

The Finite Cell Method: High order simulation of complex structures without meshing

E. Rank, A. Düster, D. Schillinger, Z. Yang

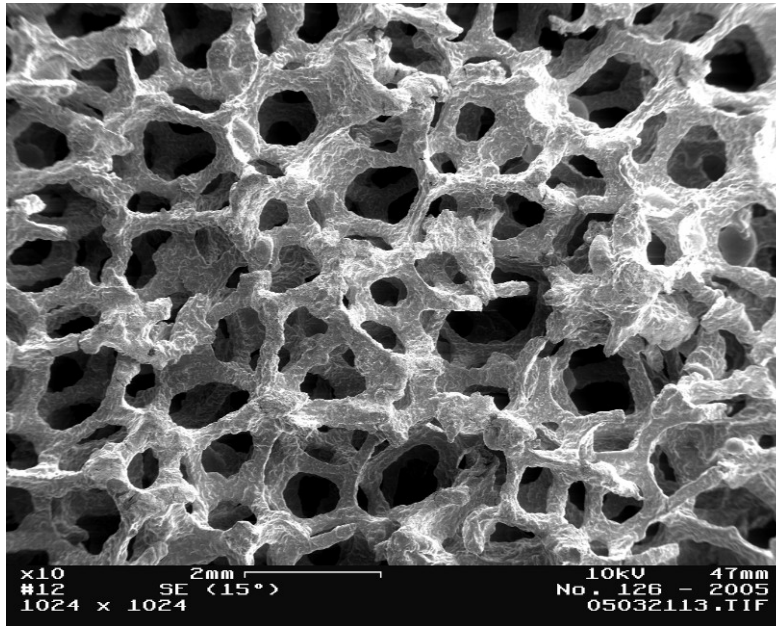
**Fakultät für Bauingenieur- und Vermessungswesen
Technische Universität München, Germany**

U. Råde, N. Thürey, T. Pohl , S. Donath, D. Bartuschat, C. Körner

**Technische Fakultät der
Universität Erlangen-Nürnberg, Germany**

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Metal foams



From: Wikipedia

Goal: Virtual material design

Obtain mechanical properties from process parameters of foam generation

Step 1: Simulation of foam generation

(Lattice Boltzmann Method)

Step 2: (Microscopic) structural simulation

to obtain mechanical properties

(Finite Cell Method)

Overview

- Motivation
- Foam generation by the Lattice Boltzmann method
- High order finite cell method: Basic principles
- Accuracy considerations
- Application to porous structures
- Summary

Lattice-Boltzmann simulation

$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho_0} \nabla P + \nu \nabla^2 \mathbf{u}$$

Partial differential equations (Navier–Stokes)

Discretization

e.g. Finite Difference /
Finite Volume equations

Multi-scale analysis

Discrete model
(LGCA or LBM)

The Boltzmann equation:

$$\frac{\partial f}{\partial t} + \xi \frac{\partial f}{\partial x} = Q(f, f)$$

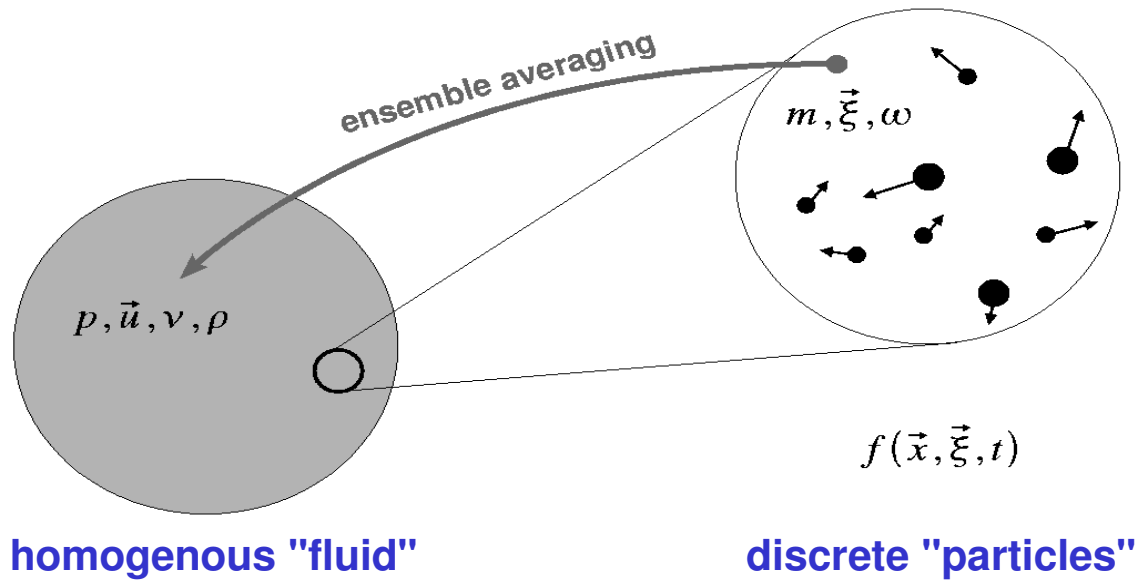
t : time

x : spatial coordinate

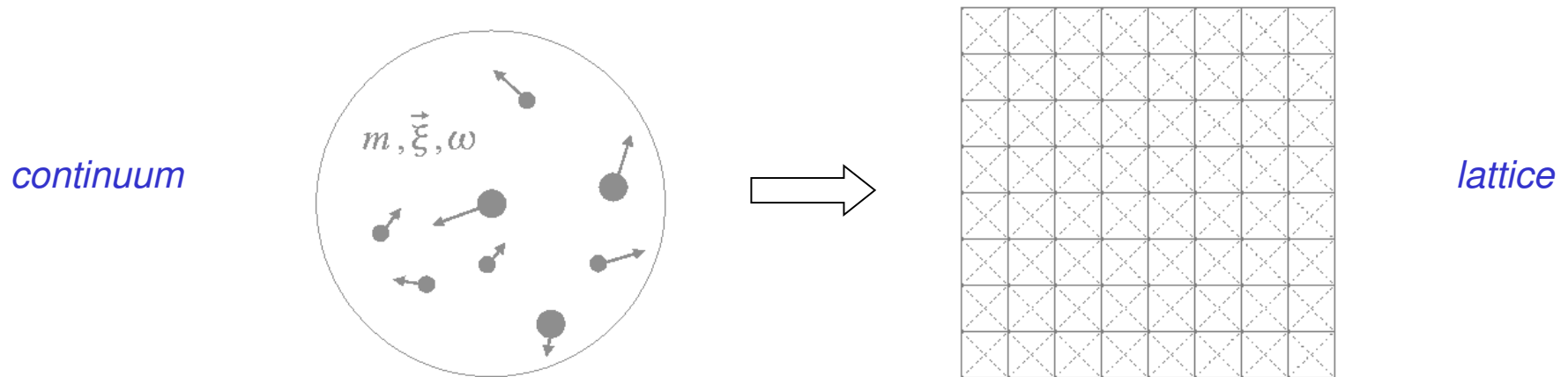
ξ : particle velocity

f : Probability to find a particle with velocity ξ at time t and position x

Q : Collision operator



- Simulate multi-particle system behaviour through **artificial microworlds of particles** residing on a computational lattice



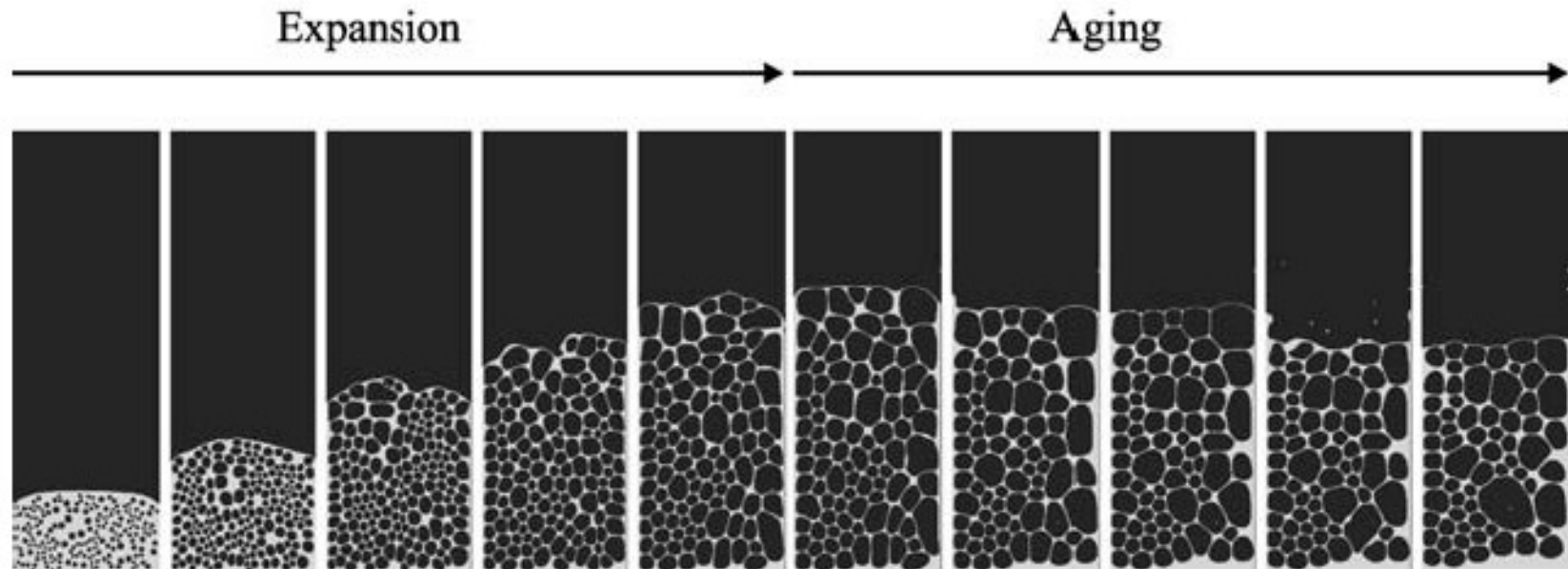
- Approximate Boltzmann equation on a lattice with FD-method

$$f_i(\vec{x} + \vec{e}_i \delta t, t + \delta t) - f_i(\vec{x}, t) = -\frac{1}{\tau} \left(f_i(\vec{x}, t) - f_i^{eq}(\vec{x}, t) \right) + F_i$$

