

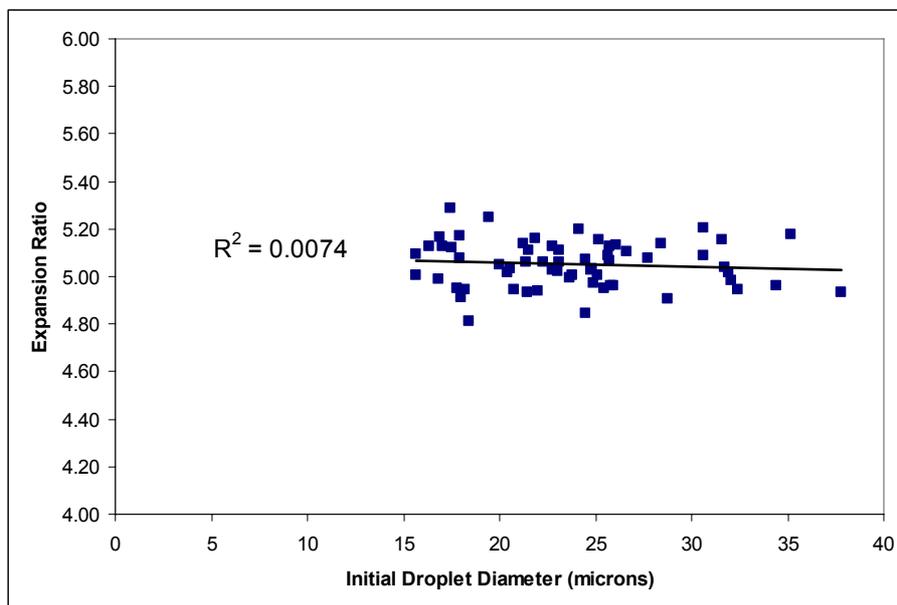
Electronic Supplemental Information for

Bubble Evolution in Acoustic Droplet Vaporization at Physiological Temperature via Ultra-High Speed Imaging

