

Security–Reliability Tradeoff Analysis for SWIPT- and AF-Based IoT Networks With Friendly Jammers

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Abstract—Radio-frequency (RF) energy harvesting (EH) in wireless relaying networks has attracted considerable recent interest, especially for supplying energy to relay nodes in the Internet of Things (IoT) systems to assist the information exchange between a source and a destination. Moreover, limited hardware, computational resources, and energy availability of IoT devices have raised various security challenges. To this end, physical-layer security (PLS) has been proposed as an effective alternative to cryptographic methods for providing information security. In this study, we propose a PLS approach for simultaneous wireless information and power transfer (SWIPT)-based half-duplex (HD) amplify-and-forward (AF) relaying systems in the presence of an eavesdropper. Furthermore, we take into account both static power splitting relaying (SPSR) and dynamic power splitting relaying (DPSR) to thoroughly investigate the benefits of each one. To further enhance secure communication, we consider multiple friendly jammers to help prevent wiretap-

ping attacks from the eavesdropper. More specifically, we provide a reliability and security analysis by deriving closed-form expressions of outage probability (OP) and intercept probability (IP), respectively, for both the SPSR and DPSR schemes. Then, simulations are also performed to validate our analysis and the effectiveness of the proposed schemes. Specifically, numerical results illustrate the nontrivial tradeoff between reliability and security of the proposed system. In addition, we conclude from the simulation results that the proposed DPSR scheme outperforms the SPSR-based scheme in terms of OP and IP under the influences of different parameters on system performance.

Index Terms—Amplify and forward (AF), dynamic power splitting (PS), intercept probability (IP), outage probability (OP), source selection, simultaneous wireless information and power transfer (SWIPT).

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I. INTRODUCTION

THE Internet of Things (IoT) has played a pivotal role in fifth generation (5G) and beyond networks, seen as a novel solution to enable a smarter and safer life via autonomous monitoring and control in fields, such as healthcare, manufacturing, and agriculture as demonstrated in [1]–[7] and the reference therein. Nevertheless, the enormous number of potential IoT devices also impose technical challenges in wireless communication due to limited resources comprising, for example, available bandwidth and energy supply. In particular, replacing or recharging batteries for IoT devices is generally costly, inconvenient, and even impossible in many scenarios, such as hazardous or toxic environments or inside the human body. Smart ways of using and harvesting energy in IoT devices have attracted particular interest.

A. Related Works

To address these issues, energy harvesting (EH) communication networks are considered as alternative solutions. Energy can be harvested from sources such solar [8], wind [9], [10], vibration [11], [12], and radio-frequency (RF) signals, among which RF-based EH is an attractive solution because of its controllability and predictability. More importantly, it can carry both energy and information. Based on the above discussion, simultaneous wireless information and power transfer (SWIPT) is a promising future direction for realizing sustainable wireless communication [13]. There are two kinds of EH

receivers used in SWIPT networks: 1) time switching (TS) and 2) power splitting (PS) techniques. For the TS technique, the receiving node switches between information transfer (IT) and EH in different time slots, whereas, in the PS method, it splits the received power into factors for IT and EH [14], [15].

Beyond the benefits of EH, relay nodes in cooperative communication networks can help a source node transfer information to a destination, which can extend the coverage of IoT devices with inherent limitations, such as low power and remote location [16]–[19]. Therefore, cooperative relay networks with EH have received significant attention from researchers in recent years [20]–[27]. For example, amplify-and-forward (AF)-based wireless cooperative or sensor networks with TS and PS protocols were considered [20]. Also, Chen *et al.* [21] proposed and investigated a novel multihop AF relaying network in terms of co-channel interference (CCI) and Nakagami- m fading, whereas each user could harvest energy from the CCI. In contrast to [20], [21] and [28] which considered only SISO systems, a multiple-input–multiple-output (MIMO) system for maximizing the efficiency of SWIPT was investigated in [22]. Furthermore, the system performance of cognitive radio networks (CRNs) was studied in [23] and [24], and the system performance of bidirectional relay networks was considered in [25]. Besides, Tin *et al.* [26] proposed a new EH-based two-way (TW) half-duplex (HD) relay sensor network in the presence of a direct link between a transmitter and a receiver. Specifically, they derived the exact and asymptotic ergodic capacity and performed an exact analysis of the symbol error rate. Furthermore, Nguyen *et al.* [27] also proposed and investigated a new system model for SWIPT-based TW relaying systems. Therein, they derived closed-form expressions for the outage probability (OP) of three relaying schemes, termed decode-and-forward (DF), AF, and hybrid-DF (HDAF). In addition, An *et al.* [29] considered hybrid time–PS (HTPS) TW HD cooperative relaying in the presence of an eavesdropper. In this context, they derived closed-form expressions for OP and intercept probability (IP) using the maximal ratio combining (MRC) and the selection combining (SC). Tin *et al.* [30] investigated physical-layer security (PLS) in a power beacon-assisted full-duplex (FD) EH relaying system using delay-tolerant (DT) and delay-limited (DL) methods. It was shown that the OP can be significantly improved by applying a dynamic PS scheme in [31] and an adaptive PS scheme as in [32] and [33]. Ye *et al.* [31] considered a novel dynamic asymmetric PS scheme based on asymmetric instantaneous channel gains between relay and destinations to improve the OP. Ashraf *et al.* [32] proposed an adaptive PS protocol to enhance OP performance and average achievable capacity. Moreover, Singh and Ochiai [33] took into account the combination of the TS protocol and the dynamic PS to demonstrate the superiority of their proposed scheme in terms of OP and data transmission rate over the TS and PS schemes.

Due to the broadcast nature of the wireless medium, information in IoT networks can be easily overheard, thus, the problem of enhancing security in IoT communications is an important issue. In comparison with conventional upper layer security methods, PLS has many advantages, such as:

1) uncomplicated secret key distribution and management due to independence in encryption/decryption operations; 2) simple signal processing operations that involve minor additional overhead; and 3) adaptive signal design and resource allocation with flexible security levels. Based on these advantages, PLS represents a promising solution for IoT networks [34]–[39]. In [40], secrecy outage performance (SOP) using transmit antenna selection (TAS)/SC of multihop cognitive wireless sensor networks was investigated, and secure performance in a dual-hop MIMO relay system with outdated channel state information (CSI) was evaluated in [41]. Also, Tran *et al.* [42] proposed and analyzed a generalized partial relay selection (PRS) protocol to improve security for CRNs with both cases of perfect or imperfect CSI. Moreover, Hieu *et al.* [43] also considered a novel system model for an EH-based PLS multihop multipath cooperative wireless network. They then proposed three relay protocols, termed the shortest path, the random path, and the best path selection schemes to enhance PLS performance. A power allocation scheme to improve the PLS of the relay network was presented in [44], and Shukla *et al.* [45] proposed user selection along with an antenna selection (AS) scheme to maximize the end-to-end signal-to-noise ratios (SNRs) of a cellular multiuser TW AF relay network. In addition, a novel wireless caching scheme to enhance the PLS of video streaming in cellular networks was proposed in [46] and [47]; and the influence of an eavesdropper and CCI on IP was considered in [48].

Despite the fruitful research in the literature, the aforementioned works in [34]–[48] did not take into account jammers or artificial noises (ANs) to improve system security. Recently, intensive works have brought ANs and jammers into consideration [49]–[55]. To prevent the eavesdropper from intercepting transmitted signals, Oggier and Hassibi [49] studied the employment of multiple transmit antennas for generating AN to interfere with the eavesdropper without disturbing the legitimate receiver. It was shown in [49] that wireless secrecy can be guaranteed with the aid of AN if the transmitter has more antennas than the eavesdropper. Wang *et al.* [50] investigated secure communication of a MIMO system, in which the source, destination, and eavesdropper are each equipped with a random number of antennas. In [51]–[53], distributed beamforming or friendly jammers were deployed in the relay networks to prevent the eavesdropper from overhearing confidential information. Zou *et al.* [54], [55] studied multiuser scheduling as a method to enhance the system PLS.

B. Motivation and Contributions

Despite previous achievements in the above-mentioned works, the investigation of SWIPT and PLS in cooperative IoT networks still has room for research in terms of the closed-form expressions for the OP and IP, which are independent of small-scale fading coefficients and can work for a long period of time. Moreover, to the best of our knowledge, there is no such related work on designing the optimal dynamic PS scheme for a SWIPT- and AF-based relay network consisting of multiple sources, multiple friendly jammers, an EH relay, and a destination in the presence of an eavesdropper.