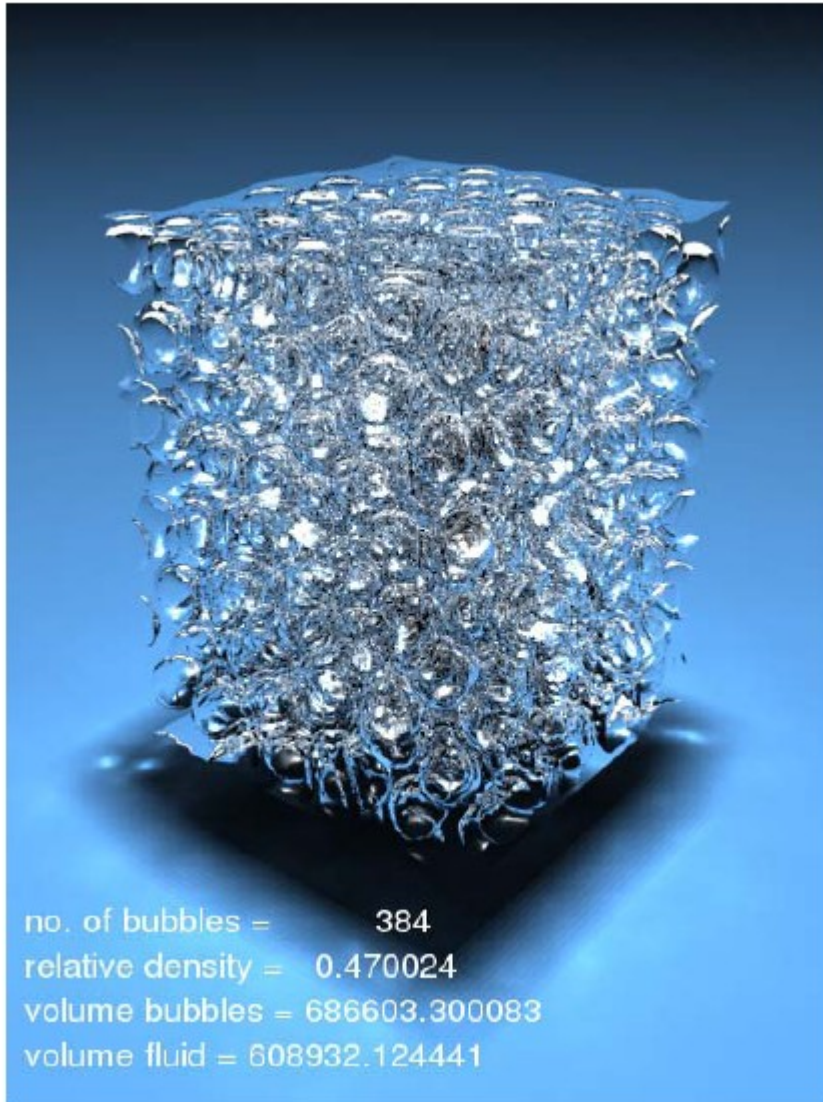
Extension to free surface flow

C. Körner, M. Thies, T. Hofmann, N. Thürey, and U. Rüde:
Journal of Statistical Physics, Vol 121, 2005

- Two phases: Gas and liquid
- Surface capturing method
- Volume of fluid approach



C. Körner, M. Thies, T. Hofmann, N. Thürey, and U. Rüde:
Journal of Statistical Physics, Vol 121, 2005



Idea:

- ‚Virtual‘ material tests to predict macroscopic mechanical properties (e.g. tension and shear test)

Problem:

- Mesh generation!

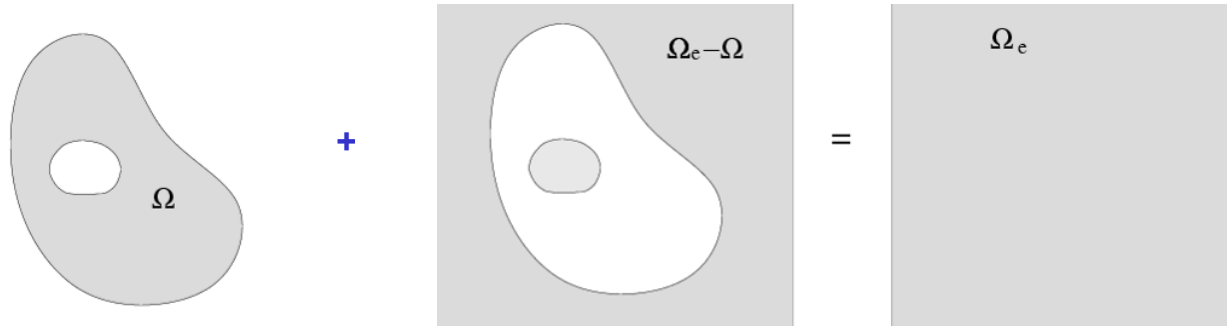
Our approach:

- Finite Cell Method for mesh-free structural simulation

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Finite Cell Method (FCM): The basic formulation



$$\mathcal{B}(\mathbf{u}, \mathbf{v}) = \mathcal{F}(\mathbf{v})$$

$$\mathcal{B}(\mathbf{u}, \mathbf{v}) = \int_{\Omega} [\mathbf{L} \mathbf{v}]^T \mathbf{C} [\mathbf{L} \mathbf{u}] d\Omega$$

$$\mathcal{F}(\mathbf{v}) = \int_{\Omega} \mathbf{v}^T \mathbf{f} dx dy + \int_{\Gamma_N} \mathbf{v}^T \mathbf{t}_N d\Gamma$$

exact solution: \mathbf{u}_{ex}

$$\mathcal{B}_e(\mathbf{u}, \mathbf{v}) = \mathcal{F}_e(\mathbf{v})$$

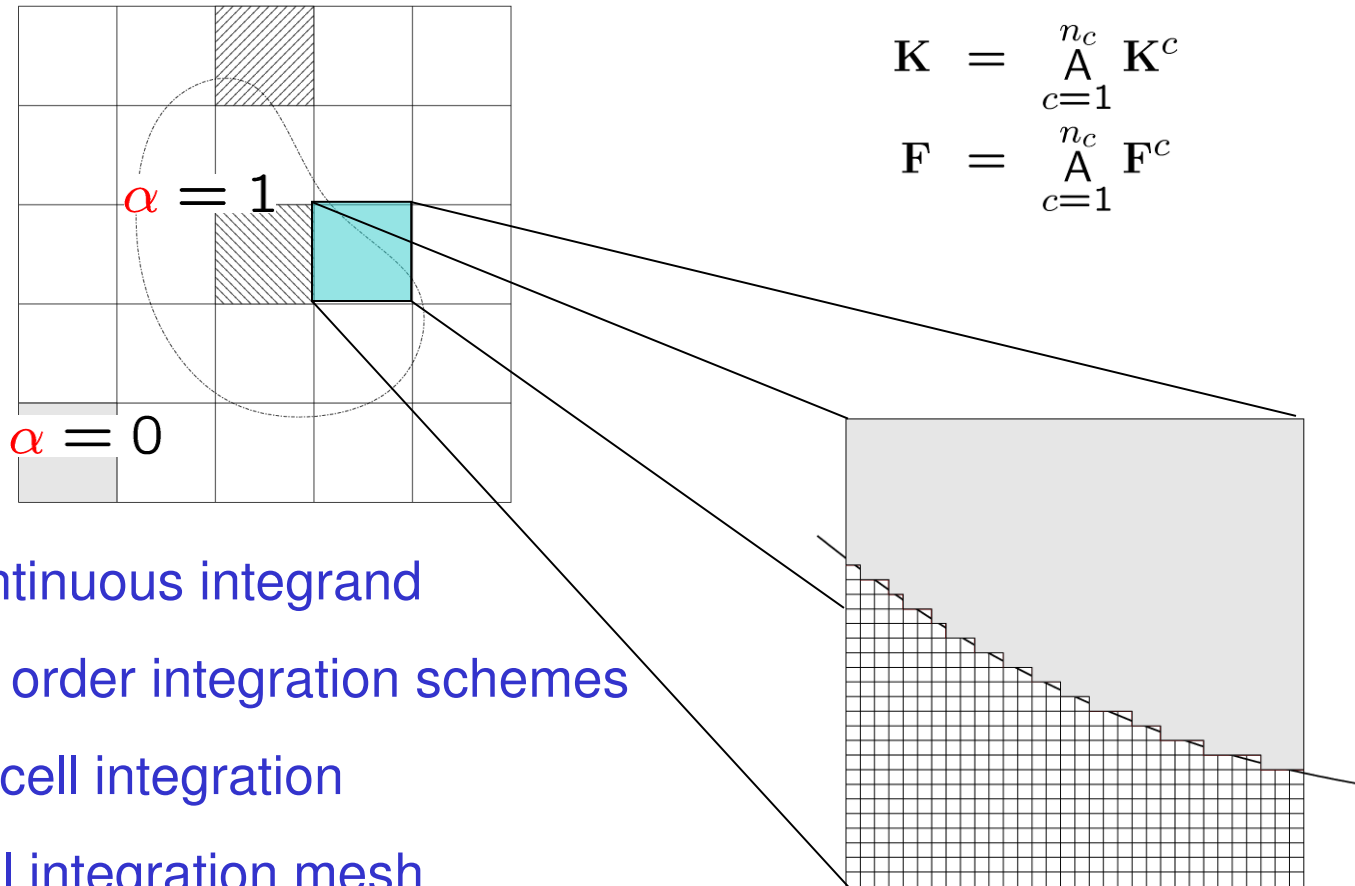
$$\mathcal{B}_e(\mathbf{u}, \mathbf{v}) = \int_{\Omega_e} [\mathbf{L} \mathbf{v}]^T \mathbf{C}_e [\mathbf{L} \mathbf{u}] d\Omega$$

$$\mathbf{C}_e = \begin{cases} \mathbf{C} & \text{in } \Omega \\ \mathbf{C}^2 & \text{in } \Omega_e \setminus \Omega \end{cases}$$

exact solution: $\mathbf{u}_{e,ex}$

$$\text{'zero extension': } \mathcal{B}_e(\mathbf{u}, \mathbf{v}) = \int_{\Omega_e} [\mathbf{L} \mathbf{v}]^T \alpha \mathbf{C} [\mathbf{L} \mathbf{u}] d\Omega \quad \alpha = \begin{cases} 1.0 & \text{in } \Omega \\ 0.0 & \text{in } \Omega_e \setminus \Omega \end{cases}$$

- A ‘cell’ is a finite element on the *extended domain* which needs yet *not conform* with the *boundary of the original domain*
- Discretization by finite element shape functions on ‘cells’



Discontinuous integrand

- High order integration schemes
- Sub-cell integration
- Local integration mesh

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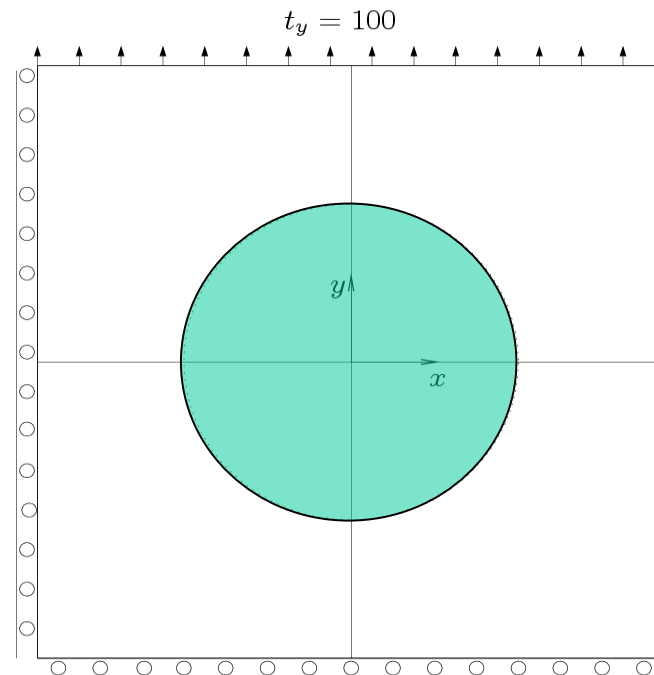
Assumptions:

- The structure consists of (homogeneous or inhomogeneous) material with (uniformly or randomly) distributed voids on the microscale
- Singularities do *not* play a dominant role on the microscale

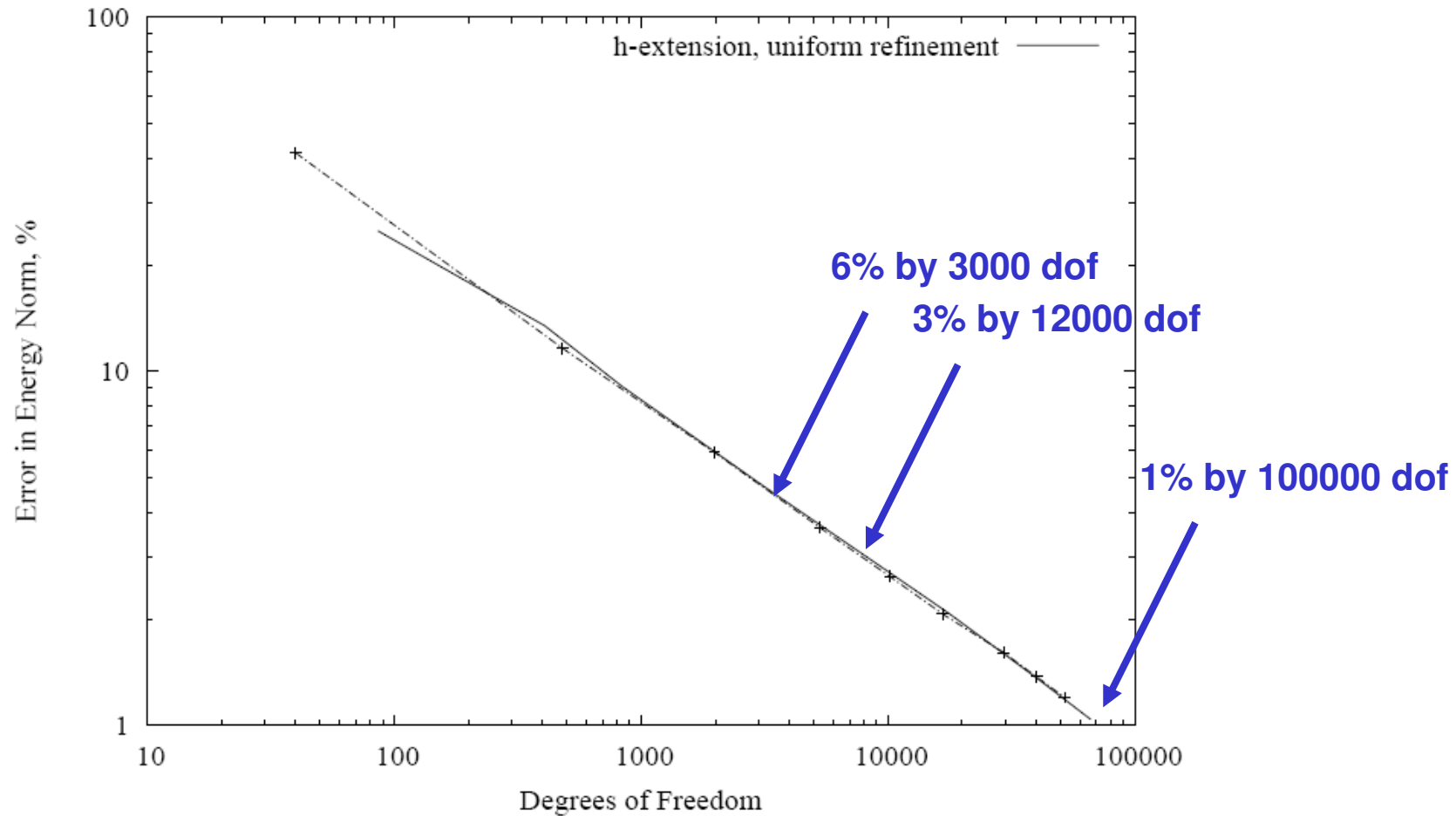
Question:

- What is, for a given desired energy norm error, the ratio of degrees of freedom between FCM and classical FEM (h-extension) ?

Model problem for investigating the energy error per unit pore

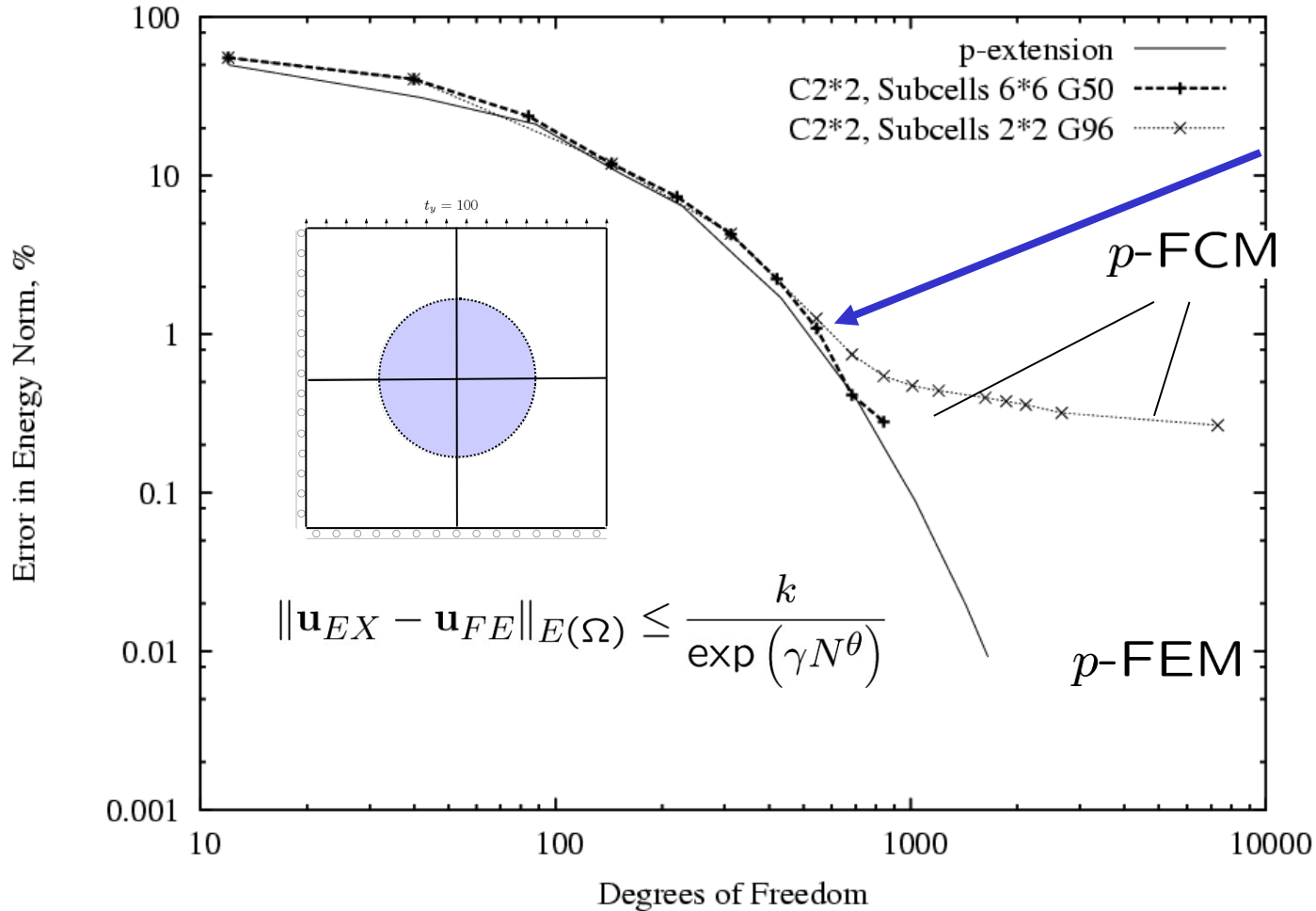


h-extension

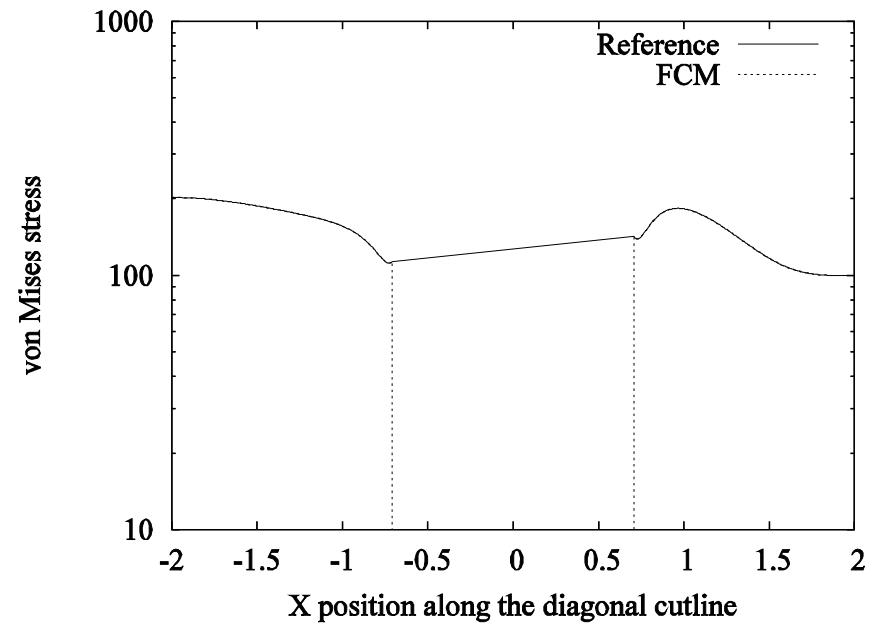
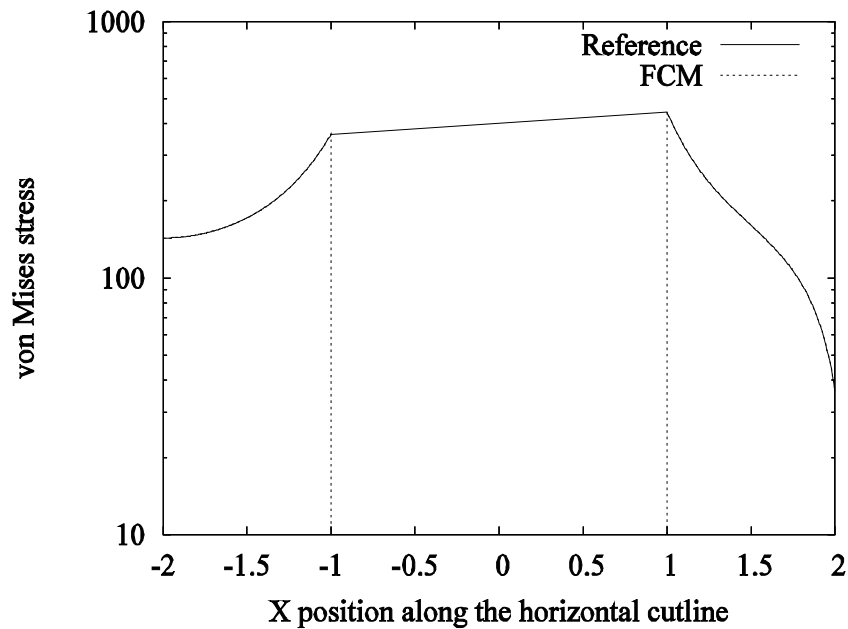