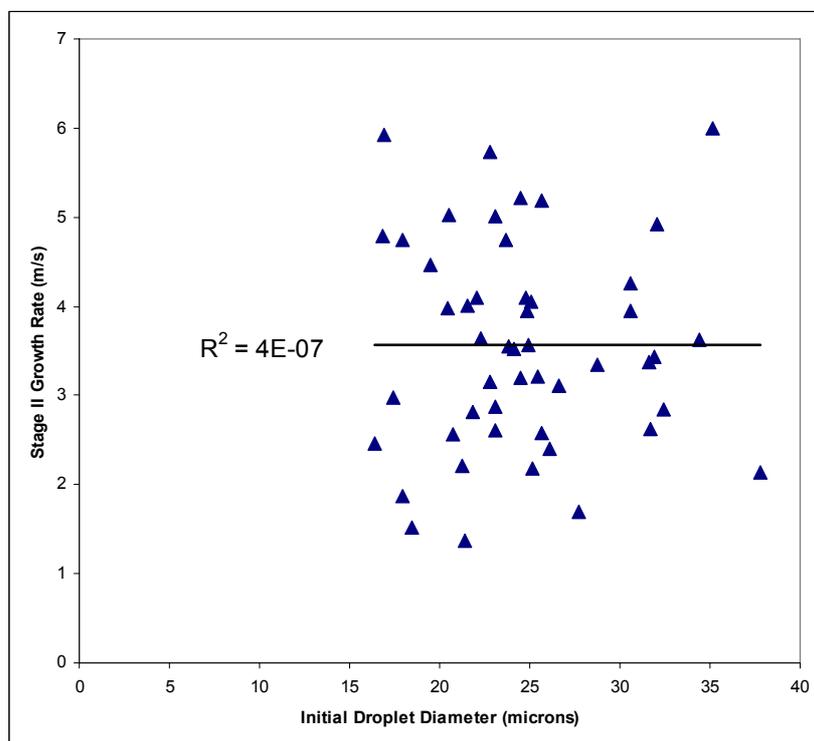
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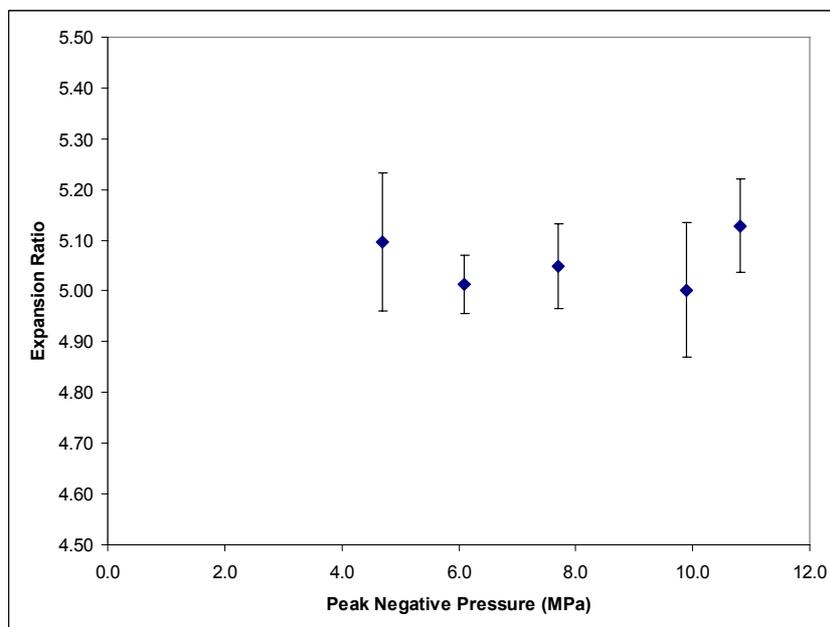
Supplementary Information (deposited electronically on journal website)



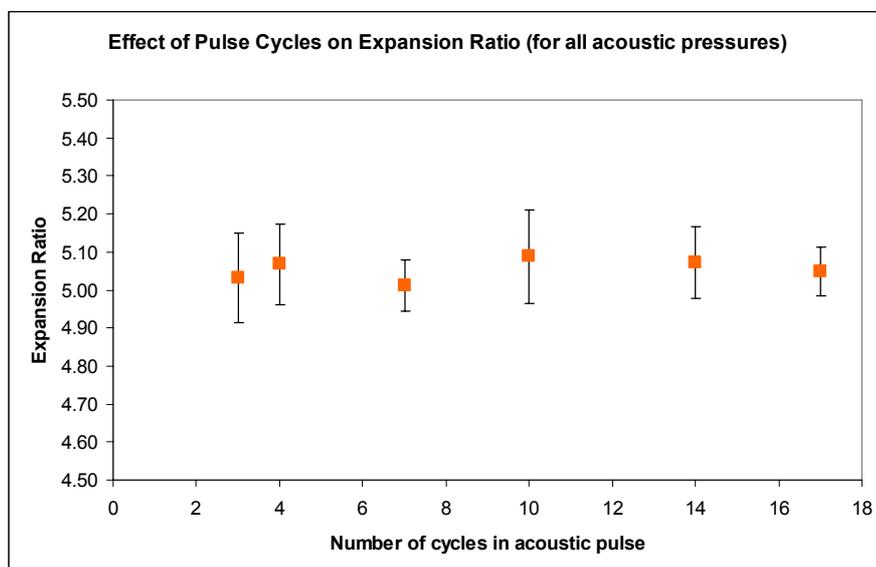
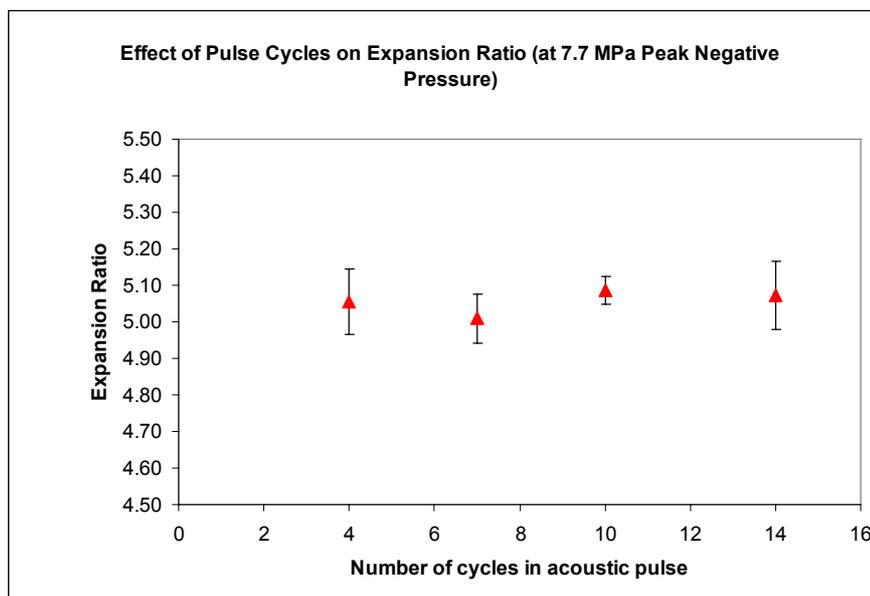
Effect of initial droplet size on the expansion ratio