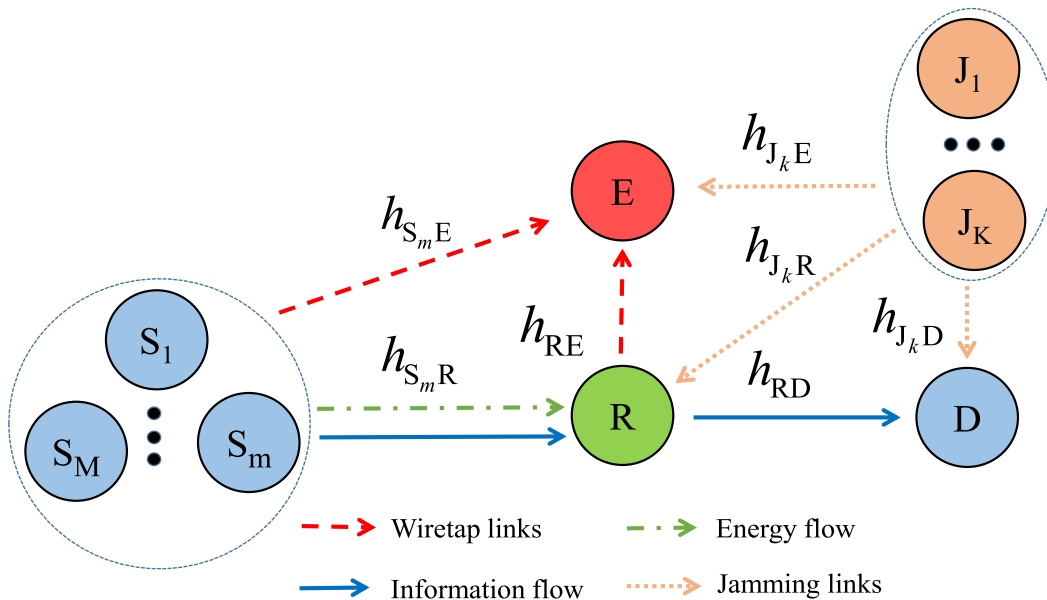


Fig. 1. SWIPT-based relay system with friendly jammers against attack from an eavesdropper.

Motivated by the above discussions, this article provides a thorough analysis of the reliability and security tradeoff using PS-based relay protocol. The best source approach is proposed to enhance performance with the effect of an eavesdropper and the presence of friendly jammers to prevent this eavesdropper. The main contributions of this research can be summarized as follows.

- 1) We derive closed-form expressions for the OP of the legitimate communications and an exact integral form for the IP of the eavesdropper's channel under the assistance from multiple friendly jammers.
- 2) This work also provides an in-depth analysis of the influence of various system parameters on security and reliability performance. For the SWIPT technique, both dynamic PS-based relaying (DPSR) and static PS-based relaying (SPSR) are considered in our work to give a full picture of the advantages of each method for OP and IP cases.
- 3) Mathematical analysis is given to obtain an exact closed-form expression for the optimal PS ratio, i.e., ρ^* , to maximize the total achievable rate at the destination.
- 4) The correctness of our analysis is confirmed through numerical simulations. From the simulation results, we provide recommendations on selecting the configurations to obtain reliable and secure transmission without paying too much for the complexity of the system.

The remainder of this article is organized as follows. The system model is given in Section II. The performance is presented in Section III. Numerical results are depicted in Sections IV and V concludes this article.

II. SYSTEM MODEL

As described in Fig. 1, the system model includes multi-source (M source nodes) transfer information to the destination (D) via one relay (R) with the presence of multi friendly

jammers (J_1, \dots, J_K) and an eavesdropper (E). Friendly jammers are legitimate users in the system and emit AN using a pseudorandom sequence, which is known to other legitimate users (i.e., source, relay, and destination) and remains unknown to eavesdropper E [56]. It should be noted that these pseudorandom sequences are known among legitimate users but not to the illegitimate user. Moreover, similar to conventional cryptography, pseudorandom sequences do not have to be preshared, they can be acquired by legitimate users through physical-layer key agreement and generation that supports channel estimation, as intensively studied in the information-theoretic PLS literature [57], [58]. Particularly, the wireless system is assumed to change the pseudorandom sequence frequently, which significantly reduces the possibility that an eavesdropper can know all of these sequences and enhances system security.

We assume that the direct connection between the M sources and the destination nodes is too weak due to severe fading or long distances, hence, the only available communication path as well as power transfer path is through relay R . We also assume that E is located far away from M sources and cannot overhear the messages transmitted from these sources. All nodes in this model are single-antenna devices and operate on the HD mode. The EH and information transmission processes for the model system are shown in Fig. 2. In Fig. 2, we exploit the first phase to supply the required power to the relay from the best source S to help the relay forward the exchange data afterward. Specifically, the relay R utilizes a power splitter to divide the received signal into two parts, whereas the first part is used for collecting energy and storing it in the battery, while the second part is used for transferring received data. We define ρ as a PS ratio, i.e., the ratio of the power received at the relay node used for the EH. Next, the IT process from R to D is conducted in the remaining time period [59]–[61].

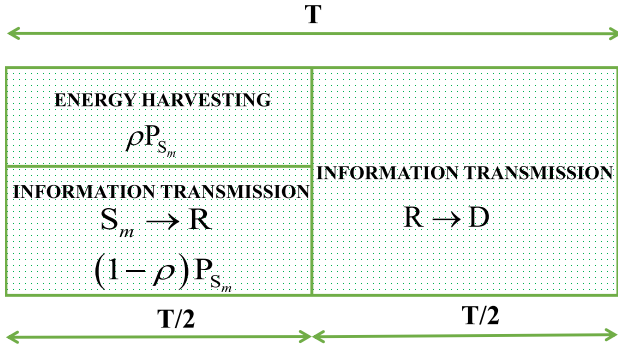


Fig. 2. EH and IT processes with PS relaying protocol.

Assuming the channel coefficient between any two nodes follows Rayleigh fading in which the channel is unchanged within a transmission block and to vary independently on different blocks. Let h_{XY} with $XY \in \{S_m R, RE, RD, JE, JR, JD\}$ denote the channel from $X \rightarrow Y$, then the corresponding channel gains can be defined as follows:

$$\gamma_{XY} = |h_{XY}|^2, XY \in \{S_m R, RE, RD, JE, JR, JD\}. \quad (1)$$

Notice that the channel gains are assumed to be exponential random variables in which probability density function (PDF) and cumulative distribution function (CDF) are, respectively, represented as follows:

$$F_X(x) = 1 - \exp(-\lambda x) \quad (2)$$

$$f_X(x) = \frac{\partial F_X(x)}{\partial x} = \lambda \exp(-\lambda x) \quad (3)$$

where λ is the rate parameter of the exponential random variable X . To take path-loss into account, we can model the parameters as follows:

$$\lambda_{XY} = (d_{XY})^\chi \quad (4)$$

where χ is the pathloss exponent and d_{XY} is distance between nodes X and Y .

Now, we discuss the adopted system model. As mention above, supposing source S_m is chosen to send its information and energy. During the first transmission phase, the received signal at the relay can be given by

$$y_R = \sqrt{1 - \rho} h_{S_m R} x_{S_m} + \sum_{k=1}^K x_k h_{J_k R} + n_R \quad (5)$$

where x_{S_m} is the message transmitted with $\mathbb{E}\{|x_{S_m}|^2\} = P_S$; x_k is the AN transmitted by the jammer J_k , which satisfies $\mathbb{E}\{|x_k|^2\} = P_J$, $\mathbb{E}\{\cdot\}$ denotes the expectation operation; and n_R is the zero mean additive white Gaussian noise (AWGN) with variance N_0 . Our proposed model only considers the multifriendly jammers, which are just against the eavesdropper. Hence, relay R and destination D will know the jamming signals and cancel them in their received signals. So, the received signal at R can be rewritten as follows:

$$y_R = \sqrt{1 - \rho} h_{S_m R} x_{S_m} + n_R. \quad (6)$$

Following the same methodology as in [62], the EH in relay can be computed as:

$$P_R = \frac{E_R}{T/2} = \eta \rho P_{S_m} \gamma_{S_m R} \quad (7)$$

where $0 < \eta \leq 1$ is energy conversion efficiency (which takes into account the energy loss by harvesting circuits and also by decoding and processing circuits); and P_{S_m} and P_R are the transmit powers of S_m and R , respectively. E_R is the amount of the harvested energy at the relay and it can be calculated as $E_R \triangleq \eta \rho P_{S_m} \gamma_{S_m R} T/2$. The channel gain $\gamma_{S_m R}$ is defined as $\gamma_{S_m R} = |h_{S_m R}|^2$, which is a special case of (1). Besides, $\rho \in [0, 1]$ is the PS factor, where ρ equals zero (or one) signifies that total received RF signals used for EH (or information transmission).

As mentioned above, the received signal at the destination can be given as follows:

$$y_D = h_{RD} x_R + n_D \quad (8)$$

where n_D is the zero mean AWGN with variance N_0 .

