| 5...  | 5 00 00.0  | 7 04 00.0  | 11 10 08.2 | 15 47 35.7 | 20 35 26.5 |
| 10... | 10 00 00.0 | 11 10 08.2 | 14 06 21.6 | 17 57 49.8 | 22 16 07.4 |
| 15... | 15 00 00.0 | 15 47 35.7 | 17 57 49.8 | 21 05 26.0 | 24 48 51.2 |
| 20... | 20 00 00.0 | 20 35 26.5 | 22 16 07.4 | 24 48 51.2 | 27 59 27.3 |
| 25... | 25 00 00.0 | 25 27 48.8 | 26 48 21.4 | 28 54 16.4 | 31 36 30.0 |
| 30... | 30 00 00.0 | 30 22 31.8 | 31 28 29.8 | 33 13 33.4 | 35 31 52.9 |
| 35... | 35 00 00.0 | 35 18 36.7 | 36 13 28.3 | 37 41 54.4 | 39 40 06.4 |
| 40... | 40 00 00.0 | 40 15 32.9 | 41 01 35.2 | 42 16 24.6 | 43 57 29.6 |
| 45... | 45 00 00.0 | 45 13 03.4 | 45 51 50.3 | 46 55 13.7 | 48 21 31.9 |
| 50... | 50 00 00.0 | 50 10 57.7 | 50 43 35.6 | 51 37 09.1 | 52 50 29.2 |
| 55... | 55 00 00.0 | 55 09 09.1 | 55 36 26.1 | 56 21 21.3 | 57 23 07.4 |
| 60... | 60 00 00.0 | 60 07 32.9 | 60 30 04.6 | 61 07 15.3 | 61 58 32.4 |
| 65... | 65 00 00.0 | 65 06 05.8 | 65 24 18.8 | 65 54 25.4 | 66 36 03.7 |
| 70... | 70 00 00.0 | 70 04 45.6 | 70 18 59.4 | 70 42 32.4 | 71 15 10.0 |
| 75... | 75 00 00.0 | 75 03 30.3 | 75 13 59.2 | 75 31 21.0 | 75 55 26.1 |
| 80... | 80 00 00.0 | 80 02 18.4 | 80 09 12.4 | 80 20 38.6 | 80 36 31.4 |
| 85... | 85 00 00.0 | 85 01 08.7 | 85 04 34.1 | 85 10 14.8 | 85 18 08.1 |
| 90... | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 |
|       | Lat. 25°.  | Lat. 30°.  | Lat. 35°.  | Lat. 40°.  | Lat. 45°.  |
| 0...  | 25 00 00.0 | 30 00 00.0 | 35 00 00.0 | 40 00 00.0 | 45 00 00.0 |
| 5...  | 25 27 48.8 | 30 22 31.8 | 35 18 36.7 | 40 15 32.9 | 45 13 03.4 |
| 10... | 26 48 21.4 | 31 28 29.8 | 36 13 28.3 | 41 01 35.2 | 45 51 50.3 |
| 15... | 28 54 16.4 | 33 13 33.4 | 37 41 54.4 | 42 16 24.6 | 46 55 13.7 |
| 20... | 31 36 30.0 | 35 31 52.9 | 39 40 06.4 | 43 57 29.6 | 48 21 31.9 |
| 25... | 34 46 31.6 | 38 17 23.7 | 42 03 48.3 | 46 01 50.7 | 50 02 02.2 |
| 30... | 38 17 23.7 | 41 24 34.7 | 44 48 48.1 | 48 26 21.2 | 52 14 19.5 |
| 35... | 42 03 48.3 | 44 48 48.1 | 47 51 17.7 | 51 08 00.9 | 54 36 13.5 |
| 40... | 46 01 50.7 | 48 26 21.2 | 51 08 00.9 | 54 04 04.9 | 57 19 08.1 |
| 45... | 50 02 02.2 | 52 14 19.5 | 54 36 13.5 | 57 12 08.9 | 60 00 00.0 |
| 50... | 54 22 06.2 | 56 10 27.0 | 58 13 40.7 | 60 30 04.6 | 62 57 57.5 |
| 55... | 58 40 43.3 | 60 12 57.6 | 61 58 32.4 | 63 56 07.3 | 66 04 21.1 |
| 60... | 63 03 13.6 | 64 20 28.0 | 65 45 44.9 | 67 28 44.4 | 69 17 42.7 |
| 65... | 67 28 44.4 | 68 31 51.5 | 69 44 44.3 | 71 06 37.7 | 72 36 44.2 |
| 70... | 71 56 32.1 | 72 46 14.2 | 73 43 47.5 | 74 48 39.9 | 76 00 16.4 |
| 75... | 76 26 01.5 | 77 02 50.9 | 77 45 34.9 | 78 33 51.7 | 79 27 16.9 |
| 80... | 80 56 42.8 | 81 21 03.0 | 81 49 20.2 | 82 21 20.6 | 82 56 49.1 |
| 85... | 85 28 10.2 | 85 40 16.5 | 85 54 21.4 | 86 10 18.4 | 86 28 00.2 |
| 90... | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 | 90 00 00.0 |

**TRANSFORMATION FROM GEOGRAPHICAL TO AZIMUTHAL  
COORDINATES—CENTER ON THE EQUATOR—Continued.**
*Values of the great circle central distance,  $\xi$ .  $\cos \xi = \cos \lambda \cos \varphi$ —Continued.*

| Long. | Lat. 45°. |    |      | Lat. 50°. |    |      | Lat. 55°. |    |      | Lat. 60°. |    |      | Lat. 65°. |    |      |
|-------|-----------|----|------|-----------|----|------|-----------|----|------|-----------|----|------|-----------|----|------|
| °     | °         | '  | ''   | °         | '  | ''   | °         | '  | ''   | °         | '  | ''   | °         | '  | ''   |
| 0...  | 45        | 00 | 00.0 | 50        | 00 | 00.0 | 55        | 00 | 00.0 | 60        | 00 | 00.0 | 65        | 00 | 00.0 |
| 5...  | 45        | 13 | 03.4 | 50        | 10 | 57.7 | 55        | 09 | 09.1 | 60        | 07 | 32.9 | 65        | 06 | 05.8 |
| 10... | 45        | 51 | 50.3 | 50        | 43 | 35.6 | 55        | 36 | 26.1 | 60        | 30 | 04.6 | 65        | 24 | 18.8 |
| 15... | 46        | 55 | 13.7 | 51        | 37 | 09.1 | 56        | 21 | 21.3 | 61        | 07 | 15.3 | 65        | 54 | 25.4 |
| 20... | 48        | 21 | 31.9 | 52        | 50 | 29.2 | 57        | 23 | 07.4 | 61        | 58 | 32.4 | 66        | 36 | 03.7 |
| 25... | 50        | 02 | 02.2 | 54        | 22 | 03.2 | 58        | 40 | 43.3 | 63        | 03 | 13.6 | 67        | 28 | 44.4 |
| 30... | 52        | 14 | 19.5 | 56        | 10 | 27.0 | 60        | 12 | 57.6 | 64        | 20 | 28.0 | 68        | 31 | 51.5 |
| 35... | 54        | 36 | 13.5 | 58        | 13 | 40.7 | 61        | 58 | 32.4 | 65        | 45 | 44.9 | 69        | 44 | 44.3 |
| 40... | 57        | 12 | 08.1 | 60        | 30 | 04.6 | 63        | 56 | 07.3 | 67        | 28 | 44.4 | 71        | 06 | 37.7 |
| 45... | 60        | 00 | 00.0 | 62        | 57 | 57.5 | 66        | 04 | 21.1 | 69        | 17 | 42.7 | 72        | 36 | 44.2 |
| 50... | 62        | 57 | 57.5 | 65        | 35 | 43.8 | 68        | 21 | 55.0 | 71        | 15 | 10.0 | 74        | 14 | 14.3 |
| 55... | 66        | 04 | 21.1 | 68        | 21 | 55.0 | 70        | 47 | 33.1 | 73        | 20 | 03.2 | 75        | 58 | 17.5 |
| 60... | 69        | 17 | 42.7 | 71        | 15 | 10.0 | 73        | 20 | 03.2 | 75        | 31 | 21.0 | 77        | 48 | 03.3 |
| 65... | 72        | 36 | 44.2 | 74        | 14 | 14.3 | 75        | 58 | 17.5 | 77        | 48 | 03.3 | 79        | 42 | 41.1 |
| 70... | 76        | 00 | 16.4 | 77        | 18 | 00.0 | 78        | 41 | 11.9 | 80        | 09 | 12.4 | 81        | 41 | 20.9 |
| 75... | 79        | 27 | 16.9 | 80        | 25 | 24.3 | 81        | 27 | 45.9 | 82        | 33 | 52.3 | 83        | 43 | 13.2 |
| 80... | 82        | 56 | 49.1 | 83        | 35 | 28.9 | 84        | 17 | 01.8 | 85        | 01 | 08.7 | 85        | 47 | 28.2 |
| 85... | 86        | 28 | 00.2 | 86        | 47 | 18.5 | 87        | 08 | 04.4 | 87        | 30 | 08.6 | 87        | 53 | 20.8 |
| 90... | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 |
|       |           |    |      |           |    |      |           |    |      |           |    |      |           |    |      |
|       | Lat. 70°. |    |      | Lat. 75°. |    |      | Lat. 80°. |    |      | Lat. 85°. |    |      | Lat. 90°. |    |      |
| 0...  | 70        | 00 | 00.0 | 75        | 00 | 00.0 | 80        | 00 | 00.0 | 85        | 00 | 00.0 | 90        | 00 | 00.0 |
| 5...  | 70        | 04 | 45.6 | 75        | 03 | 30.3 | 80        | 02 | 18.4 | 85        | 01 | 08.7 | 90        | 00 | 00.0 |
| 10... | 70        | 18 | 59.4 | 75        | 13 | 59.2 | 80        | 09 | 12.4 | 85        | 04 | 34.1 | 90        | 00 | 00.0 |
| 15... | 70        | 42 | 32.4 | 75        | 31 | 21.0 | 80        | 20 | 38.6 | 85        | 10 | 14.8 | 90        | 00 | 00.0 |
| 20... | 71        | 15 | 10.0 | 75        | 55 | 26.1 | 80        | 36 | 31.4 | 85        | 18 | 08.1 | 90        | 00 | 00.0 |
| 25... | 71        | 56 | 32.1 | 76        | 26 | 01.5 | 80        | 56 | 42.8 | 85        | 28 | 10.2 | 90        | 00 | 00.0 |
| 30... | 72        | 46 | 14.2 | 77        | 02 | 50.9 | 81        | 21 | 03.0 | 85        | 40 | 16.5 | 90        | 00 | 00.0 |
| 35... | 73        | 43 | 47.5 | 77        | 45 | 34.9 | 81        | 49 | 20.2 | 85        | 54 | 21.4 | 90        | 00 | 00.0 |
| 40... | 74        | 48 | 39.9 | 78        | 33 | 51.7 | 82        | 21 | 20.6 | 86        | 10 | 18.4 | 90        | 00 | 00.0 |
| 45... | 76        | 00 | 16.4 | 79        | 27 | 16.9 | 82        | 56 | 49.1 | 86        | 28 | 00.2 | 90        | 00 | 00.0 |
| 50... | 77        | 18 | 00.0 | 80        | 25 | 24.3 | 83        | 35 | 28.9 | 86        | 47 | 18.5 | 90        | 00 | 00.0 |
| 55... | 78        | 41 | 11.9 | 81        | 27 | 45.9 | 84        | 17 | 01.8 | 87        | 08 | 04.4 | 90        | 00 | 00.0 |
| 60... | 80        | 09 | 12.4 | 82        | 33 | 52.3 | 85        | 01 | 08.7 | 87        | 30 | 08.6 | 90        | 00 | 00.0 |
| 65... | 81        | 41 | 20.9 | 83        | 43 | 13.2 | 85        | 47 | 29.2 | 87        | 53 | 20.8 | 90        | 00 | 00.0 |
| 70... | 83        | 16 | 56.2 | 84        | 55 | 17.2 | 86        | 35 | 42.5 | 88        | 17 | 30.5 | 90        | 00 | 00.0 |
| 75... | 84        | 55 | 17.2 | 86        | 09 | 32.5 | 87        | 25 | 26.6 | 88        | 42 | 26.8 | 90        | 00 | 00.0 |
| 80... | 86        | 35 | 42.5 | 87        | 25 | 26.8 | 88        | 16 | 19.4 | 89        | 07 | 58.2 | 90        | 00 | 00.0 |
| 85... | 88        | 17 | 30.5 | 88        | 42 | 26.8 | 89        | 07 | 58.2 | 89        | 33 | 53.2 | 90        | 00 | 00.0 |
| 90... | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 | 90        | 00 | 00.0 |