Finite Cell Method: 4 cells, p -extension

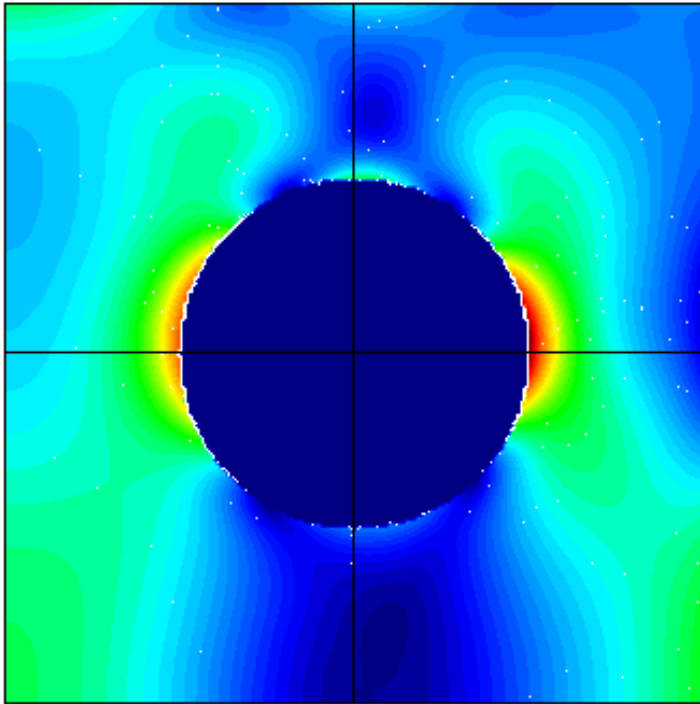
1% by 500 dof



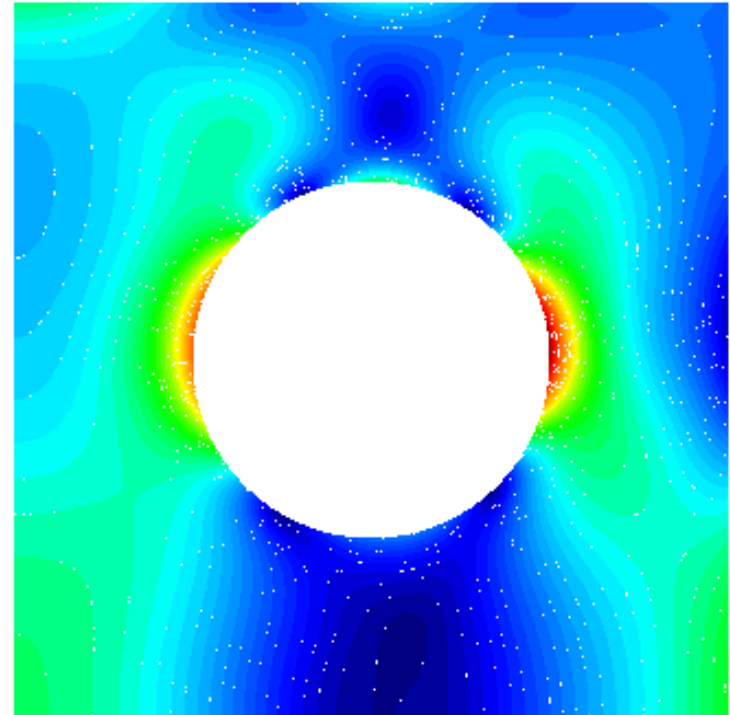
von Mises stress along the cut-lines



von Mises contours



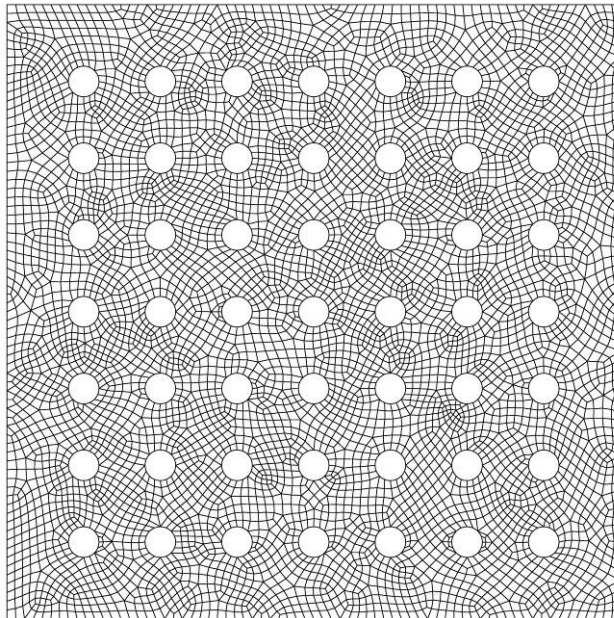
Finite Cell method



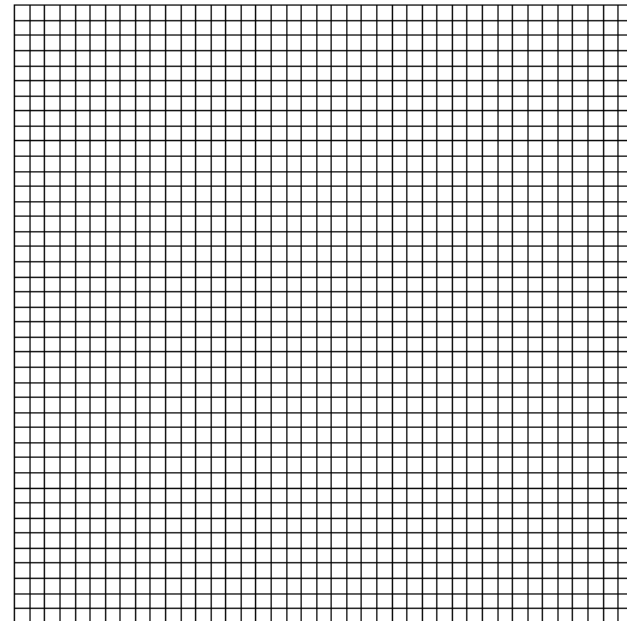
Reference Solution (p-FEM)

Tensile plate with many inclusions

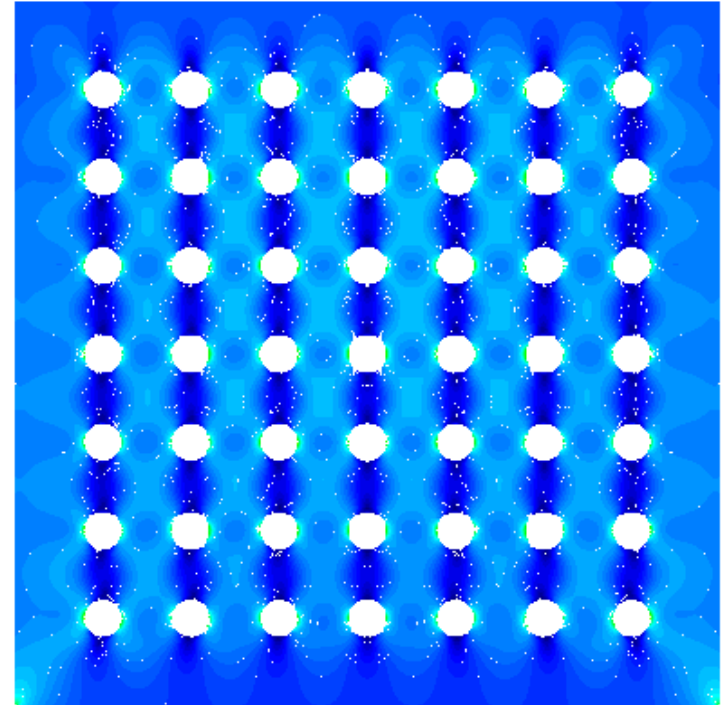
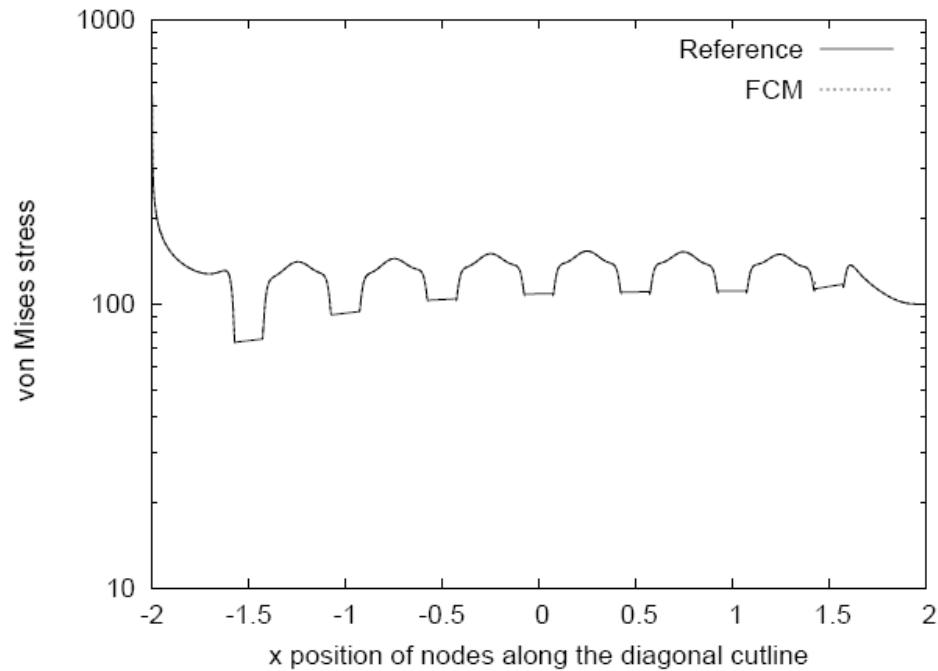
Finite element mesh