In this article, we consider the AF relaying protocol. Therefore, the signal transmitted by the relay is an amplified version of y_R , which is denoted by a factor β as follows:

$$\beta = \frac{x_R}{y_R} = \sqrt{\frac{P_R}{(1 - \rho) P_{S_m} |h_{S_m R}|^2 + N_0}} \approx \sqrt{\frac{\eta \rho}{1 - \rho}}. \quad (9)$$

From (6) and (9), the received signal at D can be rewritten by

$$\begin{aligned} y_D &= h_{RD} x_R + n_D = h_{RD} \beta y_R + n_D \\ &= h_{RD} \beta \left[\sqrt{1 - \rho} h_{S_m R} x_{S_m} + n_R \right] + n_D \\ &= \underbrace{\sqrt{1 - \rho} h_{RD} h_{S_m R} \beta x_{S_m}}_{\text{signal}} + \underbrace{h_{RD} \beta n_R + n_D}_{\text{noise}}. \end{aligned} \quad (10)$$

Hence, the SNR at D in this phase can be obtained by

$$\gamma_D = \frac{E\{\text{signal}^2\}}{E\{\text{noise}^2\}} = \frac{(1 - \rho) P_{S_m} \gamma_{S_m R} \gamma_{RD} \beta^2}{\gamma_{RD} \beta^2 N_0 + N_0}. \quad (11)$$

After some algebraic manipulations, we have

$$\gamma_D = \frac{\eta \rho (1 - \rho) \Psi \gamma_{S_m R} \gamma_{RD}}{\eta \rho \gamma_{RD} + (1 - \rho)} \quad (12)$$

where $\Psi = (P_S/N_0)$. The achievable rate of system can be claimed by

$$C_{AF} = \frac{1}{2} \log_2(1 + \gamma_D). \quad (13)$$

Taking into account the impact of eavesdropper E , at the first time slot the chosen source S_m will broadcast its signal to relay and E can overhear this information. To prevent E from eavesdropping legitimate information, jammers will send the jamming signals to E , so the received signal at E can be expressed by

$$y_E^1 = h_{S_m E} x_{S_m} + h_{RE} x_R + \sum_{k=1}^K x_k h_{J_k E} + n_E \quad (14)$$

where n_E^1 is the zero mean AWGN with variance N_0 . Based on (14), the SNR at the E during first time slot is given as follows:

$$\gamma_E^1 = \frac{P_{S_m} \gamma_{S_m E}}{P_J \sum_{k=1}^K \gamma_{J_k E} + N_0} = \frac{\Psi \gamma_{S_m E}}{\Phi \Xi + 1} \approx \frac{\Psi \gamma_{S_m E}}{\Phi \Xi} \quad (15)$$

where $\Phi = (P_J/N_0)$ and $\Xi = \sum_{k=1}^K \gamma_{J_k E}$. Here, please note that after received the information from chosen source S_m , R will amplify this information to D, and also to E with the same amplification factor β . Therefore, the received signal at E can be reexpressed by

$$\begin{aligned} \gamma_E^2 &= h_{RE} \beta \left[\sqrt{1 - \rho} h_{S_m R} x_{S_m} + n_R \right] + \sum_{k=1}^K x_k h_{J_k R} + n_E^2 \\ &= \underbrace{\sqrt{1 - \rho} h_{S_m R} h_{RE} \beta x_{S_m}}_{\text{signal}} + \underbrace{h_{RE} \beta n_R + \sum_{k=1}^K x_k h_{J_k R}}_{\text{noise}} + n_E^2 \end{aligned} \quad (16)$$

where n_E^2 is the zero mean AWGN with variance N_0 . Hence, the received SNR at E during second time slot can be obtained as follows:

$$\begin{aligned} \gamma_E^2 &= \frac{(1 - \rho) \gamma_{S_m R} \gamma_{RE} \beta^2 P_{S_m}}{\gamma_{RE} \beta^2 N_0 + P_J \sum_{k=1}^K \gamma_{J_k E} + N_0} \\ &= \frac{\eta \rho (1 - \rho) \gamma_{S_m R} \gamma_{RE} \Psi}{\eta \rho \gamma_{RE} + (1 - \rho) \Phi \Xi + (1 - \rho)}. \end{aligned} \quad (17)$$

Finally, the eavesdropper can apply SC technique, thus, the achievable rate at E can be given by

$$C_E = \frac{1}{2} \log_2(1 + \gamma_E) \quad (18)$$

where $\gamma_E = \max(\gamma_E^1, \gamma_E^2)$.

Remark 1: The best source S_m would be selected for the purpose of enhancing the transmission performance. Mathematically speaking, we can write as followings:

$$\begin{aligned} n &\triangleq \arg \max_{m=1,2,\dots,M} \{\gamma_{S_m R}\} \\ &\Leftrightarrow \gamma_{S_n R} \triangleq \max_{m=1,2,\dots,M} \{\gamma_{S_m R}\}. \end{aligned} \quad (19)$$

Assume that the links from M sources to the relay R are identical independent distribution (i.i.d), and hence CDF and PDF of $\gamma_{S_m R}$ can be formulated as, respectively

$$\begin{aligned} F_{\gamma_{S_m R}}(x) &= \Pr(\gamma_{S_m R} < x) \\ &= \Pr(\gamma_{S_m R} < x, \forall m = 1, 2, \dots, M) \\ &= \prod_{m=1}^M F_{\gamma_{S_m R}}(x) = [1 - e^{-\lambda_{S_m R} x}]^M \\ &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp(-b \lambda_{S_m R} x), \end{aligned} \quad (20)$$

$$f_{\gamma_{S_m R}}(x) = \lambda_{S_m R} \sum_{b=1}^{M-1} (-1)^b C_{M-1}^b \exp(-(b+1) \lambda_{S_m R} x) \quad (21)$$

where $C_M^b = (M! / b!(M-b)!)$.

Remark 2: Because Ξ is a summation of K i.i.d. exponential random variables, its PDF can be given by [63]

$$f_{\Xi}(x) = \frac{(\lambda_{JE})^K}{(K-1)!} x^{K-1} \exp(-\lambda_{JE} x). \quad (22)$$

III. PERFORMANCE ANALYSIS

This section provides the mathematical analysis of the OP and IP to provide further insight into the two-hop data transmission for SWIPT-based HD AF relay networks in two cases, i.e., DPSR and SPSR.

A. SPSR Case

1) *Outage Probability Analysis:* In this section, the OP of the SWIPT-aided HD AF relaying system over Rayleigh fading channels is derived. Specifically, it can be calculated as follows:

$$OP = \Pr(C_{AF} < C_{th}) = \Pr(\gamma_D < \gamma_{th}) \quad (23)$$

where $\gamma_{th} = 2^{2C_{th}} - 1$ is the SNR threshold of system and C_{th} is the target rate. The closed-form expression for the OP in (23) is given as follows.

Theorem 1: In static PS-based relaying, the closed-form expression of the OP can be given as follows:

$$\begin{aligned} OP_{SPSR} &= 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b \lambda_{SR} \lambda_{th}}{(1-\rho) \Psi}\right) \\ &\quad \times \sqrt{\frac{b \lambda_{SR} \lambda_{RD} \gamma_{th}}{\eta \rho \Psi}} K_1 \left(2 \sqrt{\frac{b \lambda_{SR} \lambda_{RD} \gamma_{th}}{\eta \rho \Psi}} \right) \end{aligned} \quad (24)$$

where $K_\nu(\cdot)$ is the modified Bessel function of the second kind and the fifth order.

Proof: The detailed proof is available in Appendix A. ■

2) *Intercept Probability Analysis:* Destination D will be intercepted if E can successfully wiretap signal, i.e., $C_E \geq C_{th}$. Therefore, the IP can be defined as [64]

$$IP = \Pr(C_E \geq C_{th}) = \Pr(\gamma_E \geq \gamma_{th}). \quad (25)$$

Theorem 2: The closed-form expression of the IP in this case can be derived by

$$\begin{aligned} IP_{SPSR} &= \left(\frac{\lambda_{JE}}{\tilde{\lambda}_{JE}} \right)^K + \sum_{t=0}^{\infty} \sum_{b=1}^M \frac{(-1)^{b+t} C_M^b \Gamma(t+K)}{t! \Phi^{t+K}} \\ &\quad \times \exp\left(-\frac{b \lambda_{SR} \gamma_{th}}{\rho_1 \Psi}\right) \\ &\quad \times \frac{(\lambda_{JE})^K}{(K-1)!} \times G_{1,3}^{3,0} \left(\frac{b \lambda_{SR} \lambda_{RE} \gamma_{th}}{\eta \rho \Psi} \middle| \begin{matrix} 0 \\ -t-K, 1, 0 \end{matrix} \right) \\ &\quad \times \left[\left(\tilde{\lambda}_{JE} \right)^t - (\lambda_{JE})^t \right] \end{aligned} \quad (26)$$

where $\Gamma(\cdot)$ is the Gamma function and $G_{p,q}^{m,n} \left(z \middle| \begin{matrix} a_1, \dots, a_p \\ b_1, \dots, b_q \end{matrix} \right)$ is the Meijer G-function.