**TRANSFORMATION FROM GEOGRAPHICAL TO AZIMUTHAL  
COORDINATES—CENTER ON THE EQUATOR—Continued.**

*Values of the azimuth reckoned from the north,  $\alpha$ .  $\tan \alpha = \sin \lambda \cot \varphi$*

| Long. | Lat. 0°.   | Lat. 5°.   | Lat. 10°.  | Lat. 15°.  | Lat. 20°.  |
|-------|------------|------------|------------|------------|------------|
| 0     | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  |
| 5...  | 90 00 00.0 | 44 53 26.8 | 26 18 08.9 | 18 01 05.3 | 13 27 59.0 |
| 10... | 90 00 00.0 | 63 15 35.2 | 44 33 41.2 | 32 56 44.9 | 25 30 29.0 |
| 15... | 90 00 00.0 | 71 19 23.5 | 55 44 03.7 | 44 00 25.3 | 35 24 59.8 |
| 20... | 90 00 00.0 | 75 39 05.2 | 62 43 36.6 | 51 55 25.5 | 43 13 09.0 |
| 25... | 90 00 00.0 | 78 18 14.7 | 67 21 10.4 | 57 37 27.9 | 49 15 50.7 |
| 30... | 90 00 00.0 | 80 04 30.0 | 70 34 28.6 | 61 48 47.6 | 53 56 51.4 |
| 35... | 90 00 00.0 | 81 19 38.7 | 72 54 42.1 | 64 57 36.5 | 57 36 08.3 |
| 40... | 90 00 00.0 | 82 14 57.1 | 74 39 36.7 | 67 22 15.4 | 60 28 47.4 |
| 45... | 90 00 00.0 | 82 56 48.4 | 75 59 53.0 | 69 14 47.1 | 62 45 49.3 |
| 50... | 90 00 00.0 | 83 29 04.5 | 77 02 15.1 | 70 43 15.7 | 64 35 10.4 |
| 55... | 90 00 00.0 | 83 54 13.3 | 77 51 07.7 | 71 53 12.4 | 66 02 35.5 |
| 60... | 90 00 00.0 | 84 13 52.9 | 78 29 29.8 | 72 48 28.4 | 67 12 14.8 |
| 65... | 90 00 00.0 | 84 29 10.1 | 78 59 25.2 | 73 31 47.0 | 68 07 11.2 |
| 70... | 90 00 00.0 | 84 40 51.2 | 79 22 20.7 | 74 05 05.0 | 68 49 37.8 |
| 75... | 90 00 00.0 | 84 49 28.4 | 79 39 17.0 | 74 29 45.3 | 69 21 11.2 |
| 80... | 90 00 00.0 | 84 55 23.8 | 79 50 56.1 | 74 46 45.3 | 69 42 58.2 |
| 85... | 90 00 00.0 | 84 58 51.6 | 79 57 45.3 | 74 56 43.1 | 69 55 46.9 |
| 90... | 90 00 00.0 | 85 00 00.0 | 80 00 00.0 | 75 00 00.0 | 70 00 00.0 |

  

|       | Lat. 25°.  | Lat. 30°.  | Lat. 35°.  | Lat. 40°.  | Lat. 45°.  |
|-------|------------|------------|------------|------------|------------|
| 0...  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  |
| 5...  | 10 35 12.4 | 8 35 04.0  | 7 05 42.7  | 5 55 47.8  | 4 58 51.8  |
| 10... | 20 25 29.3 | 16 44 22.5 | 13 55 41.1 | 11 41 31.5 | 9 51 08.9  |
| 15... | 29 01 55.2 | 24 08 46.0 | 20 17 09.3 | 17 08 32.3 | 14 30 38.9 |
| 20... | 36 15 31.4 | 30 38 32.4 | 26 02 00.4 | 22 10 33.6 | 18 52 54.2 |
| 25... | 42 11 10.6 | 36 12 14.4 | 31 06 48.8 | 26 43 56.8 | 22 54 35.3 |
| 30... | 46 59 49.0 | 40 53 36.2 | 35 31 46.7 | 30 47 23.0 | 26 33 54.2 |
| 35... | 50 53 22.2 | 44 48 43.7 | 39 19 21.7 | 34 21 18.1 | 29 50 15.2 |
| 40... | 54 02 28.1 | 48 04 11.6 | 42 33 06.5 | 37 27 13.4 | 32 43 56.7 |
| 45... | 56 35 48.5 | 50 46 06.5 | 45 16 51.2 | 40 07 14.7 | 35 15 51.8 |
| 50... | 58 40 12.9 | 52 59 43.8 | 47 34 15.4 | 42 23 38.7 | 37 27 13.4 |
| 55... | 60 20 56.5 | 54 49 23.7 | 49 28 34.8 | 44 18 38.9 | 39 19 21.7 |
| 60... | 61 41 59.8 | 56 18 35.8 | 51 02 36.3 | 45 54 16.9 | 40 53 36.2 |
| 65... | 62 46 24.8 | 57 30 05.1 | 52 18 38.0 | 47 12 18.5 | 42 11 10.5 |
| 70... | 63 36 28.2 | 58 25 59.8 | 53 18 30.7 | 48 14 12.1 | 43 13 09.0 |
| 75... | 64 13 50.7 | 59 07 57.1 | 54 03 40.8 | 49 01 09.0 | 44 00 25.3 |
| 80... | 64 39 44.6 | 59 37 07.5 | 54 35 12.5 | 49 34 03.2 | 44 33 41.2 |
| 85... | 64 54 58.4 | 59 54 19.1 | 54 53 50.3 | 49 53 32.7 | 44 53 26.8 |
| 90... | 65 00 00.0 | 60 00 00.0 | 55 00 00.0 | 50 00 00.0 | 45 00 00.0 |

**TRANSFORMATION FROM GEOGRAPHICAL TO AZIMUTHAL  
COORDINATES—CENTER ON THE EQUATOR—Continued.**

Values of the azimuth reckoned from the north,  $\alpha$ .  $\tan \alpha = \sin \lambda \cot \phi$ —  
Continued.

| Long. | Lat. 45°.  | Lat. 50°.  | Lat. 55°.  | Lat. 60°.  | Lat. 65°.  |
|-------|------------|------------|------------|------------|------------|
| "     | " "        | " "        | " "        | " "        | " "        |
| 0...  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  |
| 5...  | 4 58 51.8  | 4 10 57.8  | 3 29 32.2  | 2 52 50.4  | 2 19 38.3  |
| 10... | 9 51 03.9  | 8 17 24.4  | 6 55 57.2  | 5 43 30.4  | 4 37 45.6  |
| 15... | 14 30 38.9 | 12 15 10.6 | 10 16 19.4 | 8 29 55.6  | 6 52 54.1  |
| 20... | 18 52 54.2 | 16 00 46.4 | 13 28 04.2 | 11 10 12.8 | 9 03 41.7  |
| 25... | 22 54 35.3 | 19 31 31.7 | 16 29 04.4 | 13 42 43.8 | 11 08 54.3 |
| 30... | 26 33 54.2 | 22 45 37.7 | 19 17 43.2 | 16 06 07.6 | 13 07 27.4 |
| 35... | 29 50 15.2 | 25 42 03.4 | 21 52 53.4 | 18 19 21.1 | 14 58 26.4 |
| 40... | 32 43 56.7 | 28 20 26.8 | 24 13 54.4 | 20 21 38.1 | 16 41 07.5 |
| 45... | 35 15 51.8 | 30 40 55.4 | 26 20 27.6 | 22 12 27.6 | 18 14 56.0 |
| 50... | 37 27 13.4 | 32 43 56.7 | 28 12 31.2 | 23 51 31.2 | 19 39 26.5 |
| 55... | 39 19 21.7 | 34 30 09.7 | 29 50 15.2 | 25 18 40.4 | 20 54 20.5 |
| 60... | 40 53 36.2 | 36 00 18.8 | 31 13 57.1 | 26 33 54.2 | 21 59 26.0 |
| 65... | 42 11 10.8 | 37 15 08.5 | 32 23 57.7 | 27 37 16.1 | 22 54 35.3 |
| 70... | 43 13 09.0 | 38 15 20.3 | 33 20 38.8 | 28 28 52.5 | 23 39 44.5 |
| 75... | 44 00 25.3 | 39 01 30.2 | 34 04 20.6 | 29 08 50.7 | 24 14 51.7 |
| 80... | 44 33 41.2 | 39 34 07.3 | 34 35 20.3 | 29 37 18.0 | 24 39 56.5 |
| 85... | 44 53 26.8 | 39 53 32.9 | 34 53 50.8 | 29 54 19.8 | 24 54 59.1 |
| 90... | 45 00 00.0 | 40 00 00.0 | 35 00 00.0 | 30 00 00.0 | 25 00 00.0 |
|       | Lat. 70°.  | Lat. 75°.  | Lat. 80°.  | Lat. 85°.  | Lat. 90°.  |
| 0...  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  | 0 00 00.0  |
| 5...  | 1 49 01.0  | 1 20 16.1  | 0 52 49.6  | 0 28 12.8  | 0 00 00.0  |
| 10... | 3 36 59.2  | 2 39 50.4  | 1 45 13.6  | 0 52 13.4  | 0 00 00.0  |
| 15... | 5 22 53.5  | 3 58 01.7  | 2 36 46.7  | 1 17 49.8  | 0 00 00.0  |
| 20... | 7 05 45.5  | 5 14 10.3  | 3 27 04.2  | 1 42 50.2  | 0 00 00.0  |
| 25... | 8 44 41.0  | 6 27 38.4  | 4 15 42.3  | 2 07 03.0  | 0 00 00.0  |
| 30... | 10 18 50.8 | 7 37 50.7  | 5 02 18.1  | 2 30 17.2  | 0 00 00.0  |
| 35... | 11 47 31.1 | 8 44 14.6  | 5 46 30.3  | 2 52 22.0  | 0 00 00.0  |
| 40... | 13 10 04.2 | 9 46 20.7  | 6 27 58.9  | 3 13 07.4  | 0 00 00.0  |
| 45... | 14 25 57.9 | 10 43 42.9 | 7 06 25.5  | 3 32 24.1  | 0 00 00.0  |
| 50... | 15 34 45.8 | 11 35 58.1 | 7 41 33.5  | 3 50 03.3  | 0 00 00.0  |
| 55... | 16 36 06.4 | 12 22 45.6 | 8 13 08.0  | 4 05 57.1  | 0 00 00.0  |
| 60... | 17 29 42.9 | 13 03 51.5 | 8 40 55.9  | 4 19 58.3  | 0 00 00.0  |
| 65... | 18 15 22.0 | 13 38 59.0 | 9 04 46.1  | 4 32 00.9  | 0 00 00.0  |
| 70... | 18 52 54.2 | 14 07 57.8 | 9 24 29.0  | 4 41 59.5  | 0 00 00.0  |
| 75... | 19 22 12.2 | 14 30 39.0 | 9 39 56.9  | 4 49 49.6  | 0 00 00.0  |
| 80... | 19 43 11.1 | 14 46 55.8 | 9 51 03.9  | 4 55 27.9  | 0 00 00.0  |
| 85... | 19 55 47.6 | 14 56 43.7 | 9 57 45.8  | 4 58 51.8  | 0 00 00.0  |
| 90... | 20 00 00.0 | 15 00 00.0 | 10 00 00.0 | 5 00 00.0  | 0 00 00.0  |