Finite cell mesh



Tensile plate with many inclusions

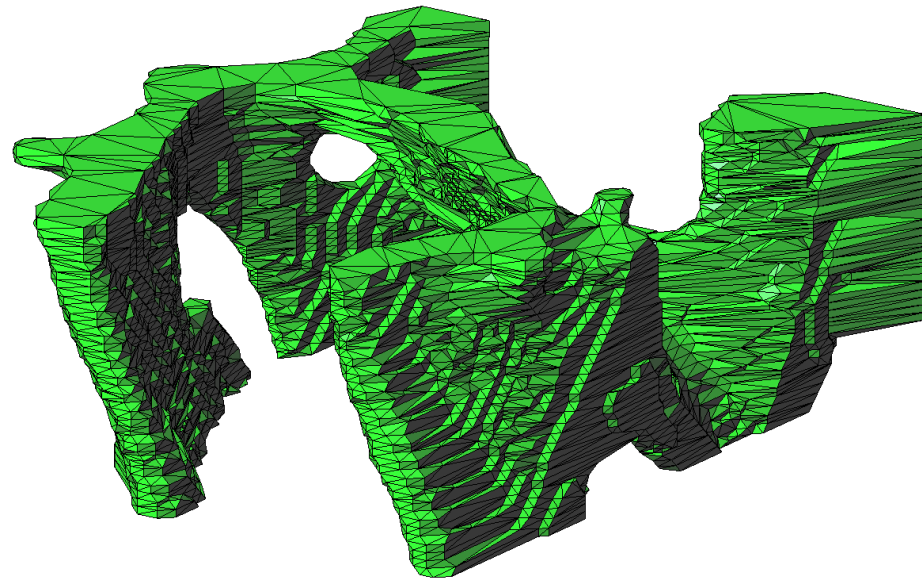


Error in von Mises stresses nowhere larger than 1%

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A 3D-example: X-ray MicroCT examination of human bone



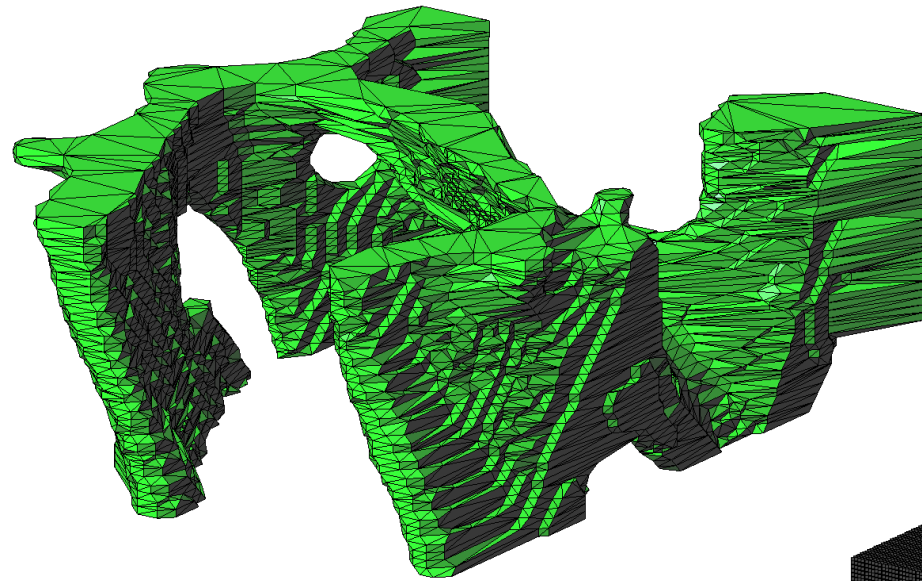
Human bone
biopsy, taken from
the femoral neck

Geometry:

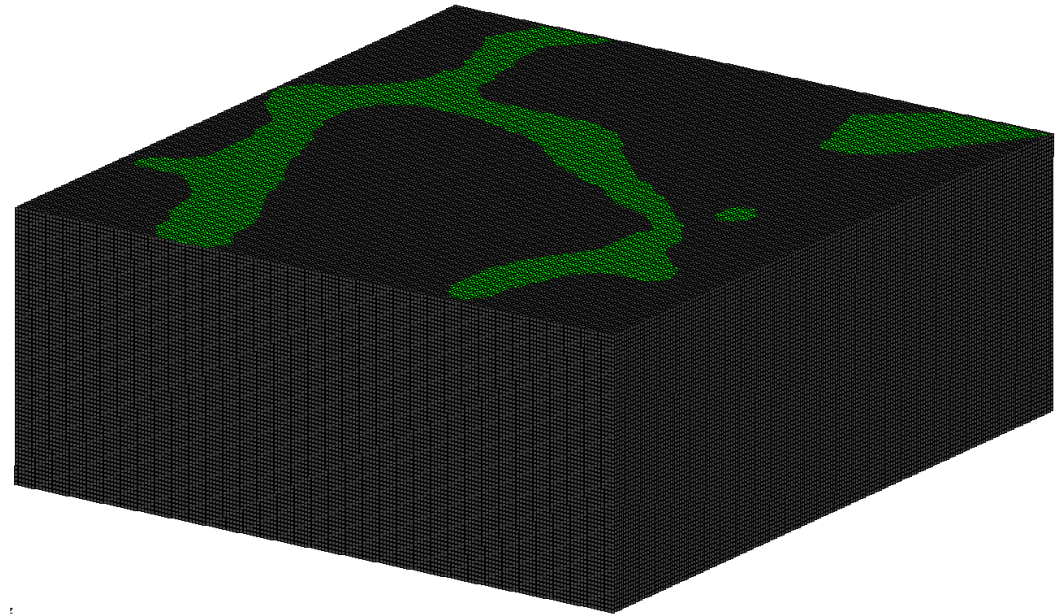
10mm × 6mm × 5mm

Baruffaldi, Perilli, Bn_326, from: *The BEL Repository*, <http://www.techno.ior.it/VRLAB>
Istituti Ortopedici Rizzoli, Bologna, Italy

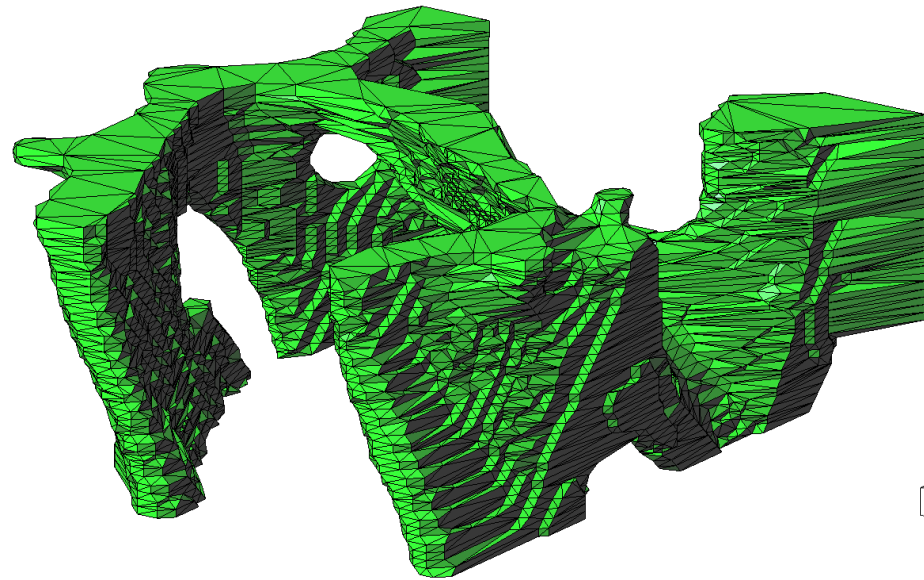
Voxel model



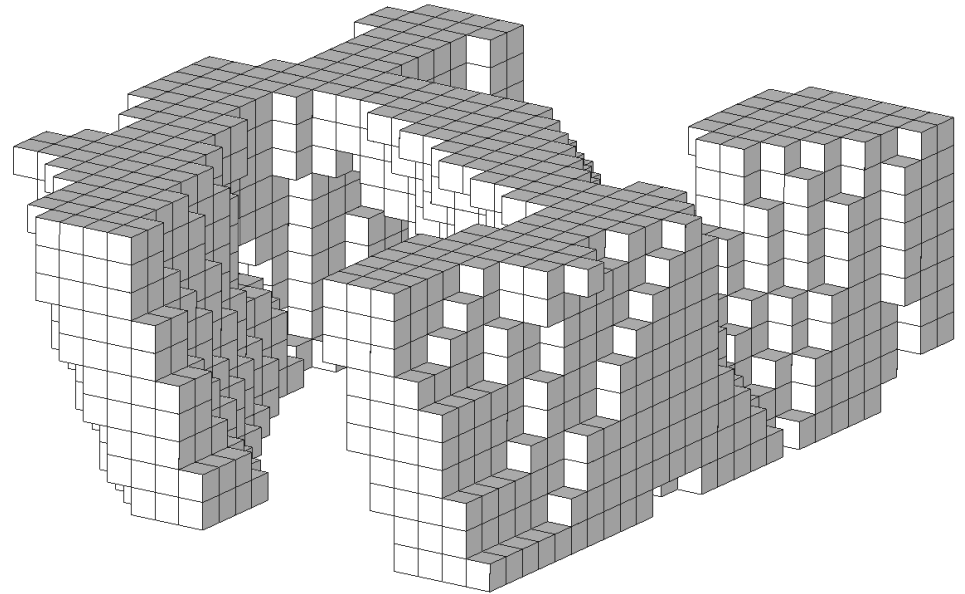
190 x 176 x 71 voxel



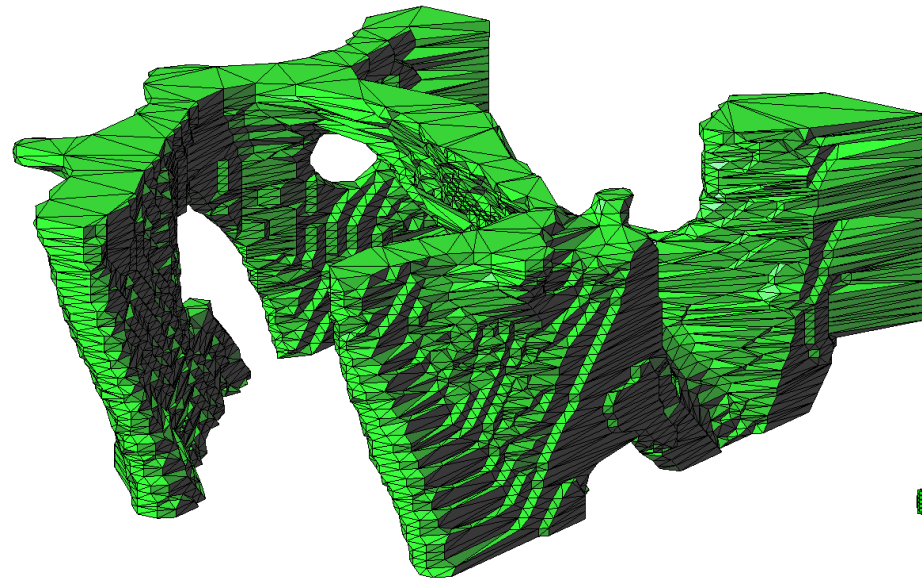
Finite Cells



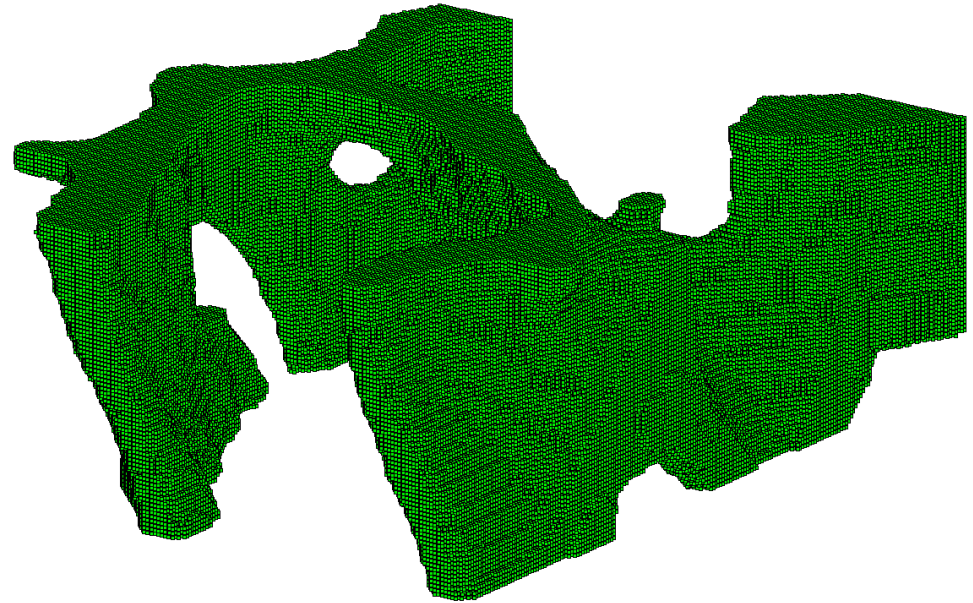
2412 hexahedrals (cells)