Proof: The detailed proof is available in Appendix B. ■

TABLE I
SIMULATION PARAMETERS

Symbol	Parameter name	Fixed value	Varying range
C_{th}	Source rate	0.25; 0.5 bps/Hz	none
η	Energy harvesting efficiency	0.8	none
ρ	Power splitting factor	0.225; 0.325; 0.5; 0.875;	0 to 1
λ_{S_mR}	Rate parameter of $ h_{S_mR} ^2$	0.1768	none
λ_{RD}	Rate parameter of $ h_{RD} ^2$	0.1768	none
λ_{RE}	Rate parameter of $ h_{RE} ^2$	2.7557 (S1); 1.3216 (S2)	none
λ_{JE}	Rate parameter of $ h_{JE} ^2$	0.1768 (S1); 1 (S2)	none
λ_{SE}	Rate parameter of $ h_{SE} ^2$	3.1434 (S1); 1 (S2)	none
Ψ	Transmit-power-to-noise-ratio of source	2 dB	-5 to 15 (dB)
Φ	Transmit-power-to-noise-ratio of jammer	-1; 1 dB	none
M	Number of source node(s)	2; 3	1 to 10
K	Number of jammer(s)	1	1 to 10

B. DPSR Case

In this section, we would like to find the optimal PS factor, i.e., ρ^* to maximize the achievable rate C_{AF} . By observing (13), we have $\max(C_{AF}) \Leftrightarrow \max(\gamma_D)$. It is easy to prove that $(\partial^2 \gamma_D / \partial^2 \rho)$ is negative for all $0 < \rho < 1$. Hence, we conclude that γ_D is a concave function of ρ . We can find the value of ρ to maximize γ_D by differentiating γ_D concerning ρ and then equate it to zero. After doing some algebraic calculations, ρ^* can be given as $\rho^* = (1/[1 + |h_{RD}|\sqrt{\eta}])$ or $\rho^* = (1/[1 - |h_{RD}|\sqrt{\eta}])$. Because of $\rho^* = (1/[1 - |h_{RD}|\sqrt{\eta}])$ results in the value of $\rho^* > 1$ or $\rho^* < 0$. Therefore, $\rho^* = (1/[1 + |h_{RD}|\sqrt{\eta}])$ is selected as the optimal solution.

Theorem 3: The closed-form expression of the OP in this case can be derived by

$$\begin{aligned}
 OP_{DPSR} &= 1 + \sum_{t=0}^{\infty} \sum_{b=1}^M \frac{(-1)^{t+b} C_M^b 2^{t+1}}{t!} \\
 &\times \left(\frac{\lambda_{RD}}{\eta}\right)^{t/4+1/2} \left(\frac{b\lambda_{SR}\gamma_{th}}{\Psi}\right)^{3t/4+1/2} \\
 &\times \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi}\right) \times K_{-t/2+1}\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RD}\gamma_{th}}{\eta\Psi}}\right)
 \end{aligned} \quad (27)$$

where $K_\nu(\cdot)$ is the modified Bessel function of the second kind and ν^{th} order.

Proof: The detailed proof is available in Appendix C. ■

1) IP Analysis:

Theorem 4: In dynamic PS-based relaying, the exact integral-form expression of the IP is derived as follows:

$$\begin{aligned}
 IP_{DPSR} &= \left(\frac{\lambda_{JE}}{\tilde{\lambda}_{JE}}\right)^K + 2 \sum_{b=1}^M \frac{(-1)^b C_M^b (\lambda_{JE})^K}{(K-1)!} \\
 &\times \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi}\right) \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\Psi}} \\
 &\times \left[\int_0^{\infty} x^{K-1} \exp(-\tilde{\lambda}_{JE}x) \Delta(\omega) \sqrt{(\Phi x + 1)} dx \right. \\
 &\quad \left. - \int_0^{\infty} x^{K-1} \exp(-\lambda_{JE}x) \Delta(\omega) \sqrt{(\Phi x + 1)} dx \right].
 \end{aligned} \quad (28)$$

We have obtained the analytical results in Theorems 1–4, which are independent of small-scale fading coefficients and only based on the statistical CSI. The obtained analyses work for a long period of time and reduce the computational complexity in evaluating the OP and IP of the network.

Remark 3: This article considers scenarios where the jammers are closer to the eavesdropper than the relay. Hence, the RF transmission from friendly jammers was neglected for the sake of simplicity. Once the information of jammers is carefully exploited, both eavesdropper (E) and destination (D) will get benefits to enhance the system performance. A framework using the RF transmission from friendly jammers shares a similar analytical methodology as initially established in this article but with more complicated in detail. This interesting extension is left for future work.

IV. SIMULATION RESULTS

In this section, Monte Carlo simulations are provided to validate the theoretical expressions and the impacts of various parameters on the system performance. To claim the OP and IP for the proposed schemes, we perform 5×10^6 independent trials, and the channel coefficients are randomly generated as Rayleigh fading in each trial. The settings of simulation parameters are detailed in Table I. In particular, we provide two scenarios in other to investigate the system performance corresponding to different node deployments. In the first scenario (S1), sources are located around (0, 0), the relay is located at (0.5, 0), the destination is located at (1, 0), and the eavesdropper is located closer to the relay at (0.5, 1.5). In the second scenario (S2), sources, relay, and destination are kept the same locations, while the eavesdropper is located closer to the sources at (0, 1). The average channel gains, $\mathbb{E}\{\gamma_{XY}\}$ are computed by utilizing (1), where the propagation distances are obtained from the above setting. Furthermore, the rate parameters λ_{S_mR} , λ_{RD} , λ_{JE} , λ_{RE} , and λ_{SE} are given in Table I. The system performance metrics comprising the OP and IP are evaluated as a function of different parameters.

In Figs. 3 and 4, we show the impact of Ψ on OP and IP, where $\eta = 0.8$, $C_{th} = 0.5$ bps/Hz, and $M = 2$. In Fig. 3, we compare DPSR with SPSR in OP analysis, whereas the SPSR is considered in two modes with ρ equals 0.225 and 0.875, respectively. First, it is easy to observe that DPSR obtains

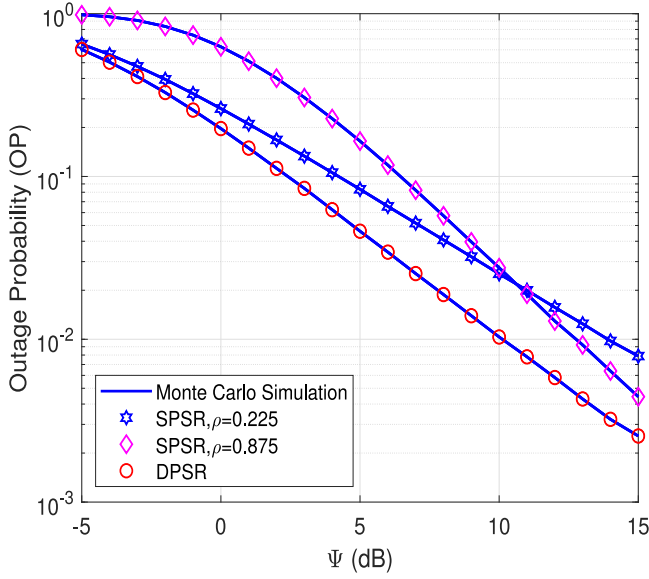


Fig. 3. OP versus Ψ with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, and $M = 2$.

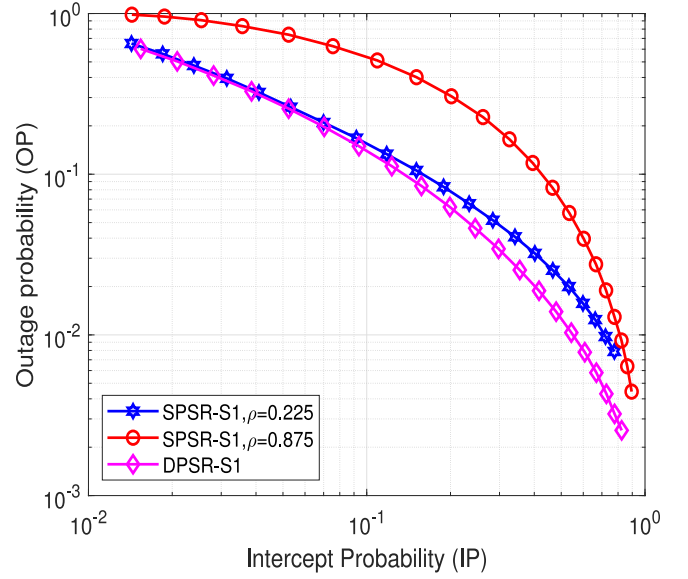


Fig. 5. OP versus IP in scenario 1 with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, $M = 2$, $K = 1$, $\Phi = 1$ dB, and $\Psi \in [-5, 15$ dB].