LAMBERT'S AZIMUTHAL EQUIVALENT PROJECTION—CENTER ON THE EQUATOR—Continued.

Rectangular coordinates in units of the earth's radius,

| Long. | Lat. 0°.  |          | Lat. 5°.  |          | Lat. 10°. |          | Lat. 15°. |          |
|-------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
|       | x         | y        | x         | y        | x         | y        | x         | y        |
| 0     | 0         | 0        | 0         | 0.087239 | 0         | 0.174311 | 0         | 0.261052 |
| 5     | 0.087239  | 0        | 0.086991  | 0.087323 | 0.086241  | 0.174476 | 0.084992  | 0.261297 |
| 10    | 0.174311  | 0        | 0.173812  | 0.087571 | 0.172318  | 0.174972 | 0.169813  | 0.262532 |
| 15    | 0.261052  | 0        | 0.260392  | 0.087996 | 0.258051  | 0.175804 | 0.254295  | 0.263265 |
| 20    | 0.347296  | 0        | 0.346294  | 0.088582 | 0.343285  | 0.176979 | 0.338266  | 0.265002 |
| 25    | 0.432879  | 0        | 0.431623  | 0.089353 | 0.427551  | 0.178510 | 0.421558  | 0.267277 |
| 30    | 0.517638  | 0        | 0.516124  | 0.090310 | 0.511581  | 0.180411 | 0.504001  | 0.270063 |
| 35    | 0.601412  | 0        | 0.599638  | 0.091461 | 0.594311  | 0.182701 | 0.585428  | 0.273485 |
| 40    | 0.684040  | 0        | 0.682000  | 0.092822 | 0.675879  | 0.186404 | 0.665570  | 0.277488 |
| 45    | 0.765367  | 0        | 0.763056  | 0.094411 | 0.756122  | 0.188550 | 0.744500  | 0.282142 |
| 50    | 0.845237  | 0        | 0.842647  | 0.096237 | 0.834881  | 0.192172 | 0.821934  | 0.287499 |
| 55    | 0.923497  | 0        | 0.920622  | 0.098326 | 0.911995  | 0.196312 | 0.897621  | 0.293617 |
| 60    | 1.000000  | 0        | 0.996827  | 0.100703 | 0.987311  | 0.201021 | 0.971458  | 0.300570 |
| 65    | 1.074599  | 0        | 1.071115  | 0.103398 | 1.06070   | 0.206359 | 1.043276  | 0.308444 |
| 70    | 1.147153  | 0        | 1.143342  | 0.106449 | 1.131919  | 0.212397 | 1.112907  | 0.317341 |
| 75    | 1.217523  | 0        | 1.213365  | 0.109901 | 1.200903  | 0.219222 | 1.180179  | 0.327383 |
| 80    | 1.285375  | 0        | 1.281044  | 0.113846 | 1.267469  | 0.226837 | 1.244912  | 0.338721 |
| 85    | 1.351180  | 0        | 1.346245  | 0.118231 | 1.331637  | 0.235465 | 1.306926  | 0.351527 |
| 90    | 1.414214  | 0        | 1.408832  | 0.123257 | 1.392729  | 0.245576 | 1.366025  | 0.366025 |
|       | Lat. 15°. |          | Lat. 20°. |          | Lat. 25°. |          | Lat. 30°. |          |
| 0     | 0         | 0.261052 | 0         | 0.347296 | 0         | 0.432879 | 0         | 0.517638 |
| 5     | 0.084992  | 0.261297 | 0.083240  | 0.347617 | 0.080981  | 0.433272 | 0.078211  | 0.518096 |
| 10    | 0.169813  | 0.262032 | 0.166306  | 0.348581 | 0.161785  | 0.434451 | 0.156241  | 0.519473 |
| 15    | 0.254295  | 0.263265 | 0.249026  | 0.350199 | 0.242235  | 0.436429 | 0.233908  | 0.521780 |
| 20    | 0.338266  | 0.265002 | 0.331220  | 0.352484 | 0.322153  | 0.439222 | 0.311030  | 0.525038 |
| 25    | 0.421558  | 0.267277 | 0.412733  | 0.355457 | 0.401363  | 0.442855 | 0.387426  | 0.529273 |
| 30    | 0.504001  | 0.270063 | 0.493374  | 0.359147 | 0.479884  | 0.447361 | 0.462910  | 0.534523 |
| 35    | 0.585428  | 0.273485 | 0.572975  | 0.363599 | 0.556939  | 0.452782 | 0.537297  | 0.540632 |
| 40    | 0.665570  | 0.277488 | 0.651364  | 0.368827 | 0.632946  | 0.459168 | 0.610397  | 0.548258 |
| 45    | 0.744500  | 0.282142 | 0.728365  | 0.374912 | 0.706006  | 0.465622 | 0.682022  | 0.556808 |
| 50    | 0.821934  | 0.287499 | 0.803803  | 0.381911 | 0.780484  | 0.475097 | 0.751972  | 0.566744 |
| 55    | 0.897621  | 0.293617 | 0.877502  | 0.389897 | 0.851841  | 0.484892 | 0.820046  | 0.577981 |
| 60    | 0.971458  | 0.300570 | 0.949282  | 0.398961 | 0.920800  | 0.495801 | 0.886036  | 0.590691 |
| 65    | 1.043276  | 0.308444 | 1.018962  | 0.409211 | 0.987761  | 0.508217 | 0.949722  | 0.605097 |
| 70    | 1.112907  | 0.317341 | 1.086352  | 0.420776 | 1.052313  | 0.522193 | 1.010871  | 0.621083 |
| 75    | 1.180179  | 0.327383 | 1.151257  | 0.433805 | 1.114235  | 0.537905 | 1.069235  | 0.639100 |
| 80    | 1.244912  | 0.338721 | 1.218472  | 0.448481 | 1.173287  | 0.555553 | 1.124542  | 0.659270 |
| 85    | 1.306926  | 0.351527 | 1.272775  | 0.465022 | 1.229210  | 0.575380 | 1.176491  | 0.681843 |
| 90    | 1.366025  | 0.366025 | 1.328926  | 0.483660 | 1.281718  | 0.597672 | 1.224745  | 0.707107 |

$$x = \rho \sin \alpha, \quad y = \rho \cos \alpha.$$



**LAMBERT'S AZIMUTHAL EQUIVALENT PROJECTION—CENTER  
ON THE EQUATOR—Continued.**
*Rectangular coordinates in units of the earth's radius—Continued.*