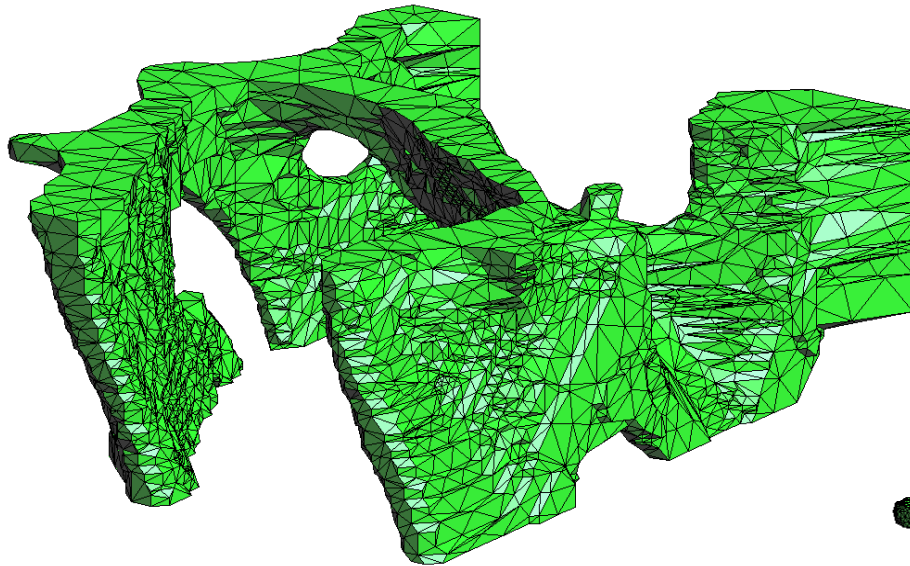
Voxel model



190 x 176 x 71 voxel



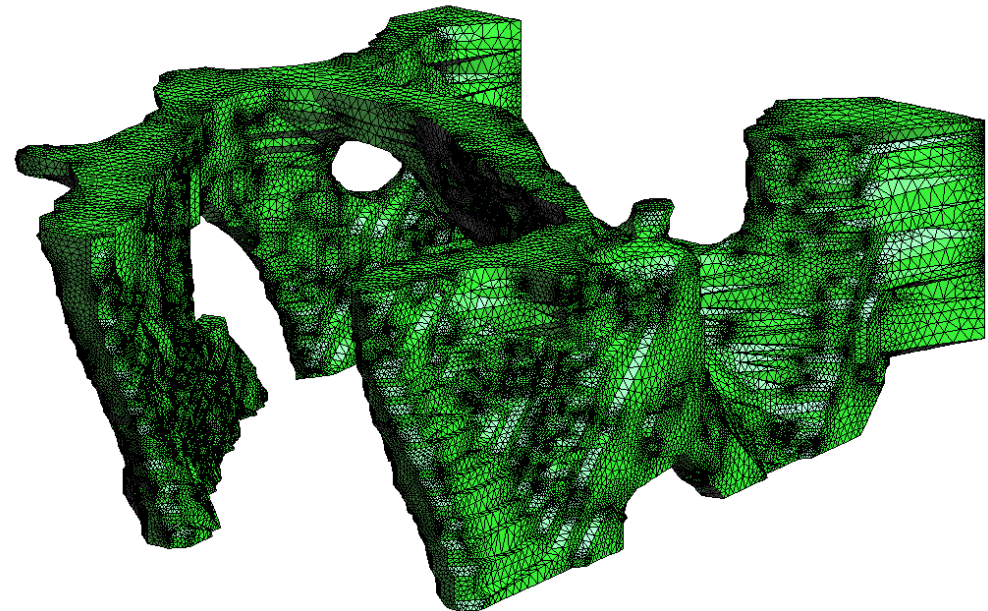
Reference solution based on the FEM (Abaqus, Netgen)



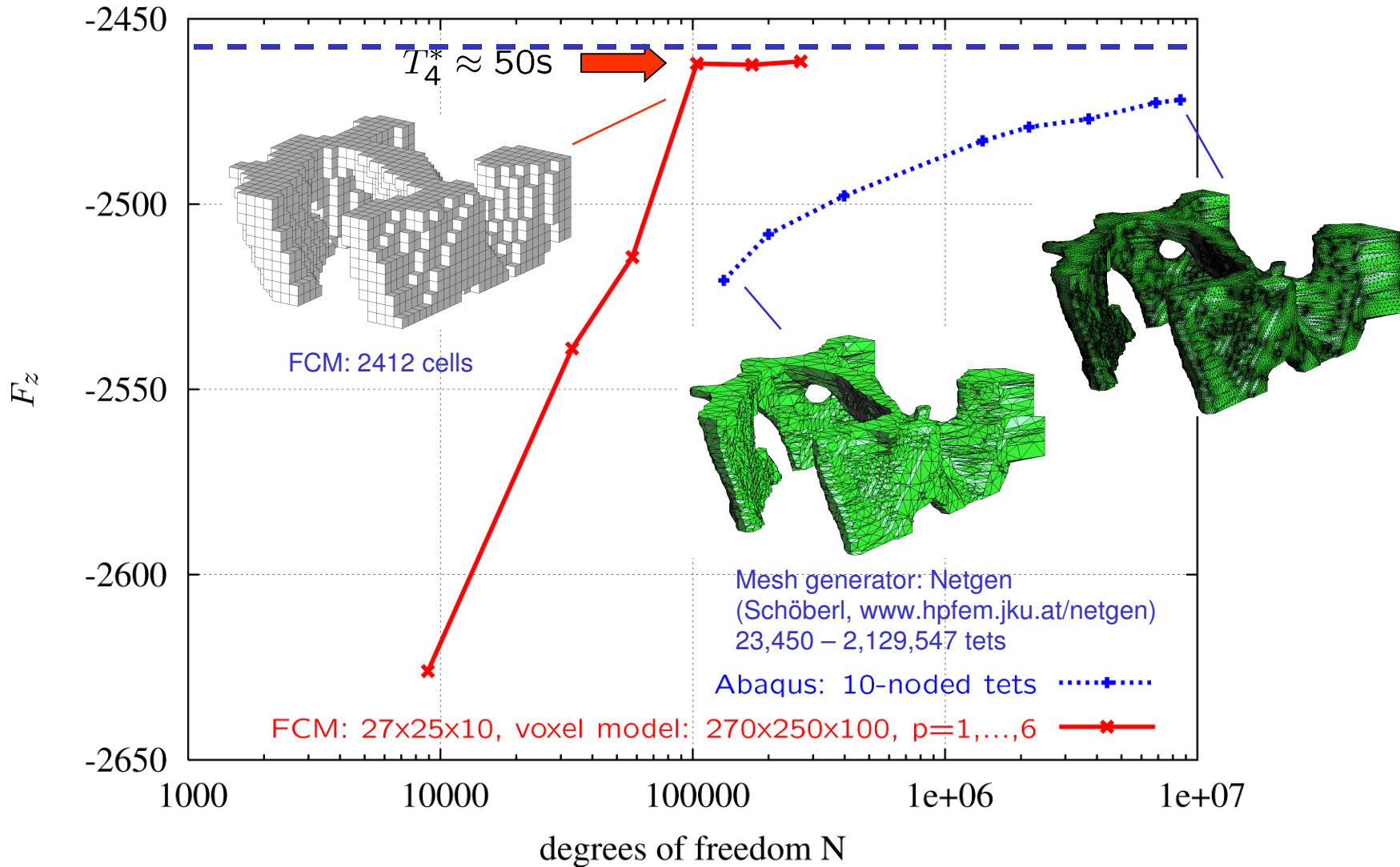
Netgen
(Schöberl, www.hpfem.jku.at/netgen)

23,450 – 2,129,547

quadratic tetrahedral
(10-noded) elements



*Intel® Xeon® E5405 (2,00 GHz, 1.333 MHz, 2 x 6 MB, Quad-Core)