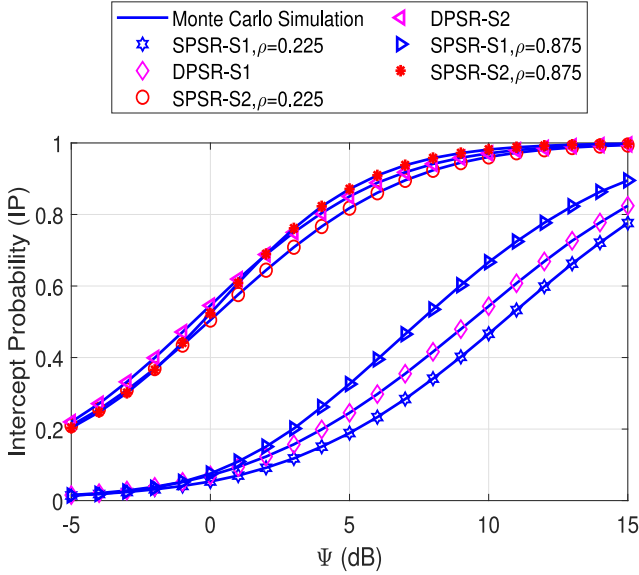


Fig. 4. IP versus Ψ with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, $M = 2$, $K = 1$, and $\Phi = 1$ dB.

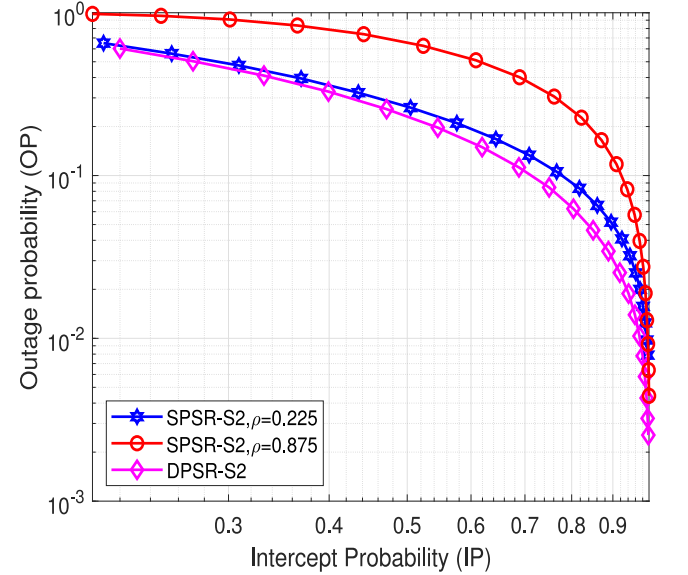


Fig. 6. OP versus IP in scenario 2 with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, $M = 2$, $K = 1$, $\Phi = 1$ dB, and $\Psi \in [-5, 15$ dB].

better OP results than SPSR methods. Specifically, when $\Psi = 15$ dB, the OP of DPSR approximately reach to $10^{-2.7}$, while the SPSBR with $\rho = 0.225$ and $\rho = 0.875$ impose 0.0025 and 0.0079, respectively. This is because the DPSR scheme aims to maximize the system capacity, thus it can improve the outage performance while the SPSR scheme always selects a fixed value of PS factor ρ . Second, the higher the Ψ value is, the better the OP can be obtained. It can be explained by the fact that the higher Ψ value means transmit power of source S is assigned more, which is defined in (24). In Fig. 4, the IP in both the DPSR and SPSR cases is studied, where $\eta = 0.8$, $C_{th} = 0.5$ bps/Hz, $M = 2$, $K = 1$, and $\Phi = 1$ dB. It can be seen that the intercept performance increases with a higher value of Ψ . It is anticipated because the eavesdropper has more ability to overhear the message with a higher source transmit power S_m . When the value of Ψ is large enough, the IP in all schemes can converge to 1. An interesting thing in Fig. 4 is

that the SPSR in S2 obtains better IP performance as compared to the case in the first scenario. When $-5 \leq \Psi \leq 1$, the IP value of SPSR with $\rho = 0.875$ is better than that of the SPSR with $\rho = 0.225$. Otherwise, when $\Psi > -1$ dB, the IP value of the SPSR with $\rho = 0.875$ is higher than that of SPSR with $\rho = 0.225$. As $-5 \leq \Psi \leq 0$ dB, the DPSR does not play a significant role compared with the other benchmarks since the PS factor ρ is only optimized for the received signal strength of a specific legitimate user. For the eavesdropper, the IP gets higher as the PS factor ρ gets larger, which is a consequence of the high transmit power of relay R. This observation is applied for all the considered benchmarks. In Figs. 3 and 4, simulations agree with the analytical values, which confirms our mathematical derivations' correctness.

In Figs. 5 and 6, we investigate security–reliability trade-off for S1 and S2 with the same parameter as in Figs. 3

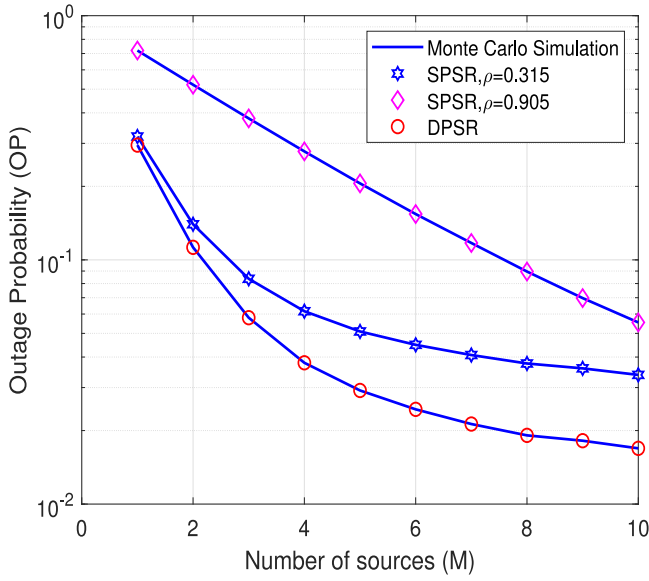


Fig. 7. OP versus number of sources (M) with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, and $\Psi = 2$ dB.

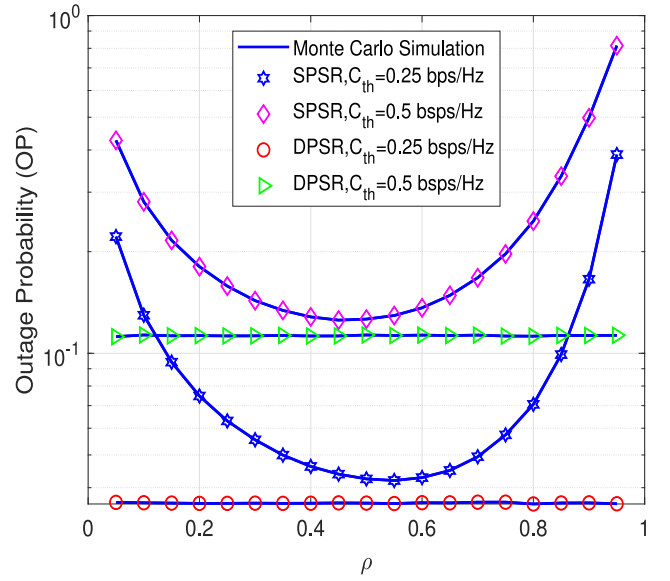


Fig. 9. OP versus ρ with $\eta = 0.8$, $M = 2$, $\Psi = 2$ dB, $\Phi = 1$ dB, and $K = 1$.

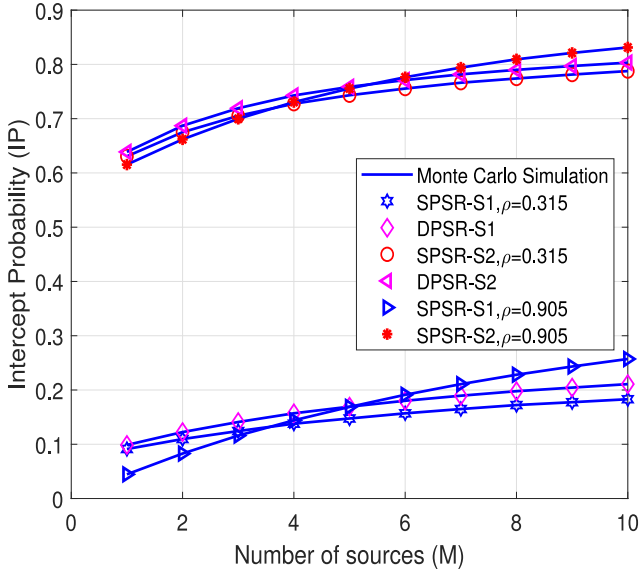


Fig. 8. IP versus number of sources (M) with $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, $K = 1$, $\Phi = 1$ dB, and $\Psi = 2$ dB.