| Long. | Lat. 30°. |          | Lat. 35°. |          | Lat. 40°. |          | Lat. 45°. |          |
|-------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
|       | <i>x</i>  | <i>y</i> | <i>x</i>  | <i>y</i> | <i>x</i>  | <i>y</i> | <i>x</i>  | <i>y</i> |
| 0     | 0         | 0.517638 | 0         | 0.601412 | 0         | 0.684040 | 0         | 0.765367 |
| 5     | 0.078211  | 0.518096 | 0.074923  | 0.601928 | 0.071109  | 0.684605 | 0.066759  | 0.765971 |
| 10    | 0.156241  | 0.519473 | 0.149660  | 0.603479 | 0.142028  | 0.686305 | 0.133325  | 0.767787 |
| 15    | 0.233908  | 0.521780 | 0.224026  | 0.606079 | 0.212568  | 0.689152 | 0.196504  | 0.770825 |
| 20    | 0.311030  | 0.525038 | 0.297835  | 0.609748 | 0.282538  | 0.693167 | 0.265103  | 0.775110 |
| 25    | 0.387426  | 0.529273 | 0.370897  | 0.614515 | 0.351743  | 0.698379 | 0.329244  | 0.779058 |
| 30    | 0.462910  | 0.534523 | 0.443023  | 0.620417 | 0.419990  | 0.704826 | 0.393765  | 0.783751 |
| 35    | 0.537297  | 0.540832 | 0.514021  | 0.627504 | 0.487078  | 0.712559 | 0.456425  | 0.789533 |
| 40    | 0.610397  | 0.548258 | 0.583694  | 0.635835 | 0.552306  | 0.721635 | 0.517691  | 0.805335 |
| 45    | 0.682022  | 0.556868 | 0.651842  | 0.645482 | 0.616961  | 0.732126 | 0.577350  | 0.816497 |
| 50    | 0.751972  | 0.566744 | 0.718257  | 0.656527 | 0.679328  | 0.744114 | 0.635176  | 0.829164 |
| 55    | 0.820046  | 0.577981 | 0.782723  | 0.669068 | 0.739682  | 0.757694 | 0.690934  | 0.843745 |
| 60    | 0.886036  | 0.590691 | 0.844341  | 0.682676 | 0.797784  | 0.772979 | 0.744377  | 0.859533 |
| 65    | 0.949772  | 0.605007 | 0.904904  | 0.699123 | 0.853380  | 0.790097 | 0.795240  | 0.877451 |
| 70    | 1.010871  | 0.621083 | 0.962126  | 0.716924 | 0.906201  | 0.809194 | 0.843242  | 0.897359 |
| 75    | 1.069235  | 0.639100 | 1.016411  | 0.736805 | 0.955952  | 0.830435 | 0.888073  | 0.919401 |
| 80    | 1.124542  | 0.659270 | 1.067459  | 0.758974 | 1.002308  | 0.854010 | 0.929400  | 0.943738 |
| 85    | 1.176491  | 0.681843 | 1.114934  | 0.783667 | 1.044910  | 0.880132 | 0.966848  | 0.970541 |
| 90    | 1.224745  | 0.707107 | 1.158456  | 0.811160 | 1.083351  | 0.909039 | 1.000000  | 1.000000 |
|       |           |          |           |          |           |          |           |          |
|       | Lat. 45°. |          | Lat. 50°. |          | Lat. 55°. |          | Lat. 60°. |          |
| 0     | 0         | 0.765367 | 0         | 0.845237 | 0         | 0.923497 | 0         | 1.000000 |
| 5     | 0.066759  | 0.765971 | 0.061860  | 0.845866 | 0.056398  | 0.924139 | 0.050351  | 1.000635 |
| 10    | 0.133325  | 0.767787 | 0.123525  | 0.847760 | 0.112600  | 0.926064 | 0.100511  | 1.002542 |
| 15    | 0.199504  | 0.770825 | 0.184800  | 0.850929 | 0.168412  | 0.929296 | 0.149939  | 1.005727 |
| 20    | 0.265103  | 0.775110 | 0.245487  | 0.855339 | 0.223635  | 0.933818 | 0.199480  | 1.010205 |
| 25    | 0.329244  | 0.779058 | 0.305387  | 0.861169 | 0.278071  | 0.939682 | 0.247901  | 1.015991 |
| 30    | 0.393765  | 0.783751 | 0.364296  | 0.868302 | 0.331516  | 0.946908 | 0.298345  | 1.023106 |
| 35    | 0.456425  | 0.789533 | 0.422007  | 0.876829 | 0.383762  | 0.955528 | 0.341338  | 1.030750 |
| 40    | 0.517691  | 0.805335 | 0.478307  | 0.886800 | 0.434595  | 0.965566 | 0.386490  | 1.041432 |
| 45    | 0.577350  | 0.816497 | 0.532976  | 0.898275 | 0.483798  | 0.977129 | 0.429767  | 1.052708 |
| 50    | 0.635176  | 0.829164 | 0.585785  | 0.911320 | 0.531139  | 0.990210 | 0.471219  | 1.065441 |
| 55    | 0.690934  | 0.843475 | 0.636495  | 0.926012 | 0.576381  | 1.004891 | 0.510618  | 1.079673 |
| 60    | 0.744377  | 0.859533 | 0.684853  | 0.942439 | 0.619275  | 1.021236 | 0.547728  | 1.095445 |
| 65    | 0.795240  | 0.877451 | 0.730590  | 0.960693 | 0.658535  | 1.039318 | 0.582232  | 1.112802 |
| 70    | 0.843242  | 0.897359 | 0.773421  | 0.980881 | 0.696939  | 1.059210 | 0.614031  | 1.131788 |
| 75    | 0.888073  | 0.919401 | 0.813035  | 1.003117 | 0.731128  | 1.080994 | 0.642692  | 1.152445 |
| 80    | 0.929400  | 0.943738 | 0.849094  | 1.027521 | 0.761799  | 1.104745 | 0.667970  | 1.174806 |
| 85    | 0.966848  | 0.970541 | 0.881231  | 1.054223 | 0.788602  | 1.130542 | 0.689552  | 1.198901 |
| 90    | 1.000000  | 1.000000 | 0.909039  | 1.083351 | 0.811160  | 1.158456 | 0.707107  | 1.224745 |

$$x = \rho \sin \alpha, \quad y = \rho \cos \alpha.$$

LAMBERT'S AZIMUTHAL EQUIVALENT PROJECTION—CENTER ON THE EQUATOR—Continued.

Rectangular coordinates in units of the earth's radius—Continued.

| Long. | Lat. 60°. |          | Lat. 65°. |          | Lat. 70°. |          | Lat. 75°. |          |
|-------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
|       | x         | y        | x         | y        | x         | y        | x         | y        |
| 0     | 0         | 1.000000 | 0         | 1.074599 | 0         | 1.147153 | 0         | 1.217523 |
| 5     | 0.050351  | 1.000635 | 0.043698  | 1.075207 | 0.036408  | 1.147710 | 0.028444  | 1.218000 |
| 10    | 0.100511  | 1.002542 | 0.087211  | 1.077032 | 0.072644  | 1.149380 | 0.056739  | 1.219429 |
| 15    | 0.149639  | 1.005727 | 0.130054  | 1.080079 | 0.108837  | 1.152166 | 0.084733  | 1.221810 |
| 20    | 0.199480  | 1.010205 | 0.172940  | 1.084356 | 0.143914  | 1.156072 | 0.112277  | 1.225142 |
| 25    | 0.247901  | 1.015991 | 0.214781  | 1.089874 | 0.178601  | 1.161099 | 0.139220  | 1.229422 |
| 30    | 0.295345  | 1.023106 | 0.255687  | 1.096644 | 0.212423  | 1.167253 | 0.165411  | 1.234664 |
| 35    | 0.341338  | 1.030750 | 0.295462  | 1.104684 | 0.245202  | 1.174540 | 0.190699  | 1.240809 |
| 40    | 0.386490  | 1.041432 | 0.333910  | 1.114008 | 0.276761  | 1.182932 | 0.214932  | 1.247906 |
| 45    | 0.429767  | 1.052708 | 0.370826  | 1.124640 | 0.306915  | 1.192524 | 0.237959  | 1.255925 |
| 50    | 0.471219  | 1.065441 | 0.408007  | 1.136597 | 0.334709  | 1.203229 | 0.259626  | 1.264857 |
| 55    | 0.510618  | 1.079673 | 0.439244  | 1.149898 | 0.362271  | 1.215076 | 0.279782  | 1.274684 |
| 60    | 0.547723  | 1.095445 | 0.470291  | 1.164563 | 0.387095  | 1.228063 | 0.298274  | 1.285385 |
| 65    | 0.582282  | 1.112802 | 0.498047  | 1.180610 | 0.409756  | 1.242180 | 0.314953  | 1.296935 |
| 70    | 0.614031  | 1.131788 | 0.524968  | 1.198048 | 0.430061  | 1.257414 | 0.329669  | 1.309303 |
| 75    | 0.642692  | 1.152445 | 0.548109  | 1.216887 | 0.447806  | 1.273745 | 0.342275  | 1.322949 |
| 80    | 0.668790  | 1.174806 | 0.568115  | 1.237122 | 0.462796  | 1.291138 | 0.352628  | 1.336326 |
| 85    | 0.689552  | 1.198901 | 0.584727  | 1.258741 | 0.474823  | 1.309551 | 0.360588  | 1.350274 |
| 90    | 0.707107  | 1.224745 | 0.597673  | 1.281713 | 0.483690  | 1.328926 | 0.366025  | 1.366025 |

  

| Long. | Lat. 75°. |          | Lat. 80°. |          | Lat. 85°. |          | Lat. 90°. |          |
|-------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
|       | x         | y        | x         | y        | x         | y        | x         | y        |
| 0     | 0         | 1.217523 | 0         | 1.285575 | 0         | 1.351180 | 0         | 1.414214 |
| 5     | 0.028444  | 1.218000 | 0.019762  | 1.285937 | 0.010305  | 1.351387 | 0         | 1.414214 |
| 10    | 0.056739  | 1.219429 | 0.039407  | 1.287022 | 0.020542  | 1.352150 | 0         | 1.414214 |
| 15    | 0.084733  | 1.221810 | 0.058818  | 1.288828 | 0.030638  | 1.353030 | 0         | 1.414214 |
| 20    | 0.112277  | 1.225142 | 0.077877  | 1.291350 | 0.040529  | 1.354459 | 0         | 1.414214 |
| 25    | 0.139220  | 1.229422 | 0.096471  | 1.294579 | 0.050147  | 1.356283 | 0         | 1.414214 |
| 30    | 0.165411  | 1.234664 | 0.114481  | 1.298509 | 0.059427  | 1.358496 | 0         | 1.414214 |
| 35    | 0.190699  | 1.240809 | 0.131794  | 1.303128 | 0.068301  | 1.361083 | 0         | 1.414214 |
| 40    | 0.214932  | 1.247906 | 0.148297  | 1.308420 | 0.076708  | 1.364033 | 0         | 1.414214 |
| 45    | 0.237959  | 1.255925 | 0.163878  | 1.314370 | 0.084588  | 1.367329 | 0         | 1.414214 |
| 50    | 0.259626  | 1.264857 | 0.178427  | 1.320956 | 0.091882  | 1.370953 | 0         | 1.414214 |
| 55    | 0.279782  | 1.274684 | 0.191837  | 1.328156 | 0.098534  | 1.374885 | 0         | 1.414214 |
| 60    | 0.298274  | 1.285385 | 0.204003  | 1.335940 | 0.104491  | 1.379104 | 0         | 1.414214 |
| 65    | 0.314953  | 1.296935 | 0.214824  | 1.344276 | 0.109706  | 1.383581 | 0         | 1.414214 |
| 70    | 0.329669  | 1.309303 | 0.224204  | 1.353126 | 0.114135  | 1.388292 | 0         | 1.414214 |
| 75    | 0.342275  | 1.322949 | 0.232051  | 1.362449 | 0.117736  | 1.393206 | 0         | 1.414214 |
| 80    | 0.352628  | 1.336326 | 0.238279  | 1.372193 | 0.120476  | 1.398291 | 0         | 1.414214 |
| 85    | 0.360588  | 1.350274 | 0.242811  | 1.382308 | 0.122324  | 1.403512 | 0         | 1.414214 |
| 90    | 0.366025  | 1.366025 | 0.245576  | 1.392729 | 0.123257  | 1.408832 | 0         | 1.414214 |

$$x = \rho \sin \alpha, y = \rho \cos \alpha.$$

## APPENDIX.

After the manuscript of this publication had been sent to the printer it was suggested that another kind of latitude might be of use in some cartographic and geodetic applications. This idea was accordingly developed and it was decided to add it as an appendix so that no change of the earlier text would be necessary.