Effect of initial droplet size on Stage II linear growth rate



Effect of acoustic pressure on expansion ratio



At 7.7 MPa			T-Test p value						
No. Cycles	Exp Ratio	Std Dev	4	7	10	14			
4	5.06	0.088444	NA	0.180	0.437	0.762			
7	5.01	0.067961		NA	0.122	0.299			
10	5.09	0.037594			NA	0.805			
14	5.07	0.094202				NA			
All acoustic pressures			T-Test p value						
No. Cycles	Exp Ratio	Std Dev	3	4	7	10	14	17	
3	5.03	0.117652	NA	0.573	0.730	0.467	0.597	0.808	
4	5.07	0.105262		NA	0.047	0.708	0.924	0.649	
7	5.01	0.067682			NA	0.199	0.304	0.370	
10	5.09	0.121375				NA	0.823	0.525	
14	5.07	0.094202					NA	0.696	
17	5.05	0.064227						NA	
			T-Test p value						
M-Pa	Exp Ratio	Std Dev	4.7	6.1	7.7	9.9	10.8		
4.7	5.10	0.135921	NA	0.246	0.481	0.247	0.722		
6.1	5.01	0.057512		NA	0.150	0.828	0.011		
7.7	5.05	0.08309			NA	0.361	0.055		
9.9	5.00	0.132814				NA	0.052		
10.8	5.12	0.086662					NA		

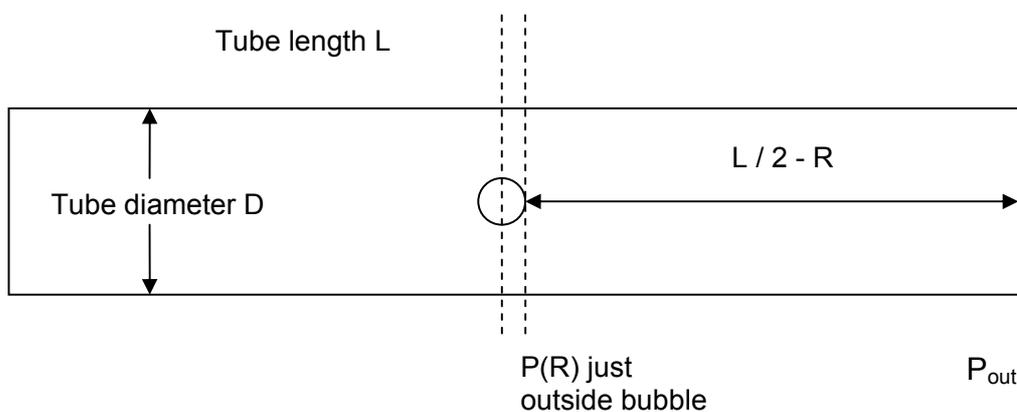
Statistical T-test (two-sided) for Independence of Means