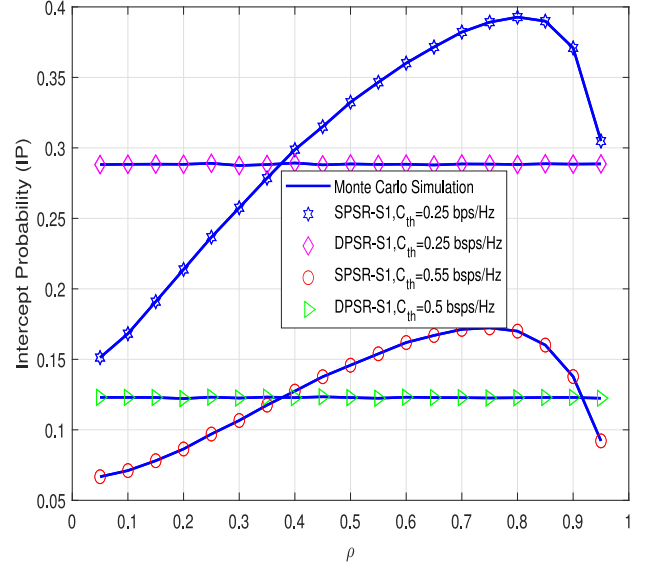


Fig. 10. IP versus ρ with $\eta = 0.8$, $M = 2$, and $\Psi = 2$ dB.

and 4. Nonetheless, these results demonstrate the benefits of our theoretical analysis. As observed in these figures, with increasing IP, the OP decrease and vice versa, indicating a tradeoff between security and reliability. Figs. 5 and 6 also shows that the DPSR method can provide the best IP and OP value. However, this requires us to tradeoff the choice that if we want the system obtains a better outage performance, it will be easier for the eavesdropper to steal information, on the contrary, if we want to restrict eavesdropping, we also reduce the outage performance.

Figs. 7 and 8 study the impact of the number of sources M on the OP and IP, respectively. Herein, simulation parameters are set as $C_{th} = 0.5$ bps/Hz, $\eta = 0.8$, $\Psi = 2$ dB, $K = 1$, and $\Phi = 1$ dB. Fig. 7 shows a better OP as the number of sources increases, i.e., M varies from 1 to 10. It is because, by increasing M , we will have more options to transmit information to

the destination and choose the best source S_m . Moreover, the OP of DPSR is still better than that of other SPSR cases. However, as shown in Fig. 8, the IP will also increase by using a larger number of sources. Once again, this shows the tradeoff between security and reliability.

In Figs. 9 and 10, we study OP and IP depending on different PS factor ρ , where $\eta = 0.8$, $M = 2$, $\Psi = 2$ dB, $\Phi = 1$ dB, and $K = 1$. The ρ value plays an important role since it influences not only the amount of harvested energy at the relay but also the data transmission from $R \rightarrow D$. Therefore, there exists an optimal value of PS factor ρ to maximize OP. Particularly, the OP of DPSR obtain the best performance compared to the two SPSR schemes since this method always optimizes the ρ value during the system design. It also explains for the fact that why the DPSR curves are straight lines because DPSR does not depend on ρ value. Besides, the DPSR scheme always obtains the best OP performance and that does not

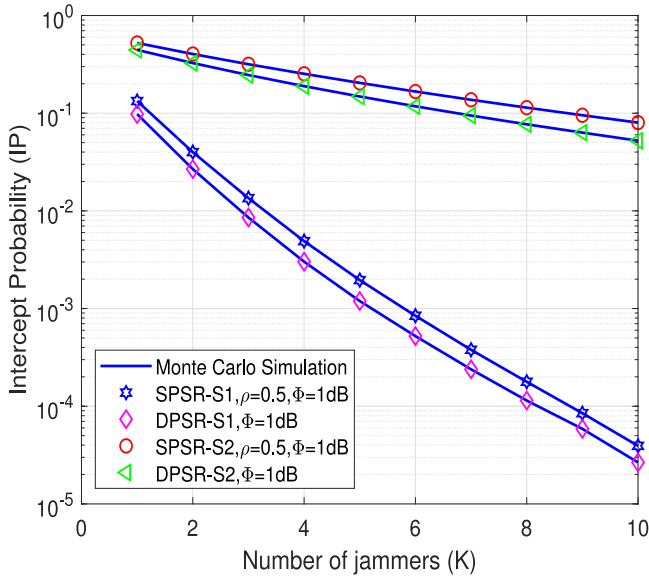


Fig. 11. IP versus number of jammers (K) with $\eta = 0.8$, $\rho = 0.5$, $M = 3$, and $\Psi = 2$ dB.

mean it will have the worst IP performance, which is verified in Fig. 10. This result is consistent with the result in Fig. 4. For instance, when $0.35 < \rho < 0.9$, the DPSR scheme has a better IP value than the SPSR scheme. In order to provide an explicit explanation, we first observe that the IP is directly proportional to the PS factor as $0.35 < \rho < 0.9$. In contrast, the DPSR yields the performance independent of the variation of ρ since this benchmark exploits the optimal value ρ^* as shown in Section III-B. Furthermore, it holds that $\rho^* < \rho$ on average and, therefore, the strength of the received signal by the DPSR is better than the SPSR. Consequently, the DPSR provides lower IP than the SPSR. Here again, the reliability-security tradeoff phenomenon also happens in both figures.

To reduce the IP as well as the eavesdropping ability of E, we will consider the effect of the number of jammers as shown in Fig. 11. In this figure, we can see that this will be consistent with reality because increasing K will cause more jamming signals to be sent to E and reduce its SNR ratio and its ability to overhear from the relay. Furthermore, in this figure, we compared DPSR with SPSR in IP analysis, while SPSR is considered in two cases with Φ equals -1 and 1 dB, respectively. It is easy to see that if the jammers' transmit power Φ is reduced, the jamming signal will be weaker and it is difficult to suppress the effect of the eavesdropping devices.

In Fig. 12, we investigate the IP as a function of Ψ (dB) for the case with and without jamming, where $\eta = 0.8$, $C_{th} = 0.5$ bps/Hz, $M = 2$, $K = 1$, $\rho = 0.55$, and $\Phi = 1$ dB. First, it can be observed from Fig. 12 that the intercept performance of the SPSR schemes is much better than that as compared to the DPSR ones, which has been explained in other figures. Furthermore, the intercept performance of the SPSR and DPSR with jamming is lower than that compared to without jamming scenarios. This is expected since the eavesdropper gains higher SNR in the case of no jamming signals. Thus, it has a higher probability to successfully decode

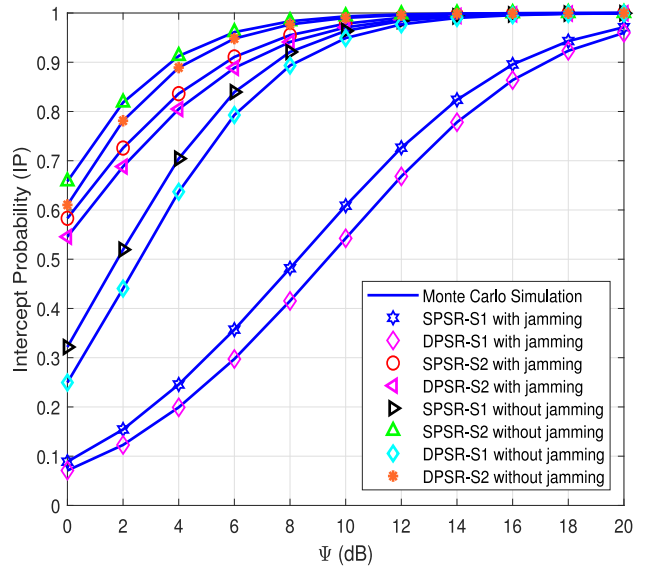


Fig. 12. IP versus Ψ with and without jamming cases.

the received signals from the source and relay. Specifically, when Ψ equals 2 and 4 dB, the IP of SPSR-S1 (or DPSR-S1) with jamming is 0.1542 (or 0.1228) and 0.2456 (or 0.1992), respectively. Meanwhile, the IP of the SPSR-S1 (or DPSR-S1) without jamming imposes 0.5194 (or 0.4404) and 0.7043 (or 0.6370), respectively. Moreover, the intercept performance of the S2 is better than that as compared to the S1. This is because the eavesdropper is located closer to sources in S2, thus it has a further distance to the jammer than the S1 case. Consequently, the jammer has less effect on the eavesdropper in S2 than S1 schemes.