### DEFINITION OF RECTIFYING LATITUDE.

A sixth kind of latitude that is of some use in applications may be defined in the following way: If a sphere is determined such that the length of a great circle upon it is equal in length to a meridian upon the earth, we may calculate the latitudes upon this sphere such that the arcs of the meridian upon it are equal to the corresponding arcs of the meridian upon the earth.

If  $M$  represents an arc of a meridian on the earth, we have

$$dM = \frac{a(1 - \epsilon^2)d\varphi}{(1 - \epsilon^2 \sin^2 \varphi)^{3/2}}$$

The development of this formula is given in full in "General Theory of Polyconic Projections," United States Coast and Geodetic Survey Special Publication No. 57, pages 9 and 10.

If  $\omega$  denotes the latitude upon the sphere of radius  $r$ , the differential element of the meridian will be given in the form

$$dm = r d\omega.$$

The arc of this meridian from the equator to latitude  $\omega$  is therefore given in the form

$$m = r\omega.$$

On the earth the arc of the meridian from the equator to latitude  $\varphi$  becomes

$$M = a(1 - \epsilon^2) \int_0^\varphi \frac{d\varphi}{(1 - \epsilon^2 \sin^2 \varphi)^{3/2}}$$

If the arc on the sphere is to be equal to this arc on the earth, we must have as the definition of  $\omega$

$$r\omega = a(1 - \epsilon^2) \int_0^\varphi \frac{d\varphi}{(1 - \epsilon^2 \sin^2 \varphi)^{3/2}}$$

**DEVELOPMENT OF  $\varphi - \omega$  IN TERMS OF  $\varphi$ .**

In order to develop this expression in a Fourier series we must first set  $\sin^2 \varphi = \frac{1}{2} (1 - \cos 2\varphi)$  and we get

$$\begin{aligned} (1 - \epsilon^2 \sin^2 \varphi)^{-3/2} &= \left[ \frac{1}{2} (2 - \epsilon^2 + \epsilon^2 \cos 2\varphi) \right]^{-3/2} \\ &= \left[ \frac{1}{4} (4 - 2\epsilon^2 + \epsilon^2 e^{2i\varphi} + \epsilon^2 e^{-2i\varphi}) \right]^{-3/2} \\ &= \frac{8}{[1 + (1 - \epsilon^2)^{1/2}]^3} \left\{ \frac{4 - 2\epsilon^2}{[1 + (1 - \epsilon^2)^{1/2}]^2} \right. \\ &\quad \left. + \frac{\epsilon^2}{[1 + (1 - \epsilon^2)^{1/2}]^2} (e^{2i\varphi} + e^{-2i\varphi}) \right\}^{-3/2} \\ &= \frac{8}{[1 + (1 - \epsilon^2)^{1/2}]^3} \{ 1 + n^2 + ne^{2i\varphi} + ne^{-2i\varphi} \}^{-3/2} \end{aligned}$$

in which

$$n = \frac{1 - (1 - \epsilon^2)^{1/2}}{1 + (1 - \epsilon^2)^{1/2}}$$

Finally we get

$$(1 - \epsilon^2 \sin^2 \varphi)^{-3/2} = \frac{8}{[1 + (1 - \epsilon^2)^{1/2}]^3} (1 + ne^{2i\varphi})^{-3/2} (1 + ne^{-2i\varphi})^{-3/2}$$

Since  $n$  is less than unity, the quantities in the last two parentheses in the right-hand member may be developed by the binomial theorem into convergent series, and in this way we get

$$(1 + ne^{2i\varphi})^{-3/2} = 1 - \frac{3}{2} ne^{2i\varphi} + \frac{15}{8} n^2 e^{4i\varphi} - \frac{35}{16} n^3 e^{6i\varphi} + \frac{315}{128} n^4 e^{8i\varphi} - \dots$$

and

$$\begin{aligned} (1 + ne^{-2i\varphi})^{-3/2} &= 1 - \frac{3}{2} ne^{-2i\varphi} + \frac{15}{8} n^2 e^{-4i\varphi} - \frac{35}{16} n^3 e^{-6i\varphi} \\ &\quad + \frac{315}{128} n^4 e^{-8i\varphi} - \dots \end{aligned}$$

If we multiply these two series and replace  $e^{2is\varphi} + e^{-2is\varphi}$  by its equivalent  $2\cos 2s\varphi$ , we get

$$\begin{aligned} (1 + ne^{2i\varphi})^{-1/2}(1 + ne^{-2i\varphi})^{-1/2} = & \left(1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots\right) \\ & - \left(3n + \frac{45}{8}n^3 + \dots\right) \cos 2\varphi + \left(\frac{15}{4}n^2 \right. \\ & \left. + \frac{105}{16}n^4 + \dots\right) \cos 4\varphi - \left(\frac{35}{8}n^3 + \dots\right) \cos 6\varphi \\ & + \left(\frac{315}{64}n^4 + \dots\right) \cos 8\varphi - \dots \end{aligned}$$

From the definition of  $n$  we obtain the values

$$1 - \epsilon^2 = \left(\frac{1-n}{1+n}\right)^2$$

and

$$\frac{8}{[1 + (1 - \epsilon^2)^{1/2}]^2} = (1+n)^3.$$

By substituting these values in the original integral we get

$$\begin{aligned} r\omega = a(1-n)(1-n^2) \int_0^\varphi & \left[ \left(1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots\right) \right. \\ & - \left(3n + \frac{45}{8}n^3 + \dots\right) \cos 2\varphi + \left(\frac{15}{4}n^2 + \frac{105}{16}n^4 \right. \\ & \left. + \dots\right) \cos 4\varphi - \left(\frac{35}{8}n^3 + \dots\right) \cos 6\varphi \\ & \left. + \left(\frac{315}{64}n^4 + \dots\right) \cos 8\varphi - \dots \right] d\varphi, \end{aligned}$$

or after integration

$$\begin{aligned} r\omega = a(1-n)(1-n^2) & \left[ \left(1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots\right) \varphi - \left(\frac{3}{2}n \right. \right. \\ & \left. + \frac{45}{16}n^3 + \dots\right) \sin 2\varphi + \left(\frac{15}{16}n^2 + \frac{105}{64}n^4 + \dots\right) \sin 4\varphi \\ & \left. - \left(\frac{35}{48}n^3 + \dots\right) \sin 6\varphi + \left(\frac{315}{512}n^4 + \dots\right) \sin 8\varphi - \dots \right]. \end{aligned}$$

The value of  $r$  may now be determined by the condition that  $\omega$  and  $\varphi$  are to become  $\frac{\pi}{2}$  at one and the same time. This condition gives for  $r$  the value

$$r = a(1-n)(1-n^2) \left( 1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots \right).$$

With this value of  $r$  we get

$$\begin{aligned} \varphi - \omega = & \frac{\frac{3}{2}n + \frac{45}{16}n^3 + \dots}{1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots} \sin 2\varphi \\ & - \frac{\frac{15}{16}n^2 + \frac{105}{64}n^4 + \dots}{1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots} \sin 4\varphi \\ & + \frac{\frac{35}{48}n^3 + \dots}{1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots} \sin 6\varphi \\ & - \frac{\frac{315}{512}n^4 + \dots}{1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots} \sin 8\varphi + \dots \end{aligned}$$

or approximately in terms of  $n$  up to the fourth order inclusive,

$$\begin{aligned} \varphi - \omega = & \left( \frac{3}{2}n - \frac{9}{16}n^3 \right) \sin 2\varphi - \left( \frac{15}{16}n^2 - \frac{15}{32}n^4 \right) \sin 4\varphi + \frac{35}{48}n^3 \sin 6\varphi \\ & - \frac{315}{512}n^4 \sin 8\varphi. \end{aligned}$$

The latitude  $\omega$  may be called the rectifying latitude, since it can be used in the computation of arcs of the meridian. The length of the meridian on the earth from the equator to a given latitude  $\varphi_1$  is given by the formula

$$M = r\omega_1$$

in which  $\omega_1$  is the rectifying latitude corresponding to the geodetic latitude  $\varphi_1$ . The meridional arc between the latitudes  $\varphi_1$  and  $\varphi_2$  is accordingly given by the expression

$$M = r(\omega_2 - \omega_1).$$

The radius of curvature in the meridian ( $\rho_m$ ) is equal to the value of the expression  $r \frac{d\omega}{d\varphi}$ . Accordingly we get as the approximation for this quantity

$$\rho_m = r - r \left( 3n - \frac{9}{8}n^3 \right) \cos 2\varphi + r \left( \frac{15}{4}n^2 - \frac{15}{8}n^4 \right) \cos 4\varphi \\ - \frac{35}{8}rn^3 \cos 6\varphi + \frac{315}{64}rn^4 \cos 8\varphi.$$

DEVELOPMENT OF  $\varphi - \omega$  IN TERMS OF  $\omega$ .

$$\text{If } f(\omega) = \left( \frac{3}{2}n - \frac{9}{16}n^3 \right) \sin 2\omega - \left( \frac{15}{16}n^2 - \frac{15}{32}n^4 \right) \sin 4\omega \\ + \frac{35}{48}n^3 \sin 6\omega - \frac{315}{512}n^4 \sin 8\omega,$$

we shall have by application of Lagrange's development

$$\varphi = \omega + \frac{1}{1!}f(\omega) + \frac{1}{2!} \frac{d}{d\omega} [f(\omega)]^2 + \frac{1}{3!} \frac{d^2}{d\omega^2} [f(\omega)]^3 \\ + \frac{1}{4!} \frac{d^3}{d\omega^3} [f(\omega)]^4 + \dots$$

By raising to the required power and reducing by aid of the reduction table on page 88, we get the approximations

$$[f(\omega)]^2 = \frac{9}{8}n^2 - \frac{207}{512}n^4 - \frac{45}{32}n^3 \cos 2\omega - \left( \frac{9}{8}n^2 - \frac{31}{16}n^4 \right) \cos 4\omega \\ + \frac{45}{32}n^3 \cos 6\omega - \frac{785}{512}n^4 \cos 8\omega,$$

$$[f(\omega)]^3 = \frac{81}{32}n^3 \sin 2\omega - \frac{405}{128}n^4 \sin 4\omega - \frac{27}{32}n^3 \sin 6\omega \\ + \frac{405}{256}n^4 \sin 8\omega,$$

$$[f(\omega)]^4 = \frac{243}{128}n^4 - \frac{81}{32}n^4 \cos 4\omega + \frac{81}{128}n^4 \cos 8\omega.$$