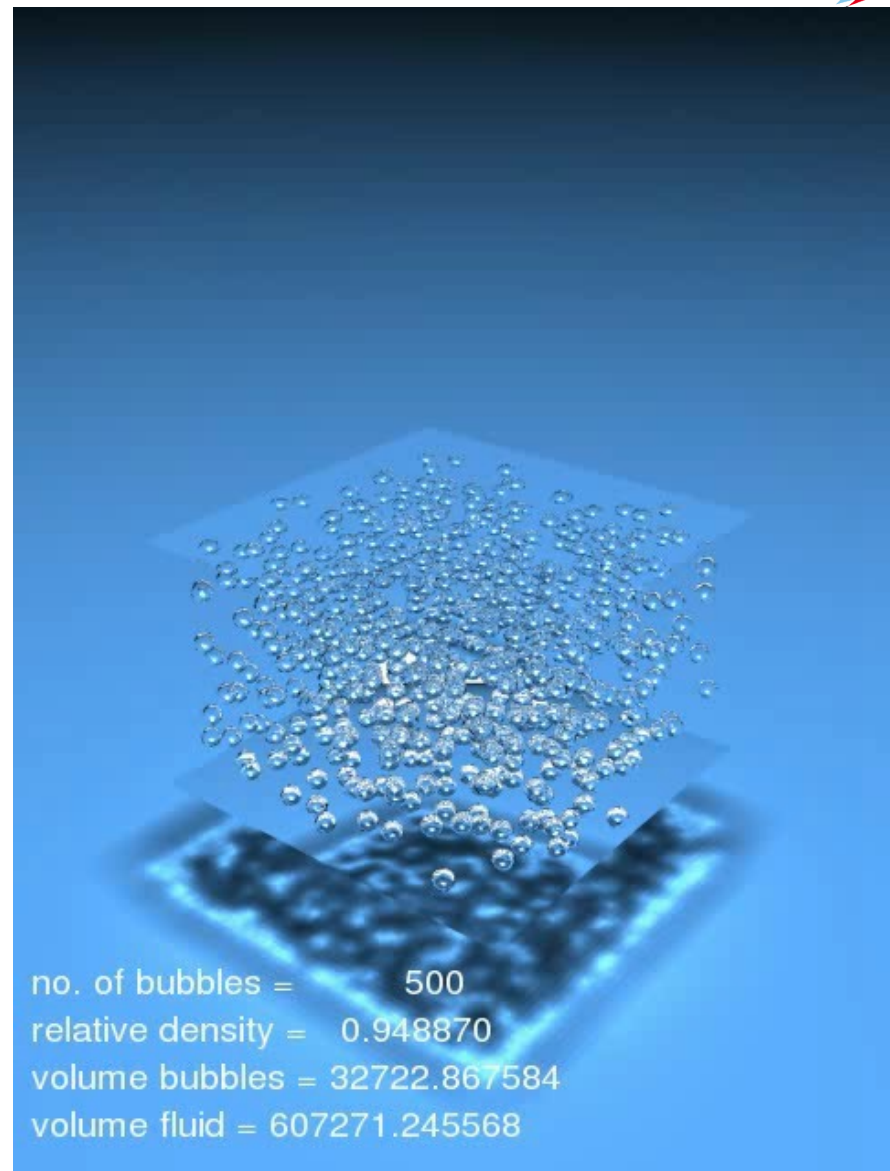


Foam generation with LBM

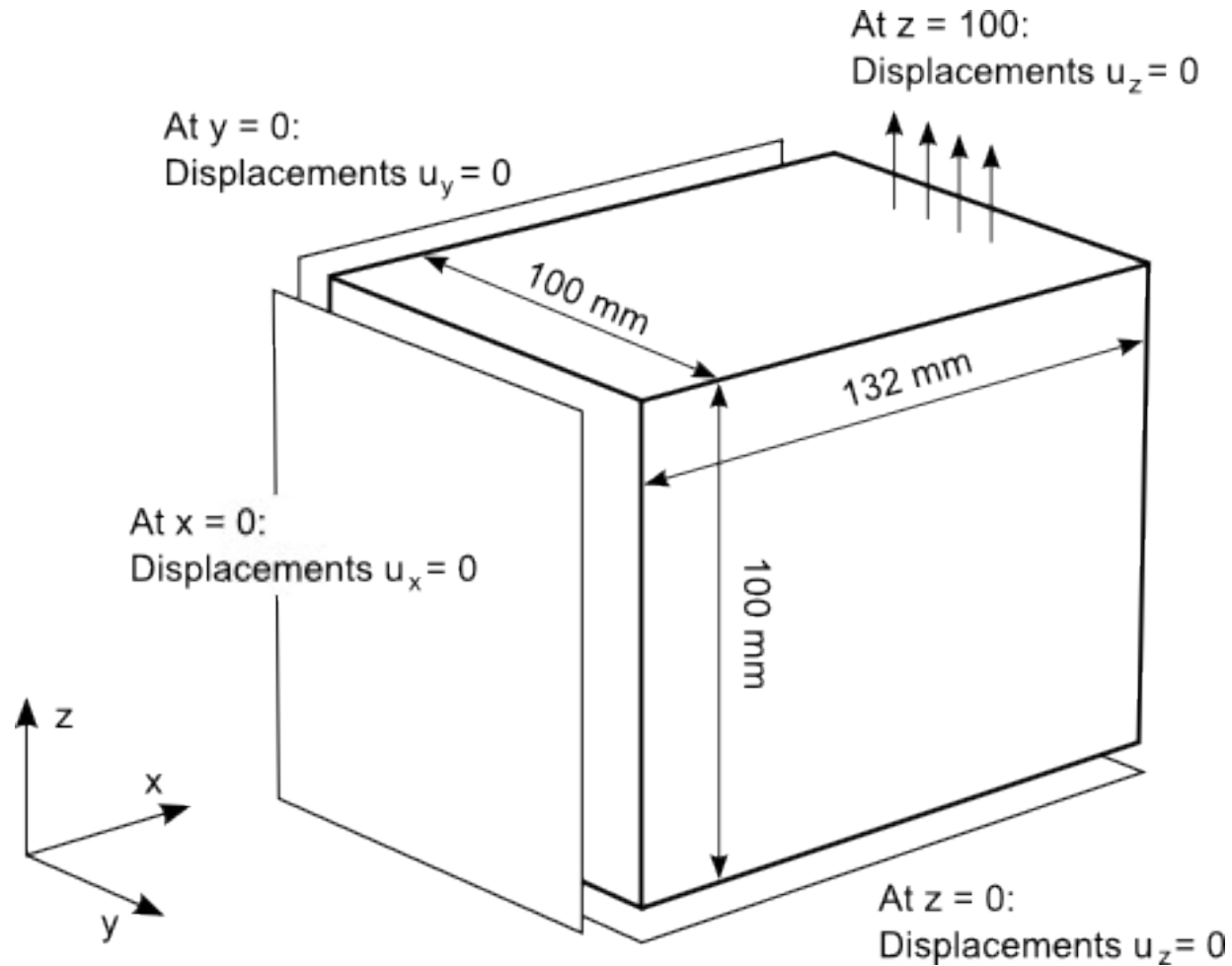
From:

C. Körner, M. Thies, T.
Hofmann, N. Thürey,
and U. Rüde:

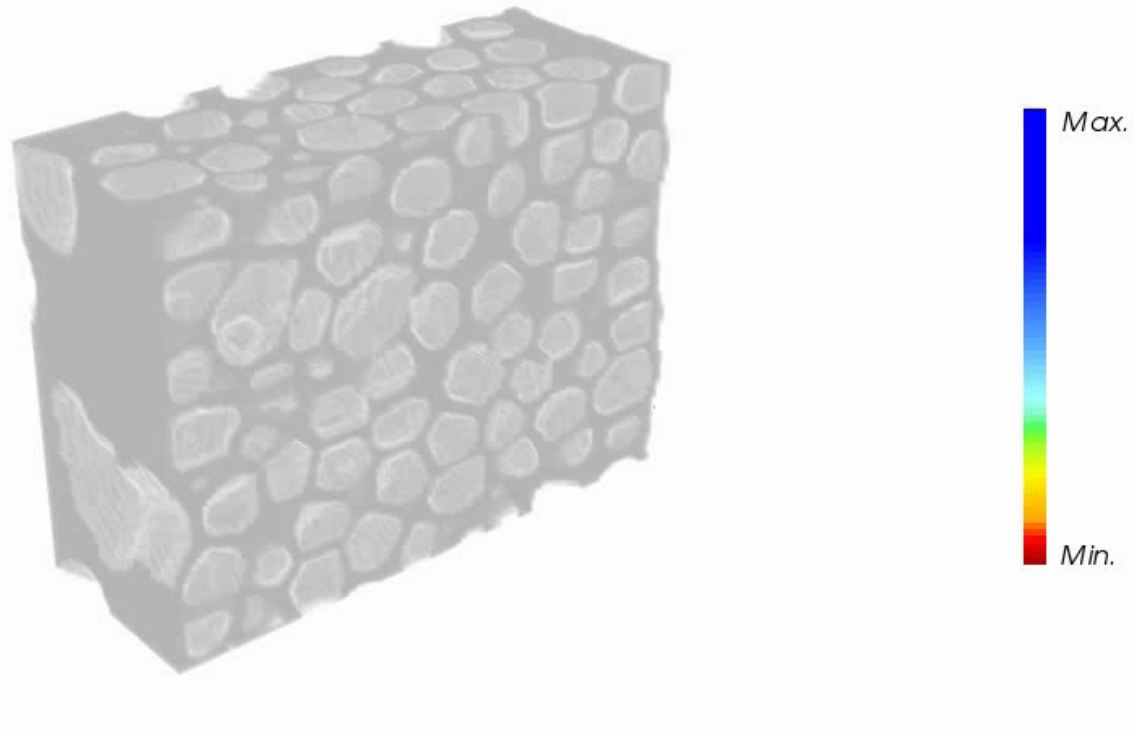
Journal of Statistical
Physics, Vol 121, 2005



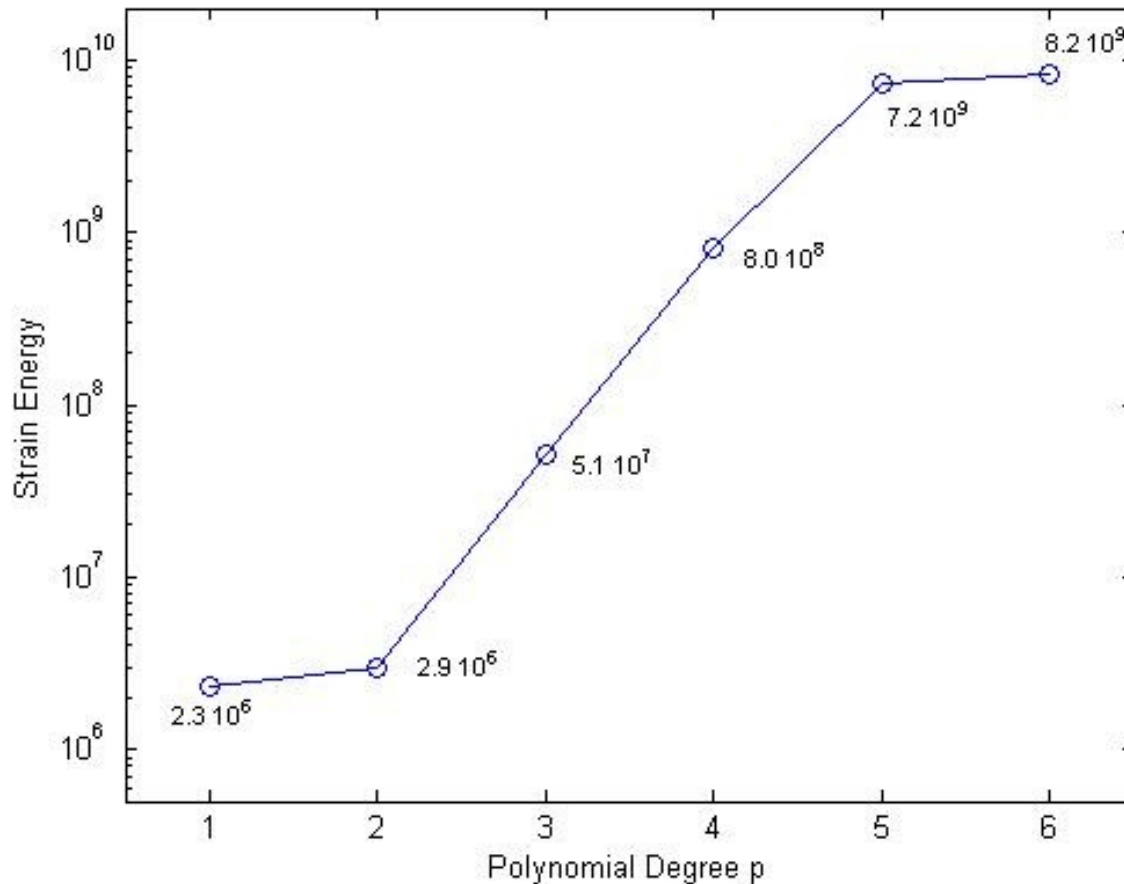
Uniaxial tension test



Structural analysis with FCM



Strain Energy as measure for Young's modulus



Computational effort for $p=6$:

- 770 sec on Intel quadcore-processor workstation
- No time for meshing

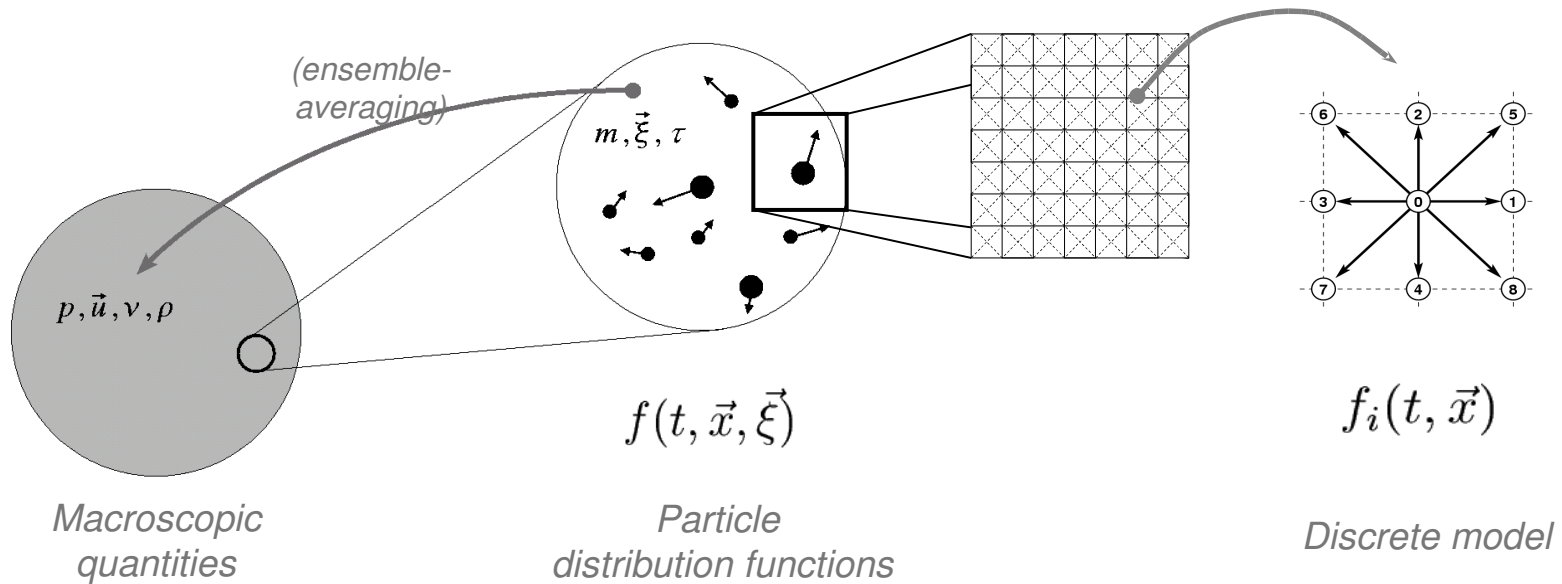
Summary

- Macroscopic mechanical properties of porous media, e.g. foam like structures are determined by their microscopic geometric structure
- The Lattice Boltzmann Method with free surface flow allows simulation of the formation of the microscopic structure of metal foams
- With the High order Finite Cell Method geometrically complex structures can be simulated without meshing

Future work

- More investigations to verification and validation necessary
- Extension of the method to obtain nonlinear material properties
- Combination with stochastic analysis

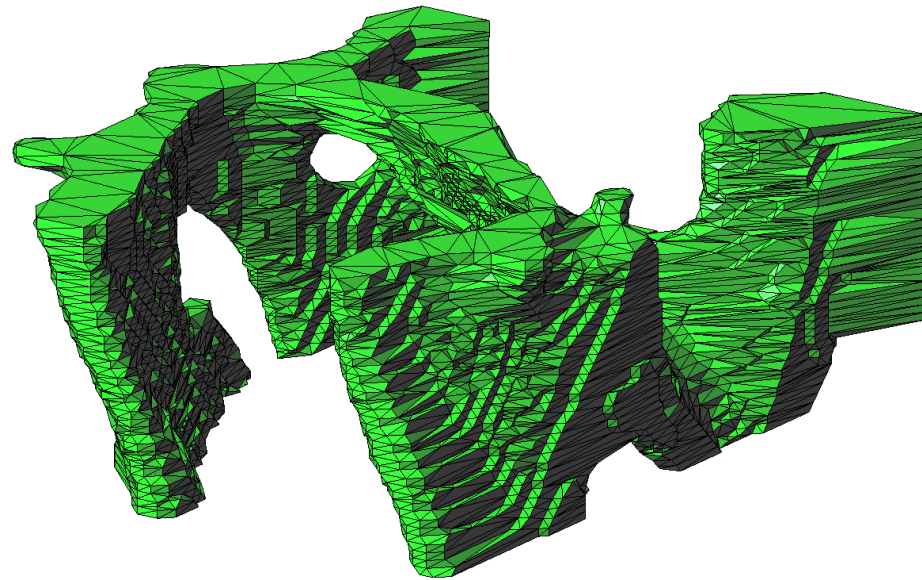
$$\frac{\partial f}{\partial t} + \vec{\xi} \frac{\partial f}{\partial \vec{x}} + \vec{F} \frac{\partial f}{\partial \vec{\xi}} = \Omega(f, f)$$



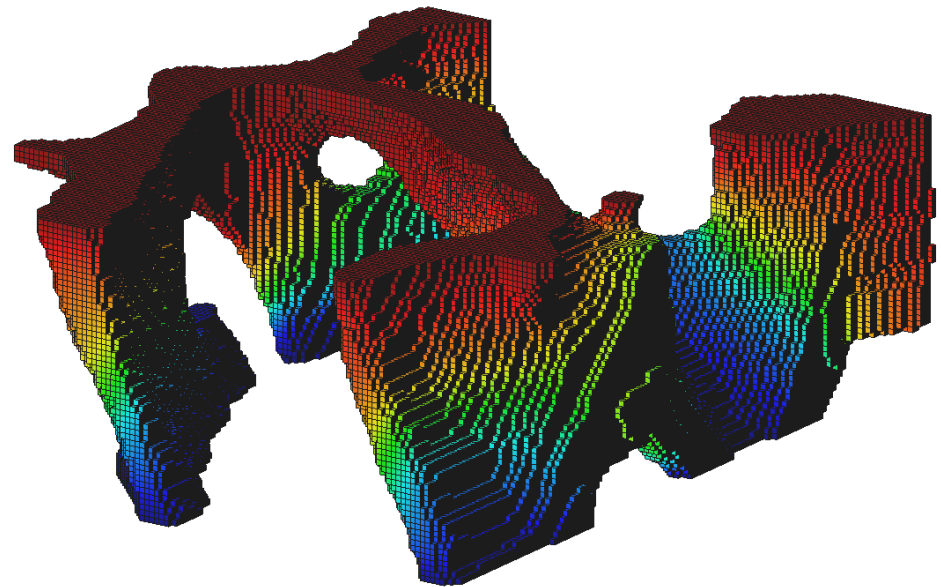
Multiple-relaxation-time lattice-Boltzmann equation

$$\underbrace{f_i(t + \Delta t, \vec{x} + \vec{\xi}_i \Delta t) - f_i(t, \vec{x})}_{\text{Propagation: phase space } \mathcal{F}} = - \mathbf{M}^{-1} \hat{\mathbf{S}} \underbrace{[m_i(t, \vec{x}) - m_i^{(0)}(t, \vec{x})]}_{\text{Collision: moment space } \mathcal{M}}$$

Finite Cells

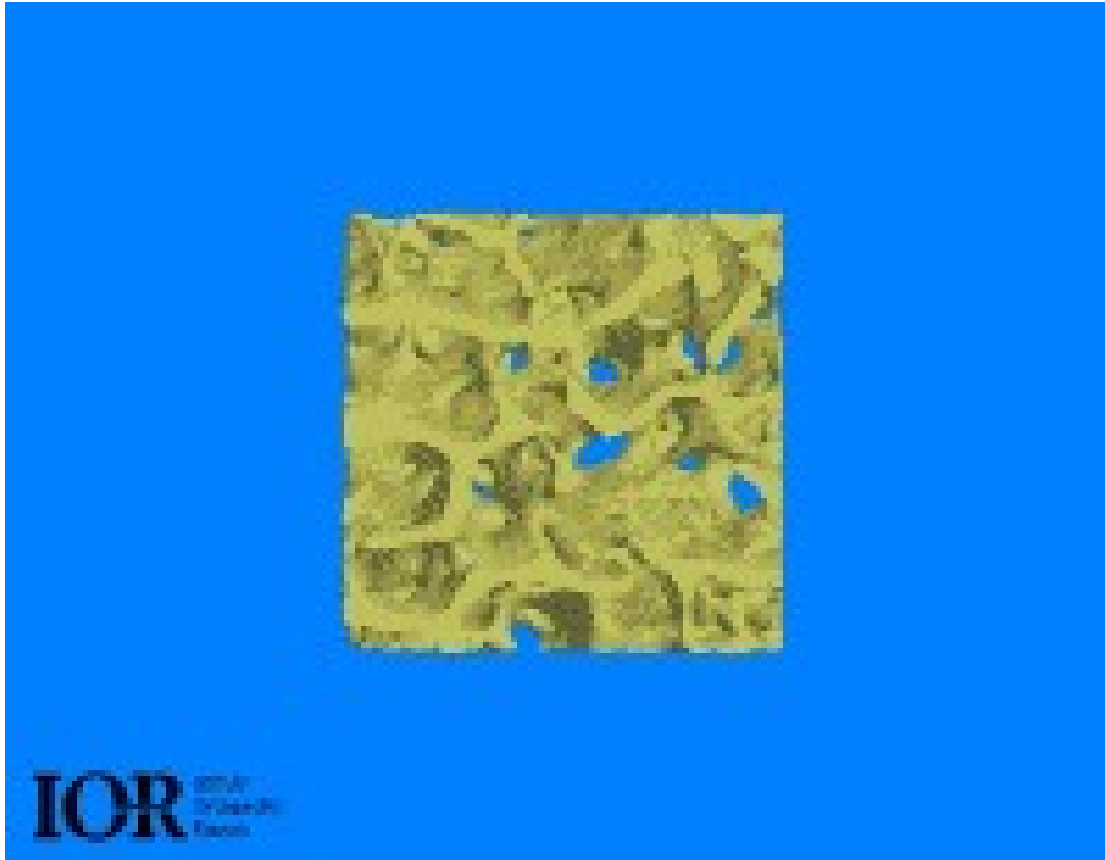


190 x 176 x 71 voxel



linear elastic material
behaviour assumed

A 3D-example: X-ray MicroCT examination of human bone



Human bone biopsy,
taken from the femoral
neck

Geometry:

10mm × 6mm × 5mm

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Some related methods

- Embedded domain method
- Fictitious domain method
- Meshfree/meshless methods
- Level set methods

in general for low order approximations, only.

Also similarities to

- Extended/enhanced finite element methods
- Generalized finite element methods
- Unfitted discontinuous Galerkin method