V. CONCLUSION AND FUTURE DIRECTIONS

In this article, we have studied PLS for an AF-based SWIPT relay network consisting of multiple sources, multiple friendly jammers, an EH relay, and a destination in the presence of an eavesdropper. We have investigated the reliability-security tradeoff performance of DPSR and SPSR schemes in terms of the IP and OP. Furthermore, the impact of system parameters on network performance, and the correctness of the analytical expressions have been verified and investigated by using Monte Carlo simulations. Based on plots of the OP versus IP, we can recommend suitable system parameters to meet the predefined requirements on IP and OP. Particularly, a sufficient number of friendly jammers can significantly enhance system security by reducing the SNR at the eavesdropper. The results of this article can provide guidance for securing IoT networks in which the confidentiality in information transmission is important. An interesting topic for further exploration in this area is the extension to cases in which source and eavesdropping nodes have multiple antennas.

The outcome of this work will motivate a more general model that considers a direct link between source and destination, which imposes new challenges and complexities but might enhance network performance.

APPENDIX A

PROOF OF THEOREM 1

Based on the definition of the OP in (23) with the SNR in (12), OP_{SPSR} can be expressed as follows:

$$\begin{aligned} OP_{\text{SPSR}} &= \Pr\left(\frac{\eta\rho(1-\rho)\Psi\gamma_{S_mR}\gamma_{RD}}{\eta\rho\gamma_{RD} + (1-\rho)} < \gamma_{th}\right) \\ &= \Pr\left(\gamma_{S_mR} < \frac{\gamma_{th}(\eta\rho\gamma_{RD} + (1-\rho))}{\eta\rho(1-\rho)\Psi\gamma_{RD}}\right) \\ &= \int_0^\infty F_{\gamma_{S_mR}}\left\{\frac{\gamma_{th}(\eta\rho x + (1-\rho))}{\eta\rho(1-\rho)\Psi x}\right\} f_{\gamma_{RD}}(x) dx \end{aligned} \quad (29)$$

where the CDF of γ_{S_mR} is given in (20) and the PDF of $f_{\gamma_{RD}}(x)$ is given in (3). By utilizing (20), we obtain the following expression:

$$\begin{aligned} &F_{\gamma_{S_mR}}\left\{\frac{\gamma_{th}(\eta\rho x + (1-\rho))}{\eta\rho(1-\rho)\Psi x}\right\} \\ &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\eta\rho\Psi x} - \frac{b\lambda_{SR}\gamma_{th}}{(1-\rho)\Psi}\right). \end{aligned} \quad (30)$$

After that, by plugging (3) and (30) into (29), OP_{SPSR} can be represented as follows:

$$\begin{aligned} OP_{\text{SPSR}} &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\lambda_{th}}{(1-\rho)\Psi}\right) \\ &\quad \times \lambda_{RD} \int_0^\infty \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\eta\rho\Psi x} - \lambda_{RD}x\right) dx. \end{aligned} \quad (31)$$

With the help of [65, 3.324.1] and some algebraic manipulations, we obtain (24), which completes the proof.

APPENDIX B

PROOF OF THEOREM 2

Based on (15), (17), (18), and (25), the IP_{SPSR} can be rewritten by

$$\begin{aligned} IP_{\text{SPSR}} &= 1 - \Pr(\alpha < \gamma_{th}) \\ &= 1 - \int_0^\infty \Pr(\max(\vartheta_1, \vartheta_2) < \gamma_{th}) f_{\Xi}(x) dx \\ &= 1 - \int_0^\infty Q(x) f_{\Xi}(x) dx \end{aligned} \quad (32)$$

where $\alpha = \max([\Psi\gamma_{S_mE}]/[\Phi\Xi], [\eta\rho(1-\rho)\Psi\gamma_{S_mR}\gamma_{RE}]/[\eta\rho\gamma_{RE} + (1-\rho)\Phi\Xi + (1-\rho)])$ and the following definitions hold:

$$\vartheta_1 \triangleq \frac{\Psi\gamma_{S_mE}}{\Phi x} \quad (33)$$

$$\vartheta_2 \triangleq \frac{\eta\rho(1-\rho)\gamma_{S_mR}\gamma_{RE}\Psi}{\eta\rho\gamma_{RE} + (1-\rho)\Phi x + (1-\rho)} \quad (34)$$

$$\begin{aligned} Q(x) &\triangleq \Pr(\max(\vartheta_1, \vartheta_2) < \gamma_{th}) \\ &= \underbrace{\Pr(\vartheta_1 < \gamma_{th})}_{Q_1(x)} \times \underbrace{\Pr(\vartheta_2 < \gamma_{th})}_{Q_2(x)}. \end{aligned} \quad (35)$$

From (35), $Q_1(x)$ and $Q_2(x)$ can be calculated by

$$\begin{aligned} Q_1(x) &= \Pr\left(\frac{\Psi\gamma_{S_mE}}{\Phi x} < \gamma_{th}\right) = \Pr\left(\gamma_{S_mE} < \frac{\gamma_{th}\Phi x}{\Psi}\right) \\ &= 1 - \exp\left(-\frac{\gamma_{th}\lambda_{SE}\Phi x}{\Psi}\right) \end{aligned} \quad (36)$$

$$\begin{aligned} Q_2(x) &= \Pr\left(\frac{\eta\rho\rho_1\Psi\gamma_{S_mR}\gamma_{RE}}{\eta\rho\gamma_{RE} + \rho_1\Phi x + \rho_1} < \gamma_{th}\right) \\ &= \Pr\left\{\gamma_{S_mR} < \frac{\gamma_{th}(\eta\rho\gamma_{RE} + \rho_1\Phi x + \rho_1)}{\eta\rho\rho_1\gamma_{RE}\Psi}\right\} \\ &= \int_0^\infty F_{\gamma_{S_mR}}\left\{\frac{\gamma_{th}(\eta\rho y + \rho_1\Phi x + \rho_1)}{\eta\rho\rho_1\gamma_{RE}\Psi}\right\} f_{\gamma_{RE}}(y) dy \end{aligned} \quad (37)$$

where $\rho_1 \triangleq (1-\rho)$. By using the same approach as what has done in (30) to the last equation of (37), we obtain the closed-form expression of $Q_2(x)$

$$\begin{aligned} Q_2(x) &= 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\rho_1\Psi}\right) \\ &\quad \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} K_1\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}}\right). \end{aligned} \quad (38)$$

Following the same methodology as done to obtain the result in (24), we obtain the closed-form expression of $Q_2(x)$ as:

$$\begin{aligned} Q_2(x) &= 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\rho_1\Psi}\right) \\ &\quad \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} \times K_1\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}}\right). \end{aligned} \quad (39)$$

Based on (22), (36), and (39), the IP_{SPSR} in (32) can be reformulated as in (40), shown at the bottom of the next page, where $\tilde{\lambda}_{JE} = ([\gamma_{th}\lambda_{SE}\Phi]/\Psi) + \lambda_{JE}$. Thanks to [65, 3.381.4], Υ_1 in (40) can be calculated as follows:

$$\Upsilon_1 = \left(\frac{\lambda_{JE}}{\tilde{\lambda}_{JE}}\right)^K. \quad (41)$$

By applying Taylor series for $\exp(-\lambda_{JE}x) = \sum_{t=0}^\infty ([-\tilde{\lambda}_{JE}x]^t/t!) = \sum_{t=0}^\infty ([-1]^t(\tilde{\lambda}_{JE})^t/t!)x^t$ and by changing the variable $y = \Phi x + 1$, Υ_2 can be rewritten as follows:

$$\begin{aligned} \Upsilon_2 &= \sum_{t=0}^\infty \frac{(-1)^t(\tilde{\lambda}_{JE})^t}{t!\Phi^{t+K}} \int_1^\infty y^{1/2}(y-1)^{t+K-1} \\ &\quad \times K_1\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}y}{\eta\rho\Psi}}\right) dy. \end{aligned} \quad (42)$$

Next, by using [65, 6.592.4], the above equation can be reformulated by

$$\begin{aligned} \Upsilon_2 &= \sum_{t=0}^\infty \frac{(-1)^t(\tilde{\lambda}_{JE})^t \Gamma(t+K)}{t!\Phi^{t+K}} \times \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\rho\Psi}}\right)^{-1} \\ &\quad \times G_{1,3}^{3,0}\left(\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\rho\Psi} \middle| \begin{matrix} 0 \\ -t-K, 1, 0 \end{matrix}\right) \end{aligned} \quad (43)$$

where $\Gamma(\cdot)$ is the Gamma function and $G_{p,q}^{m,n}\left(z \middle| \begin{matrix} a_1, \dots, a_p \\ b_1, \dots, b_q \end{matrix}\right)$ is the Meijer G-function. By applying the same approach for (43), Υ_3 can be formulated as follows:

$$\Upsilon_3 = \sum_{t=0}^\infty \frac{(-1)^t(\lambda_{JE})^t \Gamma(t+K)}{t!\Phi^{t+K}} \times \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\rho\Psi}}\right)^{-1}$$

$$\times G_{1,3}^{3,0} \left(\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\rho\Psi} \middle| \begin{matrix} 0 \\ -t-K, 1, 0 \end{matrix} \right). \quad (44)$$

Finally, by substituting (41), (43), and (44), the IP_{SPSR} we obtain (26). This is the end of the proof.