By differentiating these expressions we obtain the values

$$\frac{d}{d\omega} [f(\omega)]^2 = \frac{45}{16}n^3 \sin 2\omega + \left( \frac{9}{2} - \frac{31}{4}n^4 \right) \sin 4\omega \\ - \frac{135}{16}n^3 \sin 6\omega + \frac{785}{64}n^4 \sin 8\omega,$$

$$\frac{d^2}{d\omega^2}[f(\omega)]^3 = -\frac{81}{8}n^3 \sin 2\omega + \frac{405}{8}n^4 \sin 4\omega + \frac{243}{8}n^3 \sin 6\omega \\ - \frac{405}{4}n^4 \sin 8\omega,$$

$$\frac{d^3}{d\omega^3}[f(\omega)]^4 = -162n^4 \sin 4\omega + 324n^4 \sin 8\omega.$$

By substituting these values in the Lagrange development, we get

$$\varphi = \omega + \left(\frac{3}{2}n - \frac{9}{16}n^3\right) \sin 2\omega - \left(\frac{15}{16}n^2 - \frac{15}{32}n^4\right) \sin 4\omega \\ + \frac{35}{48}n^3 \sin 6\omega - \frac{315}{512}n^4 \sin 8\omega + \frac{45}{32}n^3 \sin 2\omega \\ + \left(\frac{9}{4}n^2 - \frac{31}{8}n^4\right) \sin 4\omega - \frac{135}{32}n^3 \sin 6\omega + \frac{785}{128}n^4 \sin 8\omega \\ - \frac{27}{16}n^3 \sin 2\omega + \frac{135}{16}n^4 \sin 4\omega + \frac{81}{16}n^3 \sin 6\omega \\ - \frac{135}{8}n^4 \sin 8\omega - \frac{27}{4}n^4 \sin 4\omega + \frac{27}{2}n^4 \sin 8\omega.$$

By collecting similar terms we obtain the approximation

$$\varphi - \omega = \left(\frac{3}{2}n - \frac{27}{32}n^3\right) \sin 2\omega + \left(\frac{21}{16}n^2 - \frac{55}{32}n^4\right) \sin 4\omega \\ + \frac{151}{96}n^3 \sin 6\omega + \frac{1097}{512}n^4 \sin 8\omega.$$

#### TABULATION OF THE DEVELOPMENT.

For convenience of reference we shall give the general approximations in terms of  $n$  and then the numerical values of the coefficients for the Clarke Spheroid of 1866.

$$\varphi - \omega = \left(\frac{3}{2}n - \frac{9}{16}n^3\right) \sin 2\varphi - \left(\frac{15}{16}n^2 - \frac{15}{32}n^4\right) \sin 4\varphi \\ + \frac{35}{48}n^3 \sin 6\varphi - \frac{315}{512}n^4 \sin 8\varphi.$$

$$\log n = 7.22991610 - 10.$$

$$\varphi - \omega = 525^{\circ}3298 \sin 2\varphi - 0^{\circ}5575 \sin 4\varphi + 0^{\circ}0007 \sin 6\varphi.$$

$$\varphi - \omega = [2.7204320] \sin 2\varphi - [9.74623 - 10] \sin 4\varphi \\ + [6.867 - 10] \sin 6\varphi.$$



$$\varphi - \omega = \left( \frac{3}{2}n - \frac{27}{32}n^3 \right) \sin 2\omega + \left( \frac{21}{16}n^2 - \frac{55}{32}n^4 \right) \sin 4\omega \\ + \frac{151}{96}n^3 \sin 6\omega + \frac{1097}{512}n^4 \sin 8\omega.$$

$$\varphi - \omega = 525.3295 \sin 2\omega + 0.7805 \sin 4\omega + 0.0016 \sin 6\omega.$$

$$\varphi - \omega = [2.7204318] \sin 2\omega + [9.89236 - 10] \sin 4\omega \\ + [7.201 - 10] \sin 6\omega.$$

$$r = a(1-n)(1-n^2) \left( 1 + \frac{9}{4}n^2 + \frac{225}{64}n^4 + \dots \right)$$

$$\log r = 6.80396212.$$

LATITUDE TRANSFORMATION.

*Geodetic to rectifying.*

| Geodetic latitude.<br>φ | Geodetic minus rectifying.<br>φ-ω | Rectifying latitude.<br>ω | Geodetic latitude.<br>φ | Geodetic minus rectifying.<br>φ-ω | Rectifying latitude.<br>ω |
|-------------------------|-----------------------------------|---------------------------|-------------------------|-----------------------------------|---------------------------|
| 0 00                    | 0 00.000                          | 0 00 00.00                | 22 30                   | 6 10.907                          | 22 23 49.09               |
| 0 30                    | 0 09.149                          | 0 29 50.85                | 23 00                   | 6 17.334                          | 22 53 42.67               |
| 1 00                    | 0 18.295                          | 0 59 41.70                | 23 30                   | 6 23.646                          | 23 23 36.35               |
| 1 30                    | 0 27.435                          | 1 29 32.56                | 24 00                   | 6 29.842                          | 23 53 30.16               |
| 2 00                    | 0 36.568                          | 1 59 23.43                | 24 30                   | 6 35.920                          | 24 23 24.08               |
| 2 30                    | 0 45.689                          | 2 29 14.31                | 25 00                   | 6 41.877                          | 24 53 18.12               |
| 3 00                    | 0 54.796                          | 2 59 05.20                | 25 30                   | 6 47.713                          | 25 23 12.29               |
| 3 30                    | 1 03.887                          | 3 28 56.11                | 26 00                   | 6 53.425                          | 25 53 06.58               |
| 4 00                    | 1 12.958                          | 3 58 47.04                | 26 30                   | 6 59.011                          | 26 23 00.99               |
| 4 30                    | 1 22.008                          | 4 28 37.99                | 27 00                   | 7 04.471                          | 26 52 55.53               |
| 5 00                    | 1 31.032                          | 4 58 28.97                | 27 30                   | 7 09.801                          | 27 22 50.20               |
| 5 30                    | 1 40.029                          | 5 28 19.97                | 28 00                   | 7 15.001                          | 27 52 45.00               |
| 6 00                    | 1 48.996                          | 5 58 11.00                | 28 30                   | 7 20.069                          | 28 22 39.93               |
| 6 30                    | 1 57.930                          | 6 28 02.07                | 29 00                   | 7 25.004                          | 28 52 35.00               |
| 7 00                    | 2 06.828                          | 6 57 53.17                | 29 30                   | 7 29.803                          | 29 22 30.20               |
| 7 30                    | 2 15.687                          | 7 27 44.31                | 30 00                   | 7 34.466                          | 29 52 25.53               |
| 8 00                    | 2 24.506                          | 7 57 35.49                | 30 30                   | 7 38.991                          | 30 22 21.01               |
| 8 30                    | 2 33.280                          | 8 27 26.72                | 31 00                   | 7 43.376                          | 30 52 16.62               |
| 9 00                    | 2 42.000                          | 8 57 17.99                | 31 30                   | 7 47.621                          | 31 22 12.38               |
| 9 30                    | 2 50.688                          | 9 27 09.31                | 32 00                   | 7 51.724                          | 31 52 08.28               |
| 10 00                   | 2 59.316                          | 9 57 00.68                | 32 30                   | 7 55.683                          | 32 22 04.32               |
| 10 30                   | 3 07.889                          | 10 26 52.11               | 33 00                   | 7 59.498                          | 32 52 00.50               |
| 11 00                   | 3 16.405                          | 10 56 43.60               | 33 30                   | 8 03.167                          | 33 21 56.33               |
| 11 30                   | 3 24.862                          | 11 26 35.14               | 34 00                   | 8 06.690                          | 33 51 53.31               |
| 12 00                   | 3 33.257                          | 11 56 26.74               | 34 30                   | 8 10.064                          | 34 21 49.94               |
| 12 30                   | 3 41.588                          | 12 26 18.41               | 35 00                   | 8 13.290                          | 34 51 46.71               |
| 13 00                   | 3 49.851                          | 12 56 10.15               | 35 30                   | 8 16.366                          | 35 21 43.63               |
| 13 30                   | 3 58.044                          | 13 26 01.96               | 36 00                   | 8 19.290                          | 35 51 40.71               |
| 14 00                   | 4 06.166                          | 13 55 53.83               | 36 30                   | 8 22.063                          | 36 21 37.94               |
| 14 30                   | 4 14.213                          | 14 25 45.79               | 37 00                   | 8 24.684                          | 36 51 35.32               |
| 15 00                   | 4 22.183                          | 14 55 37.82               | 37 30                   | 8 27.150                          | 37 21 32.85               |
| 15 30                   | 4 30.073                          | 15 25 29.93               | 38 00                   | 8 29.463                          | 37 51 30.54               |
| 16 00                   | 4 37.882                          | 15 55 22.12               | 38 30                   | 8 31.621                          | 38 21 28.38               |
| 16 30                   | 4 45.606                          | 16 25 14.39               | 39 00                   | 8 33.623                          | 38 51 26.38               |
| 17 00                   | 4 53.244                          | 16 55 06.76               | 39 30                   | 8 35.469                          | 39 21 24.53               |
| 17 30                   | 5 00.794                          | 17 24 59.21               | 40 00                   | 8 37.158                          | 39 51 22.84               |
| 18 00                   | 5 08.252                          | 17 54 51.75               | 40 30                   | 8 38.689                          | 40 21 21.31               |
| 18 30                   | 5 15.616                          | 18 24 44.38               | 41 00                   | 8 40.063                          | 40 51 19.94               |
| 19 00                   | 5 22.885                          | 18 54 37.12               | 41 30                   | 8 41.278                          | 41 21 18.72               |
| 19 30                   | 5 30.056                          | 19 24 29.94               | 42 00                   | 8 42.335                          | 41 51 17.66               |
| 20 00                   | 5 37.127                          | 19 54 22.87               | 42 30                   | 8 43.233                          | 42 21 16.77               |
| 20 30                   | 5 44.096                          | 20 24 15.90               | 43 00                   | 8 43.972                          | 42 51 16.03               |
| 21 00                   | 5 50.960                          | 20 54 09.04               | 43 30                   | 8 44.551                          | 43 21 15.45               |
| 21 30                   | 5 57.718                          | 21 24 02.28               | 44 00                   | 8 44.970                          | 43 51 15.03               |
| 22 00                   | 6 04.368                          | 21 53 55.63               | 44 30                   | 8 45.230                          | 44 21 14.77               |
| 22 30                   | 6 10.907                          | 22 23 49.09               | 45 00                   | 8 45.329                          | 44 51 14.67               |

$$\varphi - \omega = +525''3298 \sin 2\varphi - 0''5575 \sin 4\varphi + 0''0007 \sin 6\varphi.$$

$$\varphi - \omega = [2.7204320] \sin 2\varphi - [9.74623 - 10] \sin 4\varphi + [6.867 - 10] \sin 6\varphi.$$