Simplified model of bubble expansion in a tube (details of derivation)

Modified Bernoulli equation (obtain same results if start from conservation of momentum too)

$$\rho \int_{l_1}^{l_2} \frac{\partial \bar{V}}{\partial t} ds + \rho g h_L = P_1 - P_2 \quad (1)$$

P=pressure, \bar{V} = cross-sectional average velocity, s is streamline coordinate, ρ =liquid density, g =acceleration due to gravity, and h_L = head loss



Apply between point ~ at bubble surface to tube outlet, e.g. R to $L/2$

Assume laminar flow in liquid between bubble and tube outlet to estimate head loss term.

$$\rho g h_L = \frac{64}{\text{Re}} \frac{l}{D} \frac{\rho \bar{V}^2}{2} = \frac{32\mu}{D^2} \left(\frac{L}{2} - R \right) \bar{V} \quad (2)$$

Where D =tube diameter, R =bubble radius, L =tube length.

Conservation of mass for entire tube

$$\frac{d}{dt} \left[\frac{L\pi D^2}{4} - \frac{4\pi R^3}{3} \right] = -\beta Q = -\beta \bar{V} \frac{\pi D^2}{4} \quad (3)$$

where β is the number of outlets (1 or 2)

Rearranging yields

$$\bar{V} = \frac{16}{\beta D^2} R^2 \frac{dR}{dt} \quad (4)$$

$$\frac{d\bar{V}}{dt} = \frac{16}{\beta D^2} \left[R^2 \frac{d^2 R}{dt^2} + 2R \left(\frac{dR}{dt} \right)^2 \right] \quad (5)$$

Pressure jump at the bubble interface (Young-Laplace for moving interface)

$$P(R) = P_{B0} \left(\frac{R_0}{R} \right)^{3\gamma} - \frac{4\mu}{R} \frac{dR}{dt} - \frac{2\sigma}{R} \quad (6)$$

where $P(R)$ is pressure in the liquid at the bubble surface, P_{B0} is initial bubble pressure, $\gamma = 1$ for isothermal expansion (used) or close to 1 for adiabatic expansion of DDFP (1.4 for air), R_0 = initial bubble diameter

Substituting equations (2), (4), (5), and (6) into equation (1) yields

$$\frac{16\rho}{\beta D^2} \left(\frac{L}{2} - R \right) \left[R^2 \frac{d^2 R}{dt^2} + 2R \left(\frac{dR}{dt} \right)^2 \right] + \frac{512\mu}{\beta D^4} \left(\frac{L}{2} - R \right) R^2 \frac{dR}{dt} = P_{B0} \left(\frac{R_0}{R} \right)^{3\gamma} - \frac{4\mu}{R} \frac{dR}{dt} - \frac{2\sigma}{R} - P_{out}$$

Solved with the following parameter values (modifications from these noted in graph):

$\rho = 993.3 \text{ kg/m}^3$
 $\mu = 6 \times 10^{-4} \text{ Ns/m}^2$
 $\sigma = 70 \times 10^{-3} \text{ N/m}$
 $P_{out} = 101300 \text{ Pa}$
 $P_{B0} = 14.6 \times 10^6 \text{ Pa}$

L=16cm

Assumptions:

- Ignores details of flow very close to bubble
- One-dimensional flow model
- Neglect “minor losses”
- Tube length approximation
- Some parameters approximated (e.g. P_{B0} , σ)