APPENDIX C PROOF OF THEOREM 3

Substituting the optimal $\rho^* = (1/[1 + |h_{RD}|\sqrt{\eta}])$ into (29), the OP_{DPSR} is expressed as follows:

$$\begin{aligned} OP_{DPSR} &= \Pr \left(\frac{\eta\Psi\gamma_{S_mR}\gamma_{RD}}{(1 + \sqrt{\eta\gamma_{RD}})^2} < \gamma_{th} \right) \\ &= \Pr \left(\gamma_{S_mR} < \frac{\gamma_{th}(1 + 2\sqrt{\eta\gamma_{RD}} + \eta\gamma_{RD})}{\eta\Psi\gamma_{RD}} \right) \\ &= \int_0^\infty F_{\gamma_{S_mR}} \left(\frac{\gamma_{th}(1 + 2\sqrt{\eta x} + \eta x)}{\eta\Psi x} \right) \times f_{\gamma_{RD}}(x) dx \\ &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi} \right) \\ &\quad \int_0^\infty \lambda_{RD} \exp \left(-\frac{2b\lambda_{SR}\gamma_{th}}{\Psi\sqrt{\eta x}} \right) \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\eta\Psi x} - \lambda_{RD}x \right) dx. \end{aligned} \quad (45)$$

By adopting Taylor series for $\exp(-([2b\lambda_{SR}\gamma_{th}]/\Psi\sqrt{\eta x})) = \sum_{t=0}^\infty ((-1)^t 2^t / t!) ([b\lambda_{SR}\gamma_{th}]/[\Psi\sqrt{\eta}])^t x^{-t/2}$, (45) can be rewritten as follows:

$$\begin{aligned} OP_{DPSR} &= 1 + \sum_{t=0}^\infty \sum_{b=1}^M \frac{(-1)^{t+b} C_M^b 2^t \lambda_{RD}}{t!} \left(\frac{b\lambda_{SR}\gamma_{th}}{\Psi\sqrt{\eta}} \right)^t \\ &\quad \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi} \right) \int_0^\infty x^{-t/2} \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\eta\Psi x} - \lambda_{RD}x \right) dx. \end{aligned} \quad (46)$$

Finally, by applying [65, 3.471.9], we obtain (27), which finishes the proof.

APPENDIX D PROOF OF THEOREM 4

By substituting $\rho^* = (1/[1 + |h_{RD}|\sqrt{\eta}])$ into (32), Q_2^* can be calculated as follows:

$$\begin{aligned} Q_2^*(w) &= \Pr \left(\frac{\eta\gamma_{S_mR}\gamma_{RE}\Psi}{\eta\Phi_1\gamma_{RE} + \Phi_2\Phi x + \Phi_2} < \gamma_{th} \right) \\ &= \int_0^\infty \underbrace{\Pr \left(\frac{\eta\gamma_{S_mR}\gamma_{RE}\Psi}{\eta\Phi_3\gamma_{RE} + \Phi_4\Phi x + \Phi_4} < \gamma_{th} \right)}_{\Theta} f_{\gamma_{RD}}(\omega) d\omega \end{aligned} \quad (47)$$

where $\Phi_1 \triangleq ([1 + \sqrt{\gamma_{RD}\eta}]/[\sqrt{\gamma_{RD}\eta}])$, $\Phi_2 \triangleq 1 + \sqrt{\gamma_{RD}\eta}$, $\Phi_3 \triangleq ([1 + \sqrt{\eta w}]/[\sqrt{\eta w}])$, and $\Phi_4 \triangleq 1 + \sqrt{w\eta}$. Based on (21) and then with the help of [65, 3.324.1], Θ can be computed as follows:

$$\begin{aligned} \Theta(x) &= \Pr \left(\frac{\eta\gamma_{S_mR}\gamma_{RE}\Psi}{\eta\Phi_3\gamma_{RE} + \Phi_4\Phi x + \Phi_4} < \gamma_{th} \right) \\ &= \int_0^\infty \Pr \left(\gamma_{S_mR} < \frac{\gamma_{th}(\eta\Phi_3 z + \Phi_4\Phi x + \Phi_4)}{\eta z \Psi} \right) f_{\gamma_{RE}}(z) dz \\ &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}\Phi_3}{\Psi} \right) \\ &= 1 + \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}\Phi_3}{\Psi} \right) \\ &\quad \times \int_0^\infty \lambda_{RE} \exp \left(-\frac{b\lambda_{SR}\gamma_{th}(\Phi x + 1)\Phi_4}{\eta z \Psi} - \lambda_{RE}z \right) dz \\ &= 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}\Phi_3}{\Psi} \right) \\ &\quad \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)\Phi_4}{\eta\Psi}} \\ &\quad \times K_1 \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)\Phi_4}{\eta\Psi}} \right). \end{aligned} \quad (48)$$

$$\times K_1 \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)\Phi_4}{\eta\Psi}} \right). \quad (49)$$

$$\begin{aligned} IP_{SPSR} &= 1 - \int_0^\infty \left\{ 1 - \exp \left(-\frac{\gamma_{th}\lambda_{SE}\Phi x}{\Psi} \right) \right\} \left\{ \begin{array}{l} 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\rho_1\Psi} \right) \\ \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} \\ \times K_1 \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} \right) \end{array} \right\} \frac{(\lambda_{JE})^K}{(K-1)!} x^{K-1} \exp(-\lambda_{JE}x) dx \\ &= \underbrace{\frac{(\lambda_{JE})^K}{(K-1)!} \int_0^\infty x^{K-1} \exp(-x\tilde{\lambda}_{JE}) dx}_{\Upsilon_1} + 2 \sum_{b=1}^M (-1)^b C_M^b \exp \left(-\frac{b\lambda_{SR}\gamma_{th}}{\rho_1\Psi} \right) \\ &\quad \times \frac{(\lambda_{JE})^K}{(K-1)!} \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}}{\eta\rho\Psi}} \left\{ \begin{array}{l} \int_0^\infty x^{K-1} \exp(-x\tilde{\lambda}_{JE}) \times \sqrt{(\Phi x + 1)} \\ \times K_1 \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} \right) dx \\ \underbrace{\hspace{10em}}_{\Upsilon_2} \\ - \int_0^\infty x^{K-1} \exp(-\lambda_{JE}x) \sqrt{(\Phi x + 1)} \\ \times K_1 \left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\rho\Psi}} \right) dx \\ \underbrace{\hspace{10em}}_{\Upsilon_3} \end{array} \right\} \end{aligned} \quad (40)$$

By substituting (48) into (22), the term Q_2^* can be reformulated as follows:

$$Q_2^*(w) = 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi}\right) \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\Psi}} \times \lambda_{RD} \int_0^\infty \frac{\sqrt{1 + \sqrt{\eta\omega}} \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi\sqrt{\eta\omega}} - \lambda_{RD}\omega\right)}{K_1\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)(1 + \sqrt{\eta\omega})}{\eta\Psi}}\right)} d\omega \quad (50)$$

$$= 1 + 2 \sum_{b=1}^M (-1)^b C_M^b \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi}\right) \times \sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)}{\eta\Psi}} \times \Delta(\omega) \quad (51)$$

where the following definition holds:

$$\Delta(\omega) \triangleq \lambda_{RD} \int_0^\infty \frac{\sqrt{1 + \sqrt{\eta\omega}} \exp\left(-\frac{b\lambda_{SR}\gamma_{th}}{\Psi\sqrt{\eta\omega}} - \lambda_{RD}\omega\right)}{K_1\left(2\sqrt{\frac{b\lambda_{SR}\lambda_{RE}\gamma_{th}(\Phi x + 1)(1 + \sqrt{\eta\omega})}{\eta\Psi}}\right)} d\omega. \quad (52)$$

Finally, based on (32), (36), and (50), we claim (28), which completes the proof.

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