## LATITUDE TRANSFORMATION—Continued.

*Geodetic to rectifying—Continued.*

| Geodetic latitude. | Geodetic minus rectifying. | Rectifying latitude. | Geodetic latitude. | Geodetic minus rectifying. | Rectifying latitude. |
|--------------------|----------------------------|----------------------|--------------------|----------------------------|----------------------|
| $\phi$             | $\phi - \omega$            | $\omega$             | $\phi$             | $\phi - \omega$            | $\omega$             |
| 45 00              | 8 45.329                   | 44 51 14.67          | 67 30              | 6 12.022                   | 67 23 47.98          |
| 45 30              | 8 45.269                   | 45 21 14.73          | 68 00              | 6 05.482                   | 67 53 54.52          |
| 46 00              | 8 45.048                   | 45 51 14.95          | 68 30              | 5 58.831                   | 68 24 01.17          |
| 46 30              | 8 44.662                   | 46 21 15.33          | 69 00              | 5 52.069                   | 68 54 07.93          |
| 47 00              | 8 44.127                   | 46 51 15.87          | 69 30              | 5 45.200                   | 69 24 14.80          |
| 47 30              | 8 43.427                   | 47 21 16.57          | 70 00              | 5 38.225                   | 69 54 21.78          |
| 48 00              | 8 42.567                   | 47 51 17.43          | 70 30              | 5 31.147                   | 70 24 28.85          |
| 48 30              | 8 41.548                   | 48 21 18.45          | 71 00              | 5 23.967                   | 70 54 36.03          |
| 49 00              | 8 40.370                   | 48 51 19.63          | 71 30              | 5 16.688                   | 71 24 43.31          |
| 49 30              | 8 39.034                   | 49 21 20.97          | 72 00              | 5 09.312                   | 71 54 50.69          |
| 50 00              | 8 37.539                   | 49 51 22.46          | 72 30              | 5 01.841                   | 72 24 58.16          |
| 50 30              | 8 35.886                   | 50 21 24.11          | 73 00              | 4 54.278                   | 72 55 05.72          |
| 51 00              | 8 34.070                   | 50 51 25.92          | 73 30              | 4 46.625                   | 73 25 13.38          |
| 51 30              | 8 32.110                   | 51 21 27.89          | 74 00              | 4 38.884                   | 73 55 21.12          |
| 52 00              | 8 29.986                   | 51 51 30.01          | 74 30              | 4 31.058                   | 74 25 28.94          |
| 52 30              | 8 27.708                   | 52 21 32.29          | 75 00              | 4 23.148                   | 74 55 36.85          |
| 53 00              | 8 25.274                   | 52 51 34.73          | 75 30              | 4 15.158                   | 75 25 44.84          |
| 53 30              | 8 22.687                   | 53 21 37.31          | 76 00              | 4 07.090                   | 75 55 52.91          |
| 54 00              | 8 19.946                   | 53 51 40.05          | 76 30              | 3 58.946                   | 76 26 01.05          |
| 54 30              | 8 17.052                   | 54 21 42.95          | 77 00              | 3 50.729                   | 76 56 09.27          |
| 55 00              | 8 14.006                   | 54 51 45.99          | 77 30              | 3 42.442                   | 77 26 17.56          |
| 55 30              | 8 10.810                   | 55 21 49.19          | 78 00              | 3 34.086                   | 77 56 25.91          |
| 56 00              | 8 07.464                   | 55 51 52.54          | 78 30              | 3 25.664                   | 78 26 34.34          |
| 56 30              | 8 03.969                   | 56 21 56.03          | 79 00              | 3 17.180                   | 78 56 42.82          |
| 57 00              | 8 00.327                   | 56 51 59.67          | 79 30              | 3 08.635                   | 79 26 51.36          |
| 57 30              | 7 56.537                   | 57 22 03.46          | 80 00              | 3 00.032                   | 79 56 59.97          |
| 58 00              | 7 52.602                   | 57 52 07.40          | 80 30              | 2 51.374                   | 80 27 08.63          |
| 58 30              | 7 48.523                   | 58 22 11.48          | 81 00              | 2 42.664                   | 80 57 17.34          |
| 59 00              | 7 44.301                   | 58 52 15.70          | 81 30              | 2 33.904                   | 81 27 26.10          |
| 59 30              | 7 39.937                   | 59 22 20.06          | 82 00              | 2 25.096                   | 81 57 34.90          |
| 60 00              | 7 35.432                   | 59 52 24.57          | 82 30              | 2 16.245                   | 82 27 43.76          |
| 60 30              | 7 30.788                   | 60 22 29.21          | 83 00              | 2 07.351                   | 82 57 52.65          |
| 61 00              | 7 26.006                   | 60 52 33.99          | 83 30              | 1 58.418                   | 83 28 01.58          |
| 61 30              | 7 21.088                   | 61 22 38.91          | 84 00              | 1 49.449                   | 83 58 10.55          |
| 62 00              | 7 16.035                   | 61 52 43.96          | 84 30              | 1 40.447                   | 84 28 19.55          |
| 62 30              | 7 10.849                   | 62 22 49.15          | 85 00              | 1 31.414                   | 84 58 28.59          |
| 63 00              | 7 05.531                   | 62 52 54.47          | 85 30              | 1 22.352                   | 85 28 37.65          |
| 63 30              | 7 00.083                   | 63 22 59.92          | 86 00              | 1 13.266                   | 85 58 46.73          |
| 64 00              | 6 54.507                   | 63 53 05.49          | 86 30              | 1 04.157                   | 86 28 55.84          |
| 64 30              | 6 48.804                   | 64 23 11.20          | 87 00              | 0 55.028                   | 86 59 04.97          |
| 65 00              | 6 42.975                   | 64 53 17.02          | 87 30              | 0 45.882                   | 87 29 14.12          |
| 65 30              | 6 37.024                   | 65 23 22.98          | 88 00              | 0 36.723                   | 87 59 23.28          |
| 66 00              | 6 30.951                   | 65 53 29.05          | 88 30              | 0 27.552                   | 88 29 32.45          |
| 66 30              | 6 24.758                   | 66 23 35.24          | 89 00              | 0 18.373                   | 88 59 41.63          |
| 67 00              | 6 18.448                   | 66 53 41.55          | 89 30              | 0 09.188                   | 89 29 50.81          |
| 67 30              | 6 12.022                   | 67 23 47.98          | 90 00              | 0 00.000                   | 90 00 00.00          |

$$\phi - \omega = +525^{\circ}3298 \sin 2\phi - 0^{\circ}5575 \sin 4\phi + 0^{\circ}0007 \sin 6\phi.$$

$$\phi - \omega = [2.7204320] \sin 2\phi - [9.74623-10] \sin 4\phi + [6.867-10] \sin 6\phi.$$

## LATITUDE TRANSFORMATION—Continued.

Rectifying to geodetic.

| Rectifying latitude. | Geodetic minus rectifying. | Geodetic latitude. | Rectifying latitude. | Geodetic minus rectifying. | Geodetic latitude. |
|----------------------|----------------------------|--------------------|----------------------|----------------------------|--------------------|
| $\omega$             | $\varphi - \omega$         | $\varphi$          | $\omega$             | $\varphi - \omega$         | $\varphi$          |
| 0 00                 | 0 00.000                   | 0 00 00.00         | 22 30                | 6 12.246                   | 22 36 12.25        |
| 0 30                 | 0 08.198                   | 0 30 08.20         | 23 00                | 6 18.672                   | 23 06 18.67        |
| 1 00                 | 0 18.358                   | 1 00 18.39         | 23 30                | 6 24.981                   | 23 36 24.98        |
| 1 30                 | 0 27.576                   | 1 30 27.58         | 24 00                | 6 31.173                   | 24 06 31.17        |
| 2 00                 | 0 36.754                   | 2 00 36.75         | 24 30                | 6 37.245                   | 24 36 37.24        |
| 2 30                 | 0 45.921                   | 2 30 45.92         | 25 00                | 6 43.195                   | 25 06 43.20        |
| 3 00                 | 0 55.075                   | 3 00 55.08         | 25 30                | 6 49.022                   | 25 36 49.02        |
| 3 30                 | 1 04.211                   | 3 31 04.21         | 26 00                | 6 54.723                   | 26 06 54.72        |
| 4 00                 | 1 13.328                   | 4 01 13.33         | 26 30                | 7 00.298                   | 26 37 00.30        |
| 4 30                 | 1 22.422                   | 4 31 22.42         | 27 00                | 7 05.743                   | 27 07 05.74        |
| 5 00                 | 1 31.490                   | 5 01 31.49         | 27 30                | 7 11.058                   | 27 37 11.06        |
| 5 30                 | 1 40.531                   | 5 31 40.53         | 28 00                | 7 16.242                   | 28 07 16.24        |
| 6 00                 | 1 49.540                   | 6 01 49.54         | 28 30                | 7 21.292                   | 28 37 21.29        |
| 6 30                 | 1 58.518                   | 6 31 58.52         | 29 00                | 7 26.206                   | 29 07 26.21        |
| 7 00                 | 2 07.456                   | 7 02 07.46         | 29 30                | 7 30.984                   | 29 37 30.98        |
| 7 30                 | 2 16.357                   | 7 32 16.36         | 30 00                | 7 35.625                   | 30 07 35.62        |
| 8 00                 | 2 25.215                   | 8 02 25.22         | 30 30                | 7 40.125                   | 30 37 40.12        |
| 8 30                 | 2 34.029                   | 8 32 34.03         | 31 00                | 7 44.485                   | 31 07 44.48        |
| 9 00                 | 2 42.796                   | 9 02 42.80         | 31 30                | 7 48.703                   | 31 37 48.70        |
| 9 30                 | 2 51.512                   | 9 32 51.51         | 32 00                | 7 52.778                   | 32 07 52.78        |
| 10 00                | 3 00.176                   | 10 03 00.18        | 32 30                | 7 56.708                   | 32 37 56.71        |
| 10 30                | 3 08.785                   | 10 33 08.78        | 33 00                | 8 00.492                   | 33 08 00.49        |
| 11 00                | 3 17.336                   | 11 03 17.34        | 33 30                | 8 04.129                   | 33 38 04.13        |
| 11 30                | 3 25.826                   | 11 33 25.83        | 34 00                | 8 07.518                   | 34 08 07.62        |
| 12 00                | 3 34.252                   | 12 03 34.25        | 34 30                | 8 10.859                   | 34 38 10.96        |
| 12 30                | 3 42.613                   | 12 33 42.61        | 35 00                | 8 14.149                   | 35 08 14.15        |
| 13 00                | 3 50.906                   | 13 03 50.91        | 35 30                | 8 17.188                   | 35 38 17.19        |
| 13 30                | 3 59.128                   | 13 33 59.13        | 36 00                | 8 20.076                   | 36 08 20.08        |
| 14 00                | 4 07.276                   | 14 04 07.28        | 36 30                | 8 22.811                   | 36 38 22.81        |
| 14 30                | 4 15.348                   | 14 34 15.35        | 37 00                | 8 25.392                   | 37 08 25.39        |
| 15 00                | 4 23.342                   | 15 04 23.34        | 37 30                | 8 27.818                   | 37 38 27.82        |
| 15 30                | 4 31.255                   | 15 34 31.26        | 38 00                | 8 30.090                   | 38 08 30.09        |
| 16 00                | 4 39.085                   | 16 04 39.08        | 38 30                | 8 32.206                   | 38 38 32.21        |
| 16 30                | 4 46.830                   | 16 34 46.83        | 39 00                | 8 34.166                   | 39 08 34.17        |
| 17 00                | 4 54.486                   | 17 04 54.49        | 39 30                | 8 35.969                   | 39 38 35.97        |
| 17 30                | 5 02.052                   | 17 35 02.05        | 40 00                | 8 37.614                   | 40 08 37.61        |
| 18 00                | 5 09.525                   | 18 05 09.52        | 40 30                | 8 39.102                   | 40 38 39.10        |
| 18 30                | 5 16.903                   | 18 35 16.90        | 41 00                | 8 40.431                   | 41 08 40.43        |
| 19 00                | 5 24.184                   | 19 05 24.18        | 41 30                | 8 41.601                   | 41 38 41.60        |
| 19 30                | 5 31.365                   | 19 35 31.36        | 42 00                | 8 42.612                   | 42 08 42.61        |
| 20 00                | 5 38.445                   | 20 05 38.44        | 42 30                | 8 43.464                   | 42 38 43.46        |
| 20 30                | 5 45.421                   | 20 35 45.42        | 43 00                | 8 44.157                   | 43 08 44.16        |
| 21 00                | 5 52.292                   | 21 05 52.29        | 43 30                | 8 44.900                   | 43 38 44.39        |
| 21 30                | 5 59.054                   | 21 35 59.05        | 44 00                | 8 45.062                   | 44 08 45.06        |
| 22 00                | 6 05.708                   | 22 05 05.71        | 44 30                | 8 45.275                   | 44 38 45.28        |
| 22 30                | 6 12.246                   | 22 36 12.25        | 45 00                | 8 45.328                   | 45 08 45.33        |

$$\varphi - \omega = +525.73295 \sin 2\omega + 0.77805 \sin 4\omega + 0.0016 \sin 6\omega.$$

$$\varphi - \omega = [2.7204318] \sin 2\omega + [9.89236 - 10] \sin 4\omega + [7.201 - 10] \sin 6\omega.$$

## LATITUDE TRANSFORMATION—Continued.

Rectifying to geodetic—Continued.

| Rectifying latitude. | Geodetic minus rectifying. | Geodetic latitude. | Rectifying latitude. | Geodetic minus rectifying. | Geodetic latitude. |
|----------------------|----------------------------|--------------------|----------------------|----------------------------|--------------------|
| $\omega$             | $\varphi - \omega$         | $\varphi$          | $\omega$             | $\varphi - \omega$         | $\varphi$          |
| ° / "                | ' "                        | ' "                | ° / "                | ' "                        | ° / "              |
| 45 00                | 8 45.328                   | 45 08 45.33        | 67 30                | 6 10.655                   | 67 36 10.68        |
| 45 30                | 8 45.221                   | 45 38 45.22        | 68 00                | 6 04.148                   | 68 06 04.15        |
| 46 00                | 8 44.954                   | 46 08 44.95        | 68 30                | 5 57.497                   | 68 35 57.50        |
| 46 30                | 8 44.526                   | 46 38 44.53        | 69 00                | 5 50.739                   | 69 05 50.74        |
| 47 00                | 8 43.940                   | 47 08 43.94        | 69 30                | 5 43.876                   | 69 35 43.88        |
| 47 30                | 8 43.104                   | 47 38 43.10        | 70 00                | 5 36.908                   | 70 05 36.91        |
| 48 00                | 8 42.288                   | 48 08 42.29        | 70 30                | 5 29.839                   | 70 35 29.84        |
| 48 30                | 8 41.224                   | 48 38 41.22        | 71 00                | 5 22.669                   | 71 05 22.67        |
| 49 00                | 8 40.000                   | 49 08 40.00        | 71 30                | 5 15.402                   | 71 35 15.40        |
| 49 30                | 8 38.619                   | 49 38 38.62        | 72 00                | 5 08.040                   | 72 05 08.04        |
| 50 00                | 8 37.080                   | 50 08 37.08        | 72 30                | 5 00.585                   | 72 35 00.58        |
| 50 30                | 8 35.384                   | 50 38 35.38        | 73 00                | 4 53.038                   | 73 04 53.04        |
| 51 00                | 8 33.531                   | 51 08 33.53        | 73 30                | 4 45.404                   | 73 34 45.40        |
| 51 30                | 8 31.522                   | 51 38 31.52        | 74 00                | 4 37.682                   | 74 04 37.68        |
| 52 00                | 8 29.357                   | 52 08 29.36        | 74 30                | 4 29.877                   | 74 34 29.88        |
| 52 30                | 8 27.038                   | 52 38 27.04        | 75 00                | 4 21.990                   | 75 04 21.99        |
| 53 00                | 8 24.564                   | 53 08 24.56        | 75 30                | 4 14.024                   | 75 34 14.02        |
| 53 30                | 8 21.938                   | 53 38 21.94        | 76 00                | 4 05.982                   | 76 04 05.98        |
| 54 00                | 8 19.158                   | 54 08 19.16        | 76 30                | 3 57.865                   | 76 33 57.86        |
| 54 30                | 8 16.227                   | 54 38 16.23        | 77 00                | 3 49.670                   | 77 03 49.68        |
| 55 00                | 8 13.146                   | 55 08 13.15        | 77 30                | 3 41.417                   | 77 33 41.42        |
| 55 30                | 8 09.914                   | 55 38 09.91        | 78 00                | 3 33.092                   | 78 03 33.09        |
| 56 00                | 8 06.534                   | 56 08 06.53        | 78 30                | 3 24.703                   | 78 33 24.70        |
| 56 30                | 8 03.006                   | 56 38 03.01        | 79 00                | 3 16.251                   | 79 03 16.25        |
| 57 00                | 7 59.332                   | 57 07 59.33        | 79 30                | 3 07.740                   | 79 33 07.74        |
| 57 30                | 7 55.512                   | 57 37 55.51        | 80 00                | 2 59.173                   | 80 02 59.17        |
| 58 00                | 7 51.548                   | 58 07 51.55        | 80 30                | 2 50.551                   | 80 32 50.55        |
| 58 30                | 7 47.440                   | 58 37 47.44        | 81 00                | 2 41.878                   | 81 02 41.88        |
| 59 00                | 7 43.191                   | 59 07 43.19        | 81 30                | 2 33.158                   | 81 32 33.16        |
| 59 30                | 7 38.802                   | 59 37 38.80        | 82 00                | 2 24.388                   | 82 02 24.39        |
| 60 00                | 7 34.273                   | 60 07 34.27        | 82 30                | 2 15.576                   | 82 32 15.58        |
| 60 30                | 7 29.606                   | 60 37 29.61        | 83 00                | 2 06.723                   | 83 02 06.72        |
| 61 00                | 7 24.803                   | 61 07 24.80        | 83 30                | 1 57.832                   | 83 31 57.83        |
| 61 30                | 7 19.866                   | 61 37 19.87        | 84 00                | 1 48.906                   | 84 01 48.91        |
| 62 00                | 7 14.794                   | 62 07 14.79        | 84 30                | 1 39.946                   | 84 31 39.95        |
| 62 30                | 7 09.592                   | 62 37 09.59        | 85 00                | 1 30.956                   | 85 01 30.96        |
| 63 00                | 7 04.250                   | 63 07 04.26        | 85 30                | 1 21.939                   | 85 31 21.94        |
| 63 30                | 6 58.797                   | 63 36 58.80        | 86 00                | 1 12.897                   | 86 01 12.90        |
| 64 00                | 6 53.209                   | 64 06 53.21        | 86 30                | 1 03.833                   | 86 31 03.83        |
| 64 30                | 6 47.495                   | 64 36 47.50        | 87 00                | 0 54.750                   | 87 00 54.75        |
| 65 00                | 6 41.658                   | 65 06 41.66        | 87 30                | 0 45.650                   | 87 30 45.65        |
| 65 30                | 6 35.692                   | 65 36 35.70        | 88 00                | 0 36.537                   | 88 00 36.54        |
| 66 00                | 6 29.621                   | 66 06 29.62        | 88 30                | 0 27.412                   | 88 30 27.41        |
| 66 30                | 6 23.424                   | 66 36 23.42        | 89 00                | 0 18.280                   | 89 00 18.28        |
| 67 00                | 6 17.112                   | 67 06 17.11        | 89 30                | 0 09.141                   | 89 30 09.14        |
| 67 30                | 6 10.685                   | 67 36 10.68        | 90 00                | 0 00.000                   | 90 00 00.00        |

$$\varphi - \omega = +525.3295 \sin 2\omega + 0^{\circ}7805 \sin 4\omega + 0^{\circ}0016 \sin 6\omega.$$

$$\varphi - \omega = [2.7204318] \sin 2\omega + [9.89236 - 10] \sin 4\omega + [7.201 - 10] \sin 6\omega.$$

## PUBLICATION NOTICES

The Coast and Geodetic Survey maintains mailing lists containing the names and addresses of persons interested in its publications. When a new publication or a new edition of a publication is issued on any of the subjects covered by the mailing list, a circular showing the scope and contents of the publication is sent to each person whose name and address is on the mailing list of the subject covered by the publication.

If you desire to receive notices regarding publications of the Coast and Geodetic Survey as issued, you should write to the Director of the Coast and Geodetic Survey, Washington, D. C., indicating the mailing lists on which you wish your name entered, or, if you prefer, you may check the lists on the form below, remove this sheet from the publication, and mail it to the Director of the Coast and Geodetic Survey, Washington, D. C.

(Date) \_\_\_\_\_

The DIRECTOR, UNITED STATES COAST AND GEODETIC SURVEY,  
*Washington, D. C.*

DEAR SIR: I desire that my name shall be placed on the mailing lists indicated by check below to receive notices regarding publications issued by the United States Coast and Geodetic Survey:

- 100. Astronomic Work.
- 100-A. Base Lines.
- 100-B. Coast Pilot.
- 100-C. Currents.
- 100-D. Geodesy, or Measurements of the Earth.
- 100-E. Gravity.
- 100-F. Hydrography.
- 100-G. Levelling.
- 100-H. Nautical Charts.
- 100-I. Oceanography.
- 100-J. Precise Traverse.
- 100-K. Seismology.
- 100-L. Terrestrial Magnetism.
- 100-M. Tides.
- 100-N. Topography.
- 100-O. Triangulation.
- 100-P. Cartography.
- 100-R. *Airway Maps*

(Name) \_\_\_\_\_

(Address) \_\_\_\